

## CHAPTER-II

### FINANCIAL APPRAISAL OF RAILWAY PROJECTS

|                  |  |
|------------------|--|
| 201- 202         | General Principles                                 |
| 203              | Scrutiny by Accounts officer                       |
| 204-205- 206-207 | Test-of Remunerativeness                           |
| 208 - 209        | Provision of Rolling Stock                         |
| 210              | Scheme for change of traction                      |
| 211-212- 213-214 | Earnings estimate                                  |
| 215-217          | Assessment of working expenses                     |
| 218              | Provision for depreciation                         |
| 219              | Normal Lives of assets                             |
| 220              | Technique of financial appraisal of projects       |
| 221-222          | Accounting rate of return method                   |
| 223-224          | Pay back period method.                            |
| 225              | Discounted cash flow                               |
| 226-227          | Net present value (NPV) or Net Present Worth (NPW) |
| 228              | Annual Cash Flows                                  |
| 229-230- 231-232 | Rate of return under D.C.F.                        |
| 233              | Residual Value                                     |
| 234              | Alternative Schemes                                |
| 235              | Economic Evaluation                                |
| 236 - 237        | Replacements and Renewals                          |
| 238              | Reconditioning                                     |
| 239 - 240        | Scrapping, condemning and abandoning assets        |
| 241 - 242        | Second hand value                                  |
| 243              | Post-projects appraisal                            |
| 244 - 247        | New Lines  |
| 248 - 252        | Open Line Works                                    |

| ANNEXURE                    |  |
|-----------------------------|--|
| <a href="#">Annexure A</a>  | Check list with detailed notes for guidance of zonal Railways and concerned branches in Railway Board's office, in the preparation of Project Estimates.   |
| <a href="#">Annexure B</a>  | Sinking fund Payment Table   |
| <a href="#">Annexure C</a>  | Interest formulas and tables for Discounted Cash flow techniques   |
| <a href="#">Table 1 -22</a> | <a href="#">Table 1</a> , <a href="#">Table 2</a> , <a href="#">Table 3</a> , <a href="#">Table 4</a> , <a href="#">Table 5</a> , <a href="#">Table 6</a> , <a href="#">Table 7</a> , <a href="#">Table 8</a> , <a href="#">Table 9</a> , <a href="#">Table 10</a> , <a href="#">Table 11</a> , <a href="#">Table 12</a> , <a href="#">Table 13</a> , <a href="#">Table 14</a> , <a href="#">Table 15</a> , <a href="#">Table 16</a> , <a href="#">Table 17</a> , <a href="#">Table 18</a> , <a href="#">Table 19</a> , <a href="#">Table 20</a> , <a href="#">Table 21</a> and <a href="#">Table 22</a> |
| <a href="#">Annexure D</a>  | Rate of return-using Discounted Cash Flow method.  |
| <a href="#">Annexure E</a>  | Examples illustrating application of DCF techniques in the financial appraisal of railway projects.  |
| <a href="#">Annexure F</a>  | Economic evaluation of Railway investments   |
| <a href="#">Annexure G</a>  | Examples illustrating the method of financial justification to be adopted in the replacement, reconditioning or abandonment of existing assets   |
| <a href="#">Annexure-H</a>  | Examples, illustrating the determination of second hand value of assets .  |

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## CHAPTER II

### FINANCIAL APPRAISAL OF RAILWAY PROJECTS

**201 General Principle.** - Investment decisions are among the most interesting and difficult decisions to be made by the Managements. It is fundamental to railway system as a commercial undertaking that expenditure other than that wholly chargeable to Ordinary Revenue incurred on new assets or for improvement of existing assets should be financially justified and sanctioned before it is actually incurred.

**202** As an exception to [Para 201](#), while no financial justification as such need be given in the following cases, it should be seen that the scale of expenditure incurred is as economical as possible consistent with the extant orders, if any, on the subject:-

- (a) when the expenditure is incurred on a statutory obligation (for example, the fencing of machinery) ;
- (b) when the expenditure is unavoidable on considerations of safety;
- (c) when the expenditure is incurred on passenger amenity works; and
- (d) When the expenditure is incurred on labour welfare works except residential buildings for which special rules are applicable.

Note:--(1) When expenditure on any of the above items forms part of a scheme and is not essential independently of the scheme, the total cost of the scheme, inclusive of the cost of the above works, should be financially justified.

(2) In the case of savings in engine days or wagon days or both by avoidance of or reduction in detentions to stock, etc., the financial justification should be worked out on the basis of increased locomotive or wagon, etc., utilization and consequent postponement of the purchase of new engines or wagons, etc., if such saving can be definitely secured, and not on the basis of the earning capacity of the stock saved.

(3) Savings on a particular railway should not be taken into account if they mean a loss on another railway. In such cases, the interest of railways as a whole should be considered.

(4) No credit should be given to a proposed scheme for a saving which can be achieved regardless of whether the proposed scheme is or is not embarked upon.

(5) If flag stations are included in the new scheme, the cost of operating them should be taken into account as an item of expense in working out the financial justification of the scheme.

(6) Where a number of works required in connection with and/or increasing the line or transshipment capacity have to be carried out on different stations of a section as part of a scheme, the financial justification should be worked out for the section as a whole, as it might be difficult to allocate anticipated savings to individual stations.

(7) Expenditure on works required for meeting statutory obligations or on consideration of safety should be subjected to proper scrutiny to see if the proposal is the result of a fresh development not already covered by the existing rules, or for implementation of a new recommendation of the Standing Safety Committee (accepted by the competent authority) or any Commission of Enquiry set up by Government, as the case may be.

**203 Scrutiny by Accounts Officer** -The Accounts Officer in his position as the Financial Adviser to the Administration, should carefully scrutinise the justification for proposed expenditure with reference to the principles enunciated in this Chapter and other orders on the subject. Even in cases where the return on the outlay is not the determining factor, it will be incumbent on him to examine and offer his advice on the general merits of the proposal in the spirit of a prudent individual spending his own money.

**204 Test of remunerativeness:** The net financial gain expected to accrue from a project be either by way of savings in expenditure or increase In net earnings (i.e. gross earnings less working expenses), or a combination of both. Except in case residential buildings, assisted sidings and rolling stock to which special rules are applicable, no proposal for fresh investment will be considered as financially justified unless it can be shown that the net gain expected to be realized as a result of the proposed outlay would after meeting the working expenses or average annual cost of service (see para 217) yield a return of not less than 10 percent under DCF method on the initial estimated cost.

(Authority: F (X)-II/2011/ROR/1 dated 05.10.2017)

Note- (1) Interest during construction should be added to the cost (excluding that chargeable to Revenue) of the projects, the construction of which is likely to last for more than one year.

(2) Depreciation should be calculated on the total cost of the scheme and not only on the portion chargeable to Capital, unless the contrary procedure can be justified in any particular case. However, depreciation as an element of working expense is to be ignored for assessing annual cash flows under the DCF Method (see para 228).

(3) In the case of construction of bridges, maintenance charges should include, besides the maintenance charges on the bridges proper, the maintenance charges of the training works also.

(4) The element of interest charges, vide item (d) of para 215, should be ignored in determining the average annual cost of service in the case of a new project, though it should otherwise be included for the purpose of working out the comparative cost of 2 or more alternative schemes.

**205** Following is an illustrative list of the various types of investment proposals which must pass the prescribed test of financial remunerativeness: -

5 New Lines: -

|   |
|---|
| (1) Project oriented or 'single purpose'. |
| (2) General purpose.                      |

(b) Line Capacity Works-

|  |
|--|
| (1) Gauge conversions.   |
| (2) Doublings.   |
| (3) Major Signalling Schemes i. e. Tokenless Block Working, Automatic Block Signalling., CTC, Route Relay Interlocking, etc. |
| (4) Lengthening of loops and/ or provision of additional loops.  |
| (5) Crossing stations.   |
| (6) Strengthening of electric traction distribution system and/or major modifications to electric traction installations.    |

© Yard Remodellings and Terminal Facilities-

|                                    |
|------------------------------------|
| (1) Marshalling yards.             |
| (2) Goods and passenger terminals. |
| (3) Transshipment points.          |

(d) Microwave and other Telecommunication Works.

5 Change of Traction (Electrification and Dieselisation) and provision of Loco Sheds therefore.

- 5 Introduction of new services-. Passenger trains, container services, street delivery and collection, out agencies etc.

(g) Workshops---

|                       |
|-----------------------|
| (1) Production Units. |
| (2) Repair Units.     |

**206** It may sometimes be necessary to reject a more economical alternative, because of considerations on which it is difficult to put a precise money value. If on the strength of any such factor a proposal is adopted that is less economical than its alternatives, the reasons determining such a choice should be recorded in the report of the estimate containing such proposals. In those cases in which the reasons as recorded are not accepted by the Accounts Officer, the latter should offer his remarks in his certificate of verification of the estimate concerned, so that these remarks may be taken into consideration by the authority sanctioning the proposal.

**207** In regard to works proposals estimated to cost Rs.50 lakhs or more, which are intended to increase line capacity, detailed traffic surveys should be conducted by a team consisting of officers of requisite status and experience from the Commercial/Operating Department and the Accounts Department. Where the traffic survey is conducted along with an engineering survey (Reconnaissance, Preliminary Engineering or Final location), the traffic survey report should be prepared under the general guidance of the Leader of the Team who will be an officer of appropriate status from the Civil Engineering Department.

**208 Provision of Rolling Stock** – Investment proposals for purchase/manufacture of additional rolling stock are to be justified on the basis of a general increase in the level of traffic which may or may not require line capacity works being taken up at the same time for the anticipated level of traffic. Where a line capacity work is justified due to anticipated increase in traffic, and also in the case of proposals for new line construction, the initial cost estimate should, for the purpose of Project appraisal, invariably include the cost of the rolling stock and the financial return on the project should be measured with reference to the overall initial cost of the project including the cost of rolling stock.

**209** A very substantial part of the capital-at-charge on the Railways is represented by the investment in rolling stock. The assessment of rolling stock required for moving additional traffic is directly related to the targets for movement of freight traffic, commodity-wise as projected by the Planning Directorate of the Railway Board. For additional passenger coaches, the Planning Directorate makes a forecast of the rate of growth of passenger traffic over a specified plan period. This detailed exercise should take into account the existing and projected operating parameters and efficiency indices such as wagon turn-round, provision for ‘sickness’, requirements for busy season, etc. In all cases where a distinctly new type of rolling stock is proposed to be acquired or manufactured, a detailed financial appraisal should be made of the proposed investment to see that it yields the requisite financial return.

**210 Scheme for change of traction** –Projects connected with the dieselisation and electrification are best formulated on a long term basis after considering the relative claims of the various high density sections of the Railways for better traction. A thorough techno-economic appraisal should be made in respect of each of the various sections proposed to be taken up for change of traction. Wherever possible, priorities for taking up the scheme for change of traction should be determined on the basis of the relative financial return expected from the various alternative schemes.

**211 Earnings estimate** –The earnings expected from additional traffic whether on the existing line or on a new line should be very carefully estimated in the traffic survey report. The estimate of earnings should be worked out for each commodity and for the lead from its origin up to the point of termination of the traffic. It should be ensured, however, that in case line capacity works are required to be undertaken in the contiguous section or Railway system over which the additional traffic is expected to be moved, the initial cost estimate for the scheme takes into account the cost of such additional line capacity works over the entire lead of the traffic.

**212** In the case of a ‘project-oriented’ new line, i. e., when a new railway line is proposed to be built to serve the needs of a specific project or industrial complex, the estimated earnings from the traffic which will move on the line should be assessed realistically in consultation with the authorities

concerned with that specific project. It is, however, essential that the Traffic Survey Team also makes its own independent assessment of the likely traffic which the project is expected to generate, instead of placing complete reliance on the data furnished by the Project Authorities or, in the case of a public sector undertaking, the concerned Department of the Government. The traffic survey officers must deeply probe into the various stages of scheduling of the project; e. g. what commitments have been entered into by the Project Authorities and whether the progress in the execution of the project is adequate to justify any specific claim in respect of the anticipated traffic. While working out the additional earnings from the traffic expected to move on the new line over its entire lead, the Railway Administration should make a careful assessment of the line capacity works required or terminal or any other facilities to be developed on the contiguous section/Railway system to carry this traffic. As stated in Para 211, if additional works are considered necessary, the scope and cost thereof should be defined and included in the main project estimate. In case it is considered that adequate line capacity exists in the contiguous section or Railway system so that the additional traffic on the new line can be carried throughout its lead on the Railway without any hindrance the Railway Administration should confirm that no additional works would be required to be undertaken anywhere on the system to carry this traffic.

**213** This approach inevitably involves grouping of a number of works with a common (or complementary) objective, such as for movement of additional traffic by improving line capacity, or for avoidance of detention to trains through yards. 'Group Justification' in such cases should be worked out for the project as a whole in case the individual works cannot stand on their own and must necessarily be taken up as part of a single project. However, where each of the works is self-contained, selection of priorities after consideration of various alternatives should necessarily be done with a view to 'sub-optimization', i.e. to realise the optimum benefit for the project by substituting the less remunerative sub-works by those anticipated to improve the return further.

**214** Before proposals are made out for new marshalling yards or major remodelling of existing marshalling yards or mechanisation of marshalling yards, goods terminals and transshipment yards, etc., a work study team should go into the actual working and suggest such improvements in operation as can be achieved even with the existing facilities. Additional facilities should be justified only after all the possibilities of improvement in working by optimum utilisation of the existing assets have been fully explored and evaluated. For line capacity works generally Master Charts should be prepared of the existing (optimum) capacity, the extent to which it is presently utilised, and the capacity expected to be available after the provision of the proposed facilities. The additional traffic beyond the optimum existing capacity of the section should only be reckoned for financial appraisal.

**215 (A) Assessment of Working expenses/Average Annual Cost of Service.**—The average annual cost of service of an asset is the sum of

- (a) the average annual cost of operation ;
- (b) the average annual cost of maintenance and repairs of the assets ;
- © the annual depreciation charges (but [see para 228](#)) ; and
- (d) annual interest charges on the cost of the asset.

Note. —In computing working expenses in financial evaluation of any capital expenditure proposal under D. C. F. technique, only items (a) and (b) above should be reckoned.

**(B) Average cost per unit of service.**-- The average cost per unit of service is obtained by dividing the average annual cost of service by the total number of units of service rendered by the asset in a year. In comparing two assets on this basis, care must be taken to see that the number of units of service taken into account in both cases represent the actual number utilised or consumed. Units of service rendered by either of the assets in excess of the actual requirements should be ignored in computing the cost per unit of the asset.

**216** For the purpose of assessment of the average annual cost of operation and maintenance, full use should be made of the traffic costing data relevant to the investment proposal under consideration. Correct application of the cost data and, in particular, assessment of the direct/variable and the indirect/fixed or semi-variable costs is very important in arriving at a realistic estimate of the working expenses in respect of the proposed scheme.

**217** In applying the unit cost data for working out the cost of moving the additional anticipated traffic, it has to be considered whether it would be reasonable to adopt the 'incremental cost' approach or to take 'fully distributed costs' into account. Logically, it would be realistic to work on the basis of 'incremental costs' for any small increases in traffic and over the short run. In the long run, however, even the so-called fixed costs will vary, and the incremental or marginal costs may fail to cover such semi-variable expenses. On the other hand, it would be equally unreasonable to apply fully distributed costs in all cases while working out the financial implications of a line capacity work. A realistic (though somewhat conservative) approach would, therefore, be to adopt 'long term variable costs' (based on percentages given at the end of [Annexure 'A'](#) for each item of cost) which will ensure not only that projects are not thrown out because of the adoption of the 'fully distributed costs' but also that a project is considered as remunerative so long as it yields the requisite return after meeting the 'long term variable costs'.

**218 Provision for depreciation-** Depreciation provision in respect of an asset will be equal to the annual payment to a Sinking Fund which, together with the interest thereon at such rates as may be prescribed by the Railway Board, when compounded annually, will provide the amount required for the replacement of the asset at the end of the normal life. The duration of the Sinking Fund payment will be determined by the 'normal life' of the asset, and the amount of the annual Sinking Fund payment will be ascertained by referring to the table reproduced as Annexure 'B' to this Chapter, which shows the annual amount payable at different rates of interest ranging from 2% to 8% (over periods extending up to 100 years)

**219 Normal lives of assets** –For the purpose of the annual Sinking Fund payment referred to in para 218, the normal life of the various classes of railway assets should be taken as in the table below :-

**(i) CIVIL ENGINEERING ASSETS**

| S.No.                     | Class of Assets                    | Average life in years |        |      |       |
|---------------------------|------------------------------------|-----------------------|--------|------|-------|
|                           |                                    | ROUTES                |        |      |       |
|                           |                                    | A & B                 | C(Sub) | D    | E     |
| 1. RAIL & FASTENTING etc. |                                    |                       |        |      |       |
| I.                        | Rail & Fastenings                  |                       |        |      |       |
| (a).                      | Rails                              | 20                    | 15     | 30   | *30   |
| (b).                      | Wooden Sleepers                    | 10                    | 10     | 10   | *10   |
| (c.1)                     | Metal sleepers (Cast Iron & Steel) | 20                    | 20     | 20   | *20   |
| (c.2)                     | Fittings steel trough              | 10                    | 10     | 10   | *10   |
| (d).                      | Concrete sleepers                  | 35                    | 35     | 40   | *40   |
| (e).                      | Elastic Fastenings                 |                       |        |      |       |
| (i)                       | Elastic Rail clips                 | 5-8                   | 5-8    | 8-10 | *8-10 |
| (ii).                     | Rubber Pads/ Liners                | 2-4                   | 2-4    | 4    | *4-6  |
| (f).                      | Switches                           | 4                     | 2 / 3  | 5    | *5    |
| (g).                      | Crossings                          | 5                     | 4/5    | 8    | *8    |
| 2 (A). MAJOR BRIDGES      |                                    |                       |        |      |       |
| (a).                      | Bridges work- Steel work           | 60                    |        |      |       |

|   |   |     |
|---|---|-----|
| (b).                                    | Bridge Masonry                          | 100 |
| ©.                                      | Structures Steel                        | 60  |
| (d).                                    | Structure- masonry and cement concrete  | 65  |
| (e).                                    | RCC Bridge Works                        | 60  |
| (f).                                    | Pre-stressed concrete-Bridge work       | 40  |
| <b>(B). MINOR BRIDGES</b>               |   |     |
| (a).                                    | Bridges work-Steel work                 | 60  |
| (b).                                    | Bridge Masonry                          | 100 |
| ©.                                      | Structures Steel                        | 60  |
| (d).                                    | Structure- masonry and cement concrete  | 65  |
| (e).                                    | RCC Bridge Works                        | 60  |
| (f).                                    | Pre-stressed concrete-Bridge work       | 40  |
| <b>3. FOOT OVER BRIDGES</b>             |   |     |
| (a).                                    | Bridges work-Steel work                 | 60  |
| (b).                                    | Bridge Masonry                          | 100 |
| ©.                                      | Structures Steel                        | 60  |
| (d).                                    | Structure- masonry and cement concrete, | 65  |
| (e).                                    | RCC Bridge Works                        | 60  |
| (f).                                    | Pre-stressed concrete-Bridge work       | 40  |
| <b>4.TRACK MACHINE (All Categories)</b> |   | 15  |

\* The service life as indicated in the table is general life/service life for track components. However renewal/replacement will be subject to various criteria laid down in IRPWM about its condition.

**(ii) COMPUTERS AND OTHER IT SYSTEMS**

| <b>S.No.</b> | <b>Class of assets</b>  | <b>Average life in years</b>   |
|--------------|---|--|
| <b>1</b>     | Active (viz. MIS systems including external storage systems and their connects) & Passive (viz. Network cabling) networking equipments  | 8 years  |
| <b>2</b>     | Small Multi-user systems and power supply equipments (viz. individual office LANs, UPS)   | 4 years  |
| <b>3</b>     | PCs   | 3 years  |
| <b>4</b>     | Secondary systems (Portable Computers/Laptops etc.)   | 4 years  |
| <b>5</b>     | Thin clients/Dumb terminals (for PRS/UTS etc.)<br><br>(Authority: Board's letter no.2002/AC-II/2/10/Vol.II dated 2 2.08.2012)—acs no.73 | 5 years (Local administration may approve premature condemnation up to 2 years earlier than the end of average life) |
| <b>6</b>     | Printers (All type)<br><br>(Authority : Board's letter no. 2002/AC-II/2/10/Vol.II dated 15-03-2012)—ACS NO.71 for S.No. 1 to 6          | 3 years (Local administration may approve premature condemnation up to 1 year earlier than the end of average life)  |
| <b>7.</b>    | ATVM (Composite Unit)<br>(Authority: Board's letter no.2002/AC-II/2/10/Vol.II dated 2 2.08.2012)—acs no.73                              | 4 Years  |

**( iii ) ELECTRICAL ASSETS**

| <b>S.No.</b> | <b>Class of assets</b>                                       | <b>Average life in years</b> |
|--------------|--|------------------------------|
| <i>1.</i>    | <i>Electric Locomotives</i>                                  | <i>35</i>                    |
| <i>2.</i>    | <i>EMU/Metro Motor Coaches and EMU/Metro Tractor Coaches</i> | <i>25</i>                    |
| <i>3.</i>    | <i>Rail Bus</i>  | <i>15</i>                    |
| <i>4.</i>    | <i>Over Head Power Lines</i>                                 | <i>40</i>                    |
| <i>5.</i>    | <i>Over Head Traction Line excluding contact wire</i>        | <i>60</i>                    |
| <i>6.</i>    | <i>Electric under ground Cables</i>                          | <i>30</i>                    |
| <i>7 (a)</i> | <i>Electric contact wire (Alm.)</i>                          | <i>25</i>                    |





| <b>S.No.</b> | <b>Class of assets</b>  | <b>Average life in years</b> |
|--------------|---|------------------------------|
| 1            | <b>AC EQUIPMENT</b>   |                              |
| (i)          | 25 KV Inverter  | 15                           |
| (ii)         | AC Control Panel (As per F-I codal life is 12 yrs.)   | 15                           |
| (iii)        | Inverter Panel  | 15                           |
| 2            | <b>TL Power Equipment</b>   |                              |
| (i)          | 4.5/18/22.75/25 KW Alternator (As per F-I codal life of Dynamo is 20 years)   | 12                           |
| (ii)         | 800 A.H.L.A Battery   | 4                            |
| (iii)        | 1100 AH VRLA (SMF) Battery  | 4                            |
| (iv)         | Diesel Engine for Power Cars  | 16                           |
| (v)          | Alternator for Power Car  | 15                           |
| 3            | <b>Electric Locomotive Equipments</b>   |                              |
| (i)          | All Electric rotating machines up to 25 HP used on Electric Locomotives, EMU's Coaches and stationary items                     | 12                           |
| (ii)         | All Electric rotating machines above 25 HP and upto 750 HP used on Electric Locomotives, EMU's Coaches and for stationary items | 12                           |
| (iii)        | Traction Motor  | 18                           |
| (iv)         | Traction Converters   | 18                           |
| (v)          | Auxiliary Converters  | 18                           |
| (vi)         | Control Electronics   | 18                           |
| (vii)        | Tap-Changer   | 35                           |
| (viii)       | Rectifier Block   | 18                           |
| (ix)         | Traction Gears  | 12                           |
| (x)          | Motor Suspension  | 12                           |
| (xi)         | Bogies with Wheel   | 18                           |
| (xii)        | Armature for Traction Motors  | 15                           |
| (xiii)       | Stator for Traction Motor   | 18                           |
| (xiv)        | Commutator for Traction Motor   | 15                           |
| (xv)         | Locomotive re-cabling   | 18                           |
| 4            | Microprocessor based control and fault diagnostic system  | 12                           |
| 5            | Speedometer cum recorder and monitoring system  | 10                           |
| 6            | BA Panel  | 18                           |
| 7            | VCB   | 18                           |
| 8            | DBR (roof mounted)  | 9                            |
| 9            | DBR (vertical mounted)  | 9                            |
| 10           | Pantograph  | 12                           |
| 11           | <b>TRD Equipments</b>   |                              |

Contd 2-

|               |  |  |
|---------------|--|--|
| (i)           | Current/Potential/transformer  | 30                                     |
| (ii)          | Earthling system in sub-station <i>etc.</i>                                  | 15                                     |
| (iii)         | Lighting arrestor (Gapless type)   | 15                                     |
| (iv)          | Lighting arrestor (Convertor type)   | 15                                     |
| (v)           | Buster & Terminal connection   | 30                                     |
| (vi)          | Battery charger  | 15                                     |
| (vii)         | Relay (Electromechanical)  | 15                                     |
| (viii)        | Relay (Electronic)   | 15                                     |
| (ix)          | Instruments (Electrical)   | 30                                     |
| (x)           | Instruments (Electronic)   | 30                                     |
| (xi)          | Relay testing kit & other testing equipment                                  | 15                                     |
| <b>(xii)</b>  | <b>OHE conductors &amp; components - For Normal Zone</b>                     |  |
| (a)           | OHE fixed structures   |  |
|               | (i) Mast / Structure / Guy Rod / foundation                                  | 80                                     |
| (b)           | <b>Other than fixed structures</b>   |  |
|               | (i) Cantilever assembly and all types of insulators                          | 40                                     |
|               | (ii) Isolators / ATD   | 30                                     |
| (c)           | <b>Wires</b>   |  |
|               | (i) Catenary / feeder wire / return conductor                                | 60                                     |
|               | (ii) Contact wire  | *40 or on the basis of condemning date |
| <b>(xiii)</b> | <b>OHE conductors &amp; components - For Polluted Zone</b>                   |  |
|               | (i) Cantiliver assembly & all types of insulators                            | On condition basis                     |
|               | (ii) ATD   | On condition basis                     |
| <b>(xiv)</b>  | <b>PSI equipments</b>  |  |
| (a)           | <b>Substation's equipments</b>   |  |
|               | (i) Power Transformer / Auxiliary Transformers                               | 40                                     |
|               | (ii) All types of cables   | 30                                     |
|               | (iii) Fixed capacitor bank   | 15                                     |
| (b)           | <b>Control equipments</b>  |  |
|               | (i) Circuit Breaker, panels, all switchgear and protective circuits          | 25                                     |
|               | (ii) SCADA system  | 10                                     |
| <b>(xv)</b>   | <b>Transmission line equipments &amp; components</b>                         |  |
|               | (i) 110KV/132 KV, ACSR conductors / Earth wire / insulators / Tower fittings | 60                                     |
| 12            | 38 Tower Wagons (both 4 wheeler, 8 wheeler & all types)                      | 40                                     |

(Authority: Railway Board's letter no 2002/ACII/2/10 Vol II dated 29.11.2019)

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**C). Equipments required for replacement through Revenue**

| <b>S.No.</b> | <b>Class of assets</b>  | <b>Average life in years</b> |
|--------------|---|------------------------------|
| <b>1</b>     | <b>Electric Loco Equipment</b>                                      |                              |
| (i)          | <i>Armature for Traction Motor</i>                                  | <i>15</i>                    |
| (ii)         | <i>Stator for Traction Motor</i>                                    | <i>18</i>                    |
| (iii)        | <i>Commutator for Traction Motor</i>                                | <i>15</i>                    |
| (iv)         | <i>Auxiliary Motor</i>  | <i>18</i>                    |
| (v)          | <i>Arno Converter</i>   | <i>18</i>                    |
| (vi)         | <i>Blower Impeller/Casing</i>                                       | <i>10</i>                    |
| (vii)        | <i>Locomotive re-cabling</i>  | <i>18</i>                    |
| (viii)       | <i>Power Cables</i>   | <i>18</i>                    |
| (ix)         | <i>Control Cables</i>   | <i>18</i>                    |
| (x)          | <i>Compressor with exhausters complete recondition /replacement</i> | <i>10/15</i>                 |
| <b>2</b>     | <b>AC Equipment</b>   |                              |
| (i)          | <i>Compressor ACCEL/ CARRIER</i>                                    | <i>10</i>                    |
| (ii)         | <i>Sealed Compressor KCL make</i>                                   | <i>5</i>                     |
| (iii)        | <i>Sealed Compressor Maneurope make</i>                             | <i>8</i>                     |
| (iv)         | <i>Compressor Motor DC</i>  | <i>10</i>                    |

| <b>S.No.</b> | <b>Class of assets</b>   | <b>Average life in years</b> |
|--------------|--|------------------------------|
| (v)          | <i>Compressor Motor AC</i>   | 15                           |
| (vi)         | <i>Condenser Fan Motor (DC)</i>                                    | 8                            |
| (vii)        | <i>Condenser Fan Motor (AC)</i>                                    | 10                           |
| (viii)       | <i>Condenser Fan Motor (RMPU)</i>                                  | 10                           |
| (ix)         | <i>Evaporater Fan Motor (AC)</i>                                   | 10                           |
| (x)          | <i>Evaporater Fan Motor (DC)</i>                                   | 10                           |
| (xi)         | <i>Evaporater Fan Motor (RMPU)</i>                                 | 12                           |
| (xii)        | <i>Condenser Unit</i>  | 8                            |
| (xiii)       | <i>Condenser Unit (RMPU)</i>                                       | 10                           |
| (xiv)        | <i>Evaporater unit</i>   | 10                           |
| (xv)         | <i>Evaporater unit (RMPU)</i>                                      | 10                           |
| (xvi)        | <i>Mercury in glass thermostat</i>                                 | 5                            |
| <b>3</b>     | <b>TL/Power Equipment</b>  |                              |
| (i)          | <i>4.5/18/22.75/25 KW alternator regulator</i>                     | 12                           |
| (ii)         | <i>Emergency 90 AH L!A. Battery</i>                                | 3                            |
| (iii)        | <i>120 AH VRLA (SMF) Batttery</i>                                  | 4                            |
| (iv)         | <i>290 AH starting L.A. Batteries for Power Car</i>                | 3                            |
| (v)          | <i>Power Car power panel</i>                                       | 15                           |
| (vi)         | <i>Power panel (AC coaches)</i>                                    | 15                           |
| (vii)        | <i>Pre Cooling cum battery charging transformer rectifier unit</i> | 12                           |
| (viii)       | <i>50 KVA 750/415 V transformer unit</i>                           | 15                           |
| (ix)         | <i>3 KVA 415/190 V transformer</i>                                 | 15                           |
| (x)          | <i>Water Raising Apparatus (WRA)</i>                               | 5                            |
| (xi)         | <i>Water Boiler for Pantry</i>                                     | 5                            |
| (xii)        | <i>Hot Case for Pantrv</i>   | 5                            |
| (xiii)       | <i>Bottle Cooler cum deep freezer</i>                              | 5                            |
| (xiv)        | <i>Ventilation Blower Motor for Power Car</i>                      | 12                           |
| (xv)         | <i>Radiator for Power car</i>                                      | 10                           |
| (xvi)        | <i>Radiator Motor for Power Car</i>                                | 15                           |

#### **(IV) MECHANICAL ASSETS**

| <b>S.No.</b> | <b>Class of assets</b>   | <b>Average life in years</b> |
|--------------|--|------------------------------|
|              | <b>Machinery &amp; Plant</b>   |                              |
| 1            | <i>Machine Tools like Lathes, Planners, Drilling, Boring and Milling machines etc.</i> | 15                           |
| 2            | <i>High Precision and special purpose machines like wheel Lathes etc.</i>              | 15                           |
| 3            | <i>Tool Room and Testing Laboratory equipment</i>                                      | 15                           |
| 4            | <i>Foundry and Forge Equipment</i>   | 15                           |

| <b>S.No.</b> | <b>Class of assets</b>   | <b>Average life in years</b> |
|--------------|--|------------------------------|
| 5            | <i>Heat Treatment Equipment</i>  | 15                           |
| 6            | <i>Cranes-EOT /140 B.D Crane</i>   | 36                           |
| 7            | <i>Power Generation Machinery &amp; Switches</i>   | 15                           |
| 8            | <i>General purpose light machinery e.g. band saws, floor grinder etc.</i>  | 10                           |
| 9            | <i>Air Compressors</i>   | 15                           |
| 10           | <i>Other miscellaneous machines e.g. light cleaning machines, test equipment in diesel sheds, workshops, depots &amp; sick lines</i> | 15                           |
| 11           | <i>(i). Construction Machinery</i>   | 15                           |
|              | <i>(ii). Track Maintenance equipment</i>   | 20                           |
| 12           | <i>Station machinery e.g. weighing machines etc.</i>   | 15                           |
| 13           | <i>Miscellaneous machinery and equipment for hospital, offices etc.</i>  | 10                           |
| 14           | <i>Mechanical Weigh Bridges</i>  | 15                           |
| 15           | <i>Electronic in motion Weigh Bridges</i>  | 08                           |
| 16           | <i>Diesel Pumps</i>  | 10                           |
| 17           | <i>Welding equipment including diesel welding sets</i>   | 10                           |
| 18           | <i>Diesel refrigeration equipment</i>  | 15                           |
| 19           | <i>Material handling equipment like FLT, Lister trucks etc.</i>  | 10                           |
| 20           | <i>Traversers</i>  | 25                           |
| 21           | <i>Fuel Station Dispensation Equipment</i>   | 10                           |
| 22           | <i>Bulldozers and other earth moving equipment</i>   | 15                           |
| 23           | <i>Motor Boats</i>   | 10                           |
| 24           | <i>Hydraulic re-railing equipments/Hydraulic Systems</i>   | 16                           |
|              | <b>ROAD VEHICLES</b>   |                              |
| 25           | <i>Staff Cars including Jeeps</i>  | 07                           |
| 26           | <i>Light Motor Vehicles</i>  | 10                           |
| 27           | <i>Heavy Motor Vehicles</i>  | 10                           |
| 28           | <i>Tractors</i>  | 10                           |
|              | <b>ROLLING STOCK</b>   |                              |
| 29           | <i>Diesel Electric/Hydraulic Locomotives</i>   | 36                           |
| 30           | <i>Diesel Engine</i>   | 18                           |
| 31           | <i>Shunting Locomotives</i>  | 36                           |
| 32           | <i>Steam Locomotives</i>   | 40                           |
| 33           | <i>Boiler and Tender</i>   | 20                           |
| 34           | <i>Steam Cranes</i>  | 30                           |
| 35           | <i>Diesel Hydraulic Cranes</i>   | 25                           |
| 36           | <i>Steel Body Coaches including DMUs / EMUs, Restaurant Cars etc.</i>  | 25                           |
| 37           | <i>Full Stainless Steel Body Coaches including DMUs/EMUs, Restaurant Cars etc.</i>   | 30                           |
| 38           | <i>Light utilisation categories of coaches (steel body) like inspection carriages etc.</i>   | 40                           |

| <b>S.No.</b> | <b>Class of assets</b>   | <b>Average life in years</b> |
|--------------|--|------------------------------|
| 39           | <i>IRS Coaches</i>   | 30                           |
| 40           | <i>Open Bogie wagons with air brakes and Casnub bogies</i>               | 30                           |
| 41           | <i>Bogie tank wagons with air brakes and Casnub bogies</i>               | 40                           |
| 42           | <i>All other types of Bogie wagons with air brakes and Casnub bogies</i> | 35                           |
| 43           | <i>Open wagons with vacuum brakes and UIC bogies</i>                     | 25                           |
| 44           | <i>Other wagons with vacuum brakes and UIC bogies</i>                    | 30                           |
| 45           | <i>4- Wheeler wagons (open and covered)</i>                              | 30                           |
| 46           | <i>4- Wheeler tank wagons (with plain bearings)</i>                      | 35                           |
| 47           | <i>4-Wheeler tank wagons (with roller bearings)</i>                      | 35                           |
|              | <b>Equipment/Sub assemblies of Diesel locos</b>                          |                              |
| 48           | Engine Block   | <b>18</b>                    |
| 49           | Crank Shaft  | <b>18</b>                    |
| 50           | Turbo Super Charger  | <b>12</b>                    |
| <b>51</b>    | Governor   | <b>18</b>                    |
| 52           | ECC assembly with RA Gear Box  | <b>18</b>                    |
| 53           | Radiator Fan   | <b>16</b>                    |
| <b>54</b>    | Heat Exchangers including radiator                                       | <b>10</b>                    |
| 55           | Expressor/Compressor   | <b>16</b>                    |
| 56           | Bogies with wheels   | <b>18</b>                    |
| 57           | Traction Motor   | <b>18</b>                    |
| 58           | Traction Generator/Alternator  | <b>18</b>                    |

| <b>S.No.</b> | <b>Class of assets</b>   | <b><i>Average life in years</i></b> |
|--------------|--|-------------------------------------|
| <b>59</b>    | All electrical rotating machines above 5 HP on Diesel locos          | <b>18</b>                           |
| 60           | Rectifiers   | <b>18</b>                           |
| 61           | Traction Gear  | <b>18</b>                           |
| 62           | Loco Batteries   | <b>4</b>                            |
| 63           | Power Cables   | <b>18</b>                           |
| 64           | Control Cables   | <b>18</b>                           |
| 65           | Blowers  | <b>10</b>                           |
| 66           | Armature for Traction Motor  | <b>18</b>                           |
| 67           | Stator for Traction Motor  | <b>20</b>                           |
| 68           | Control Equipments   | <b>18</b>                           |
|              | <b>Equipment/Sub assemblies of DMUs</b>                              |                                     |
| 69           | Power Pack   | <b>16</b>                           |
| 70           | Bogies with wheels   | <b>18</b>                           |
| 71           | Traction Motor   | <b>18</b>                           |
| 72           | Traction Generator/Alternator  | <b>18</b>                           |
| <b>73</b>    | All electrical rotating machines above 5 HP on DMUs/Rail bus/Railcar | <b>18</b>                           |
| <b>74</b>    | Rectifiers   | <b>18</b>                           |
| 75           | Heat Exchangers  | <b>10</b>                           |
| 76           | Batteries  | <b>4</b>                            |
| <b>77</b>    | Power Cables   | <b>18</b>                           |



| <b>S.No.</b> | <b>Class of assets</b>   | <b>Average life in years</b> |
|--------------|--|------------------------------|
| <b>78</b>    | Control Cables   | <b>18</b>                    |
| <b>79</b>    | Control Equipments   | <b>18</b>                    |
| <b>80</b>    | Hydraulic Transmission Rehabilitation/Replacement  | <b>16</b>                    |
|              | (Authority: Board's letter no.2002/AC-II/1/10 dated 12.10.2007)S.No. 48 to 80-acs no.65. |                              |

**(V) SIGNAL & TELECOMMUNICATION ASSETS**

**(A) SIGNALLING SYSTEM**

| <b>S.No.</b> | <b>Class of assets</b>  | <b>Routes</b>  | <b>Average life in years</b>                                |
|--------------|---|--|---|
| <b>1.</b>    | <i>Electrical/ Mechanical Signalling System</i>                                 | <ul style="list-style-type: none"> <li>Route-' A '</li> <li>Route- 'C'/Sub Urban section</li> <li>Big Yards on all Routes</li> </ul> | <i>25 Yrs.</i>  |
|              |   | <ul style="list-style-type: none"> <li>Routes- 'B'</li> <li>Route 'D'</li> <li>Route 'D'-special'</li> </ul>                         | <i>25 to 28 Yrs depending upon location &amp; condition</i> |
|              |   | <ul style="list-style-type: none"> <li>Routes-'E'</li> <li>Route 'E- Special'</li> </ul>   | <i>30 Yrs</i>   |
| <b>2.</b>    | <i>Electronic Signalling system like SSI, Axle Counter, AWS, AFTC, IPS etc.</i> |  | <i>15 years or based on obsolescence.</i>                   |

**(B) SIGNALLING EQUIPMENT**

| <b>S No</b> | <b>Class of assets</b>                       | <b>Life in terms of operations</b> | <b>Average life in years</b> |           |                    |                      |                      |
|-------------|--|------------------------------------|------------------------------|-----------|--------------------|----------------------|----------------------|
|             |  |                                    | <b>Routes</b>                |           |                    |                      |                      |
|             |  |                                    | <b>A</b>                     | <b>B</b>  | <b>C/ Suburban</b> | <b>D &amp; D-Spl</b> | <b>E &amp; E-Spl</b> |
| <b>1</b>    | <i>Cranks and Compensators</i>               | <i>50,000</i>                      | <i>2</i>                     | <i>2</i>  | <i>1</i>           | <i>4</i>             | <i>4</i>             |
| <b>2</b>    | <i>Lock Bar Clips</i>                        | <i>1,00,000</i>                    | <i>3</i>                     | <i>3</i>  | <i>3</i>           | <i>5</i>             | <i>7</i>             |
| <b>3</b>    | <i>Facing Point Lock with bolt detection</i> | <i>3,00,000</i>                    | <i>8</i>                     | <i>8</i>  | <i>8</i>           | <i>15</i>            | <i>15</i>            |
| <b>4</b>    | <i>Mechanical Detectors</i>                  | <i>5,00,000</i>                    | <i>-</i>                     | <i>15</i> | <i>—</i>           | <i>20</i>            | <i>25</i>            |

| S<br>No | Class of assets  | Life in<br>terms of<br>operations  | Average life in years |                |                |              |           |
|---------|--|--|-----------------------|----------------|----------------|--------------|-----------|
|         |  |  | Routes                |                |                |              |           |
|         |  |  | A                     | B              | C/<br>Suburban | D &<br>D-Spl | E & E-Spl |
| 5       | Circuit breakers   | 5,00,000   | 15                    | 15             | 15             | 25           | 30        |
|         | Lever locks  | -  | 7                     | 7              | 7              | 12           | 15        |
| 6       | EK Transmitter   | -  | 10                    | 10             | 10             | 15           | 15        |
| 7       | SM's Slide Frame   | -  | 30                    | 30             | 30             | 30           | 30        |
| 8       | Electric Point Detector &<br>Reversors   | -  | 15                    | 15             | 15             | 20           | 20        |
| 9       | Signal Machines  | 1,50,000   | -                     | 10             | -              | 20           | 20        |
| 10      | Signal Wire Transmission   | -  | 3                     | 3              | 3              | 3            | 3         |
| 11      | Point Machine  | 3,00,000   | 12                    | 12             | 7              | 15           | 15        |
| 12      | Plug-in and Shelf type<br>Relays   | 10,00,000  | 25                    | 28             | 25             | 28           | 30        |
| 13      | Track Feed battery chargers  | -  | 10                    | 10             | 10             | 10           | 10        |
| 14      | Signal Transformers,   | -  | 12                    | 12             | 12             | 12           | 12        |
|         | Transformers   | -  | 10                    | 10             | 10             | 10           | 10        |
| 15      | Batteries  | -  | 4                     | 4              | 4              | 4            | 4         |
| 16      | Block Instruments  | -  | 25                    | 25             | 25             | 25           | 25        |
| 17      | Cable<br>(Authority : Board's letter<br>no.2002/AC-II/1/10 dated<br>18.08.2006)-AC NO.63 | -  | 25                    | 25<br>to<br>28 | 25             | 30           | 30        |
| 18      | Block Instrument Electro<br>Mechanical   | -  | 20                    | 20             | 20             | 20           | 20        |
| 19.     | LED Signals (all<br>aspect types) of<br>specification prior to<br>version 2011           | (Authority :<br>Board's letter<br>no.2002/AC-<br>II/1/10 dated<br>28.08.2015)-<br>AC NO.78 | 6                     | 6              | 6              | 6            | 6         |
| 20.     | LED Signals (all<br>aspect types) of<br>specification version<br>2011 or later           | (Authority :<br>Board's letter<br>no.2002/AC-<br>II/1/10 dated<br>28.08.2015)-<br>AC NO.78 | 8                     | 8              | 8              | 8            | 8         |

**(C) TELECOMMUNICATION EQUIPMENT**

| S..No. | Class of assets                  | Average life in years |
|--------|----------------------------------|-----------------------|
| 1      | Microwave Equipment              | 12-15 Years           |
| 2      | Exchange & accessories including | 12-15 Years           |

| <i>S.No.</i> | <i>Class of assets</i>  | <i>Average life in years</i>    |
|--------------|---|---------------------------------|
|              | <i>Telephone equipment</i>  |                                 |
| 3            | <i>Under Ground Cables</i>  | <i>Quad}-20 Years<br/>PLJF}</i> |
|              |   | <i>OFC -20 Years</i>            |
| 4            | <i>Overhead alignment</i>   | <i>25 Years</i>                 |
| 5            | <i>All other electronic/ wireless items including OFC equipment</i>   | <i>12-15 Years</i>              |
| 6            | <i>Cell Phones</i>  | <i>5-8 Years</i>                |
| 7            | <i>FAX</i>  | <i>10 Years</i>                 |
| 8            | <i>Walkie-Talkie Sets/VHF</i>   | <i>5-8 Years</i>                |
| 9            | <i>Datacomm. Equipment, Routers, Modems, PCs etc.</i>   | <i>5-8 Years</i>                |
| 10.          | LED display Board for Passenger Information System, True Colour Video cum Train Information Display System<br>(Authority: Board's letter no.2002/AC-II/2/10(Vol.II)...ACS no.76 dated 25.0.2014 | <i>10 Years</i>                 |
| 11.          | GPS based Digital Clocks<br>(Authority: Board's letter no.2002/AC-II/2/10(Vol.II)...ACS no.76 dated 25.0.2014   | <i>10 Years</i>                 |
|              |   |                                 |

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**(Authority Railway Board letter No.2002/AC-II/1/10 dated 24 /05/06)-acs no. 62**

**220 Technique of financial appraisal of projects-** The following methods of appraisal of capital expenditure proposals are commonly used in industrial and commercial undertakings: -

- (a) Accounting rate of return,
- (b) Pay back period, and
- (c) Discounted Cash Flow.

Of these, methods, (a) & (b) are employed without considering the time value of money. These are also known as the 'Financial statement' methods since the calculation involves data taken from and used essentially in the same form as in financial statements. When time is considered, the method employed for financial appraisal is the Discounted Cash Flow method, also called the 'Present value method', since the time value of money is an explicit consideration.

**221 Accounting rate of return method -** Under this method, the rate of return is worked out by arriving at a percentage ratio of the net gain (i. e., earnings less working expenses) over the initial anticipated investment of the project. Simply illustrated, it is proposed to construct a masonry building at a cost of Rs.1 lakh to accommodate an office which is now housed in a building at a rental of Rs.15,000 per annum. It will be necessary to ascertain (a) the average annual cost of maintenance and repairs of the proposed building and (b) its scrap value at the end of its normal life. If these are taken to be (say) Rs. 5,000 and Rs. 10,000 respectively, then the average annual cost of the proposed new building will be (a) Rs.5,000 plus (b) Rs. 801 being the annual sinking fund payments (at 3 per cent for 50 years which is equal to 0.0089 multiplied by Rs.1 lakh minus Rs.10,000), or Rs.5,801 in all. This will result in a saving of Rs. 9,199 (Rs.15,000 minus Rs. 5,801) in the annual rental charges that are presently being paid, or a net return of 9.2 percent on the investment of Rs.1 lakh.

**222** A minor variant of the above illustration would be to take the average investment over the life of the asset at half the initial cost, viz., Rs.50,000 on the assumption that depreciation is written off in equal instalments over the life of the asset and the amount invested on the asset will decrease each year as funds are released through the effect of the depreciation charge. In that case the return on the average investment will work out to 18.4%.

**223 Pay back period method** -Since recoupment of the original capital invested in a project is an important consideration in appraising a capital investment, the method of working out the pay back period lays emphasis on the calculation of the time it takes to recoup the expenditure incurred on the project. In the table given below, the pay back period is 5 years, as the accumulation of the net cash flow, year by year equals the initial investment at the end of 5 years:

**Original Investment-Rs. 1,00,000**

**Net Cash Flows (i. e., net earnings or reduction in expenditure) : --**

| Year | Annual | Cumulative |
|------|--------|------------|
|      | Rs.    | Rs.        |
| 1    | 10,000 | 10,000     |
| 2    | 12,000 | 22,000     |
| 3    | 20,000 | 42,000     |
| 4    | 30,000 | 72,000     |
| 5    | 28,000 | 1,00,000   |

Under this method no attempt is made to assess the return on the capital invested. It only shows the length of time required to recoup the amount invested on the project, the assumption being that projects with short pay back period are better investment propositions than those with long pay back periods. Bare recoupment of the amount invested under the pay back period method would yield no return unless a suitable rate of interest return on the capital outstanding in each of the years involved is built into the calculation of the net cash flow.

**224** The method of ranking projects, or project grading, on the basis of pay back period is of limited application as it can be employed only in situations where there is a strict time limit to the investment before the expiry of the useful life of the project. An example would be of a proposed investment in a project in a foreign country where the political stability can be foreseen only for a limited number of years, or in plant and machinery involving processes or products that are likely to be replaced by technological changes within a few years or a 'single purpose' new line where the known reserves of coal, iron ore, etc., are expected to be depleted/exhausted after a specific number of years. Though presently not in vogue on the Indian Railways, there is no bar to the application of the Pay Back Period method to evaluation of Railway Projects in consultation with the FA & CAO in the special circumstances illustrated in this Para.

**225 Discounted Cash Flow** -The accounting 'Rate of Return' (R.O.R.) Method commonly in use on the Railways does not take into account the time value of money. Also, the return on investment is worked out as at the time of completion of the project or at a single point of time (6<sup>th</sup> year or 11<sup>th</sup> year) and not through the entire useful life of the project. The R.O.R. method may, therefore, yield an incorrect result depending on the point of time selected for the purpose of project appraisal. A factor of fundamental importance to investment decisions and one which the R.O.R. method does not take into account is the timing of profits and cash flows that result from an investment and this factor is crucial to the Discounted Cash Flow Method of project appraisal.

**226 Net Present Value (NPV) or Net Present Worth (NPW)** -The concept of the time value of money which is basic to the Discounted Cash Flow Method is illustrated thus :

Rs.100 receivable today is more than Rs.100 receivable a year hence, as Rs. 100 received today will earn interest or profits and shall accumulate to more than Rs. 100 in a year's time. Alternatively, Rs. 100 received today can be used to reduce borrowing thereby avoiding interest payments as well as reducing debts by Rs.100. Assuming that the Railways' cost of finance is its current dividend rate (say 6% per annum), Rs. 106 received a year hence should be worth Rs.100 today and Rs.100 which may be received in a year's time is worth about Rs. 94 today (actually it is worth Rs.94.34). Likewise, the present value of Rs.100 receivable 2 years hence is about Rs.89, and so on. In this way the cash flow for the project in any future year can be discounted to obtain the present value.

**227** The NPV/NPW of a project is sum of the present values of the net cash flows for all the years of the project's economic life. The net cash flow in each year will be the expected net reduction in expenditure or increase in net earnings. The net cash flows are discounted to arrive at the NPV of a project by applying a pre-determined discount rate. Interest formulae & tables commonly used in the Discounted Cash Flow method are given in [Annexure 'C'](#). Present value/worth factors (PWF) of Re. 1 are shown in the Annexure separately for 'single payment', i. e., when cash flows are uneven, and for uniform series, i.e., when cash flows in each year are the same. For example, consider the following excerpts:

| TABLE--A<br>From Col.2 under 'Single payment' |       |       |       |
|---|-------|-------|-------|
| Present value of Re. 1                        |       |       |       |
| Year  | 12%   | 15%   | 20%   |
| 1   | 0.893 | 0.870 | 0.833 |
| 2   | 0.797 | 0.756 | 0.694 |
| 3   | 0.712 | 0.657 | 0.579 |
| 4   | 0.635 | 0.572 | 0.482 |
| 5   | 0.567 | 0.498 | 0.402 |

| TABLE-B<br>From Col. 4 under 'Uniform series' |   |       |       |
|---|---|-------|-------|
| Years   | Present Value of Re.1 received annually |       |       |
|   | 12%                                     | 15%   | 20%   |
| 1   | 0.893                                   | 0.870 | 0.833 |
| 2   | 1.690                                   | 1.626 | 1.528 |
| 3   | 2.402                                   | 2.283 | 2.106 |
| 4   | 3.037                                   | 2.855 | 2.589 |
| 5   | 3.605                                   | 3.352 | 2.991 |

TABLE -B is derived by adding the data in Table A, . At 20% the 0.833 in TABLE-B is the same as the 0.833 in TABLE-A since the time involved is only one year. The 0.833 and the 0.694 for years 1 and 2 under 20% represent the 1.528 under TABLE-B at 20% in year 2. The 0.833, 0.694 and 0.579 in TABLE-A are added to form the 2.106 in TABLE-B. Thus, it can be seen that TABLE-B is essentially a summation of TABLE-A. With TABLE-B, present value calculations can be made more quickly if the cash in flows or out flows are constant. Instead of multiplying the same cash flows by the individual items of TABLE-A, one can multiply

the annual cash flow only once by the sum of the data in TABLE-A which is conveniently arranged in TABLE-B.

**228 Annual Cash Flows-** It is important that the annual cash flows should be estimated on a realistic basis. By definition, the cash flow will take into account only the realisable earnings and cash expenditure or, in the case of expenditure reducing projects, the net reduction in cash expenditure. Purely accounting adjustments such as depreciation and other provisions are to be completely ignored. The reason is that cash flow is the foundation of the NPV and depreciation is an expense item not involving a flow of cash. It is implicit in the basic arithmetic of the D.C.F. Method of project appraisal that so long as the cash flows are adequate from year to year and the NPV computed at the requisite discount rate equals or exceeds the investment, the capital invested in the Project will remain intact. This is shown by a solved example below :

Basic data-

|                          |    |                                      |
|--------------------------|----|--------------------------------------|
| Initial investment       | .. | Rs. 4,00,000                         |
| Annual Cash Flow         | .. | Rs. 1,00,000                         |
| Life of the Project      | .. | 10 years                             |
| DCF rate of return (say) | .. | 21.4% <a href="#">(See Para 230)</a> |

| Year | Capital in the beginning of the year | Net surplus the year | Payment of interest @ 21.41 % | Recovery of Capital | Capital at the end of the Year |
|------|--------------------------------------|----------------------|-------------------------------|---------------------|--------------------------------|
| (1)  | (2)                                  | (3)                  | (4)                           | (5)                 | (6)                            |
| 1    | 4,00,000                             | 1,00,000             | 85,652                        | 14,348              | 3,85,652                       |
| 2    | 3,85,652                             | 1,00,000             | 82,580                        | 17,420              | 3,68,232                       |
| 3    | 3,68,232                             | 1,00,000             | 78,919                        | 21,081              | 3,47,151                       |
| 4    | 3,47,151                             | 1,00,000             | 74,335                        | 25,665              | 3,21,486                       |
| 5    | 3,21,486                             | 1,00,000             | 68,840                        | 31,160              | 2,90,326                       |
| 6    | 2,90,326                             | 1,00,000             | 62,168                        | 37,832              | 2,52,494                       |
| 7    | 2,52,494                             | 1,00,000             | 54,067                        | 45,933              | 2,06,561                       |
| 8    | 2,06,561                             | 1,00,000             | 44,231                        | 55,769              | 1,50,792                       |
| 9    | 1,50,792                             | 1,00,000             | 32,289                        | 67,711              | 83,081                         |
| 10   | 83,081                               | 1,00,000             | 17,790                        | 82,210              | 871                            |
|      |                                      |                      |                               | 3,99,129            |                                |

The small margin of difference (Rs.871) is accounted by the error in interpolation of the rate of return. It will be seen that at the discount rate of 21.41%, the project has recovered the original cost in full (Col. 5), apart from paying off interest at the same rate.

**229 Rate of return under D. C. F.-**Two alternative methods can be used for assessing the viability of a project under the D. C. F. technique. For example, assuming an even cash flow of Rs.4,000 per annum over a period of 10 years in respect of a project where the original investment is estimated to be Rs.18,000, it will be observed from the following table that the discount factor of 4.5 (18,000 ÷ 4,000) occurs against the 10th year under the discount rate of 18%;

|      | Present value of the Re. 1 received annually |     |     |
|------|--|-----|-----|
| Year | 16%  | 18% | 20% |

|    |       |       |       |
|----|-------|-------|-------|
| 8  | 4.344 | 4.078 | 3.837 |
| 9  | 4.607 | 4.303 | 4.031 |
| 10 | 4.833 | 4.494 | 4.192 |
| 11 | 5.029 | 4.656 | 4.327 |

In this case the rate of return under the D.C.F method for an even cash flow of Rs.4,000 per annum for an investment of Rs.18,000 will be about 18%. Since the D.C.F. return of 18% is more than the minimum acceptable rate of return (say 10%), the project would be considered desirable from the financial point of view. Under an alternative method, the minimum acceptable rate of return (say 10%) would be applied to calculate the NPV of the project. If the NPV is (zero or) positive, it would be financially acceptable, and if the NPV is negative, the project will not be financially acceptable. In judging the ranking of competing projects, under the first method, the D. C. F. rate of return would be used and whichever project gives the higher rate of return would be preferred. Under the second method, the competing projects will be ranked according to their NPV and whichever project gives a higher NPV at the minimum acceptable rate of return would be the preferred project.

**230.** Another illustration may be given of a case where the initial outlay of (say) Rs. 4,00,000 is incurred in one year and the project starts giving a net cash flow of Rs.1,00,000 per annum over 10 years thereafter. Discounted cash flow at various rates of interest would be as shown below where the cash flows are uniform throughout the project life:

|   | 10%       | 20%      | 25%      |
|---|-----------|----------|----------|
| Factor for 10th year                              | 6.145     | 4.192    | 3.571    |
| NPV for even cash flow of<br>Re. 1 lakh per annum | 6,14, 500 | 4,19,200 | 3,57,100 |

R. O.R. will be about 21.41%

**231** The simple illustrations given above presume that the investment is completed in one year and the project starts yielding a return immediately thereafter. Where the investment is spread over a number of years, it is necessary to work out the value of the investment, by applying the relevant rate of interest, from the inception up to the point when the project is expected to be ready for operation, the rate of interest being the minimum acceptable rate of return of (say) 10%. In the illustration given in the preceding para, if the investment of Rs. 4,00,000 is assumed to have been spread over a period of three years including the year in which the project was completed, the total investment, inclusive of interest, up to the year of completion would be as shown below :----

| Year             | 0%<br>Interest<br>Rs. | 10%<br>interest<br>Rs. |
|------------------|-----------------------|------------------------|
| -2               | 1,00,000              | 1,21,000               |
| -1               | 1,50,000              | 1,65,000               |
| 0                | 1,50,000              | 1,50,000               |
| Total investment | 4,00,000              | 4,36,000               |

In this case, if the net return over the life of the project of ten years assumed in the earlier illustration is constant amount of Rs.100,000, the return would be about 18% instead of 21.41 % worked out in Para 230.

**232** A short write-up on the technique of working out the rate of return under the Discounted Cash Flow Method is at [Annexure 'D'](#). Detailed examples of railway projects showing application of the D. C. F. technique are given in [Annexure 'E'](#).

**233 Residual Value** -Each project will have an estimated life span at the end of which the various assets will be disposed of or put to other uses. The flow of funds created by the sale or disposal of the assets at the end of the life of the project should be estimated so that appropriate credit can be given to the project in the year in which the flow of funds is expected to occur by the sale or disposal of the assets. Since all the assets may not be discarded or sold at the same time, the cash flows resulting from residual values should be allocated to the years in which they are likely to be received. If some of the assets are to be taken out of service and disposed of before the termination of the project, the resultant cash flows must be included in the appropriate years.

**234 Alternative Schemes --- Equivalent Annual Cost** - The criterion of choice between alternative schemes, each of which is capable of rendering the required service, is the principle of least cost in the long run. This approach is particularly applicable when the cash outflows under each competing project have sharply different time patterns. To obtain the annual cost, the outlays of the project are summarised into a single present worth amount and then spread over the years of the project life as an equal amount per year, which includes interest at a standard rate. By the same summarization and spreading for an alternate project, the two projects can be compared by reference to the per year figure for each. The comparison is usually of cost only, revenues being assumed as the same under either project. An illustration appears below :

|  | Year | 0     | 1    | 2    | 3    | 4    | Total. |
|--|------|-------|------|------|------|------|--------|
| <b>Project A :</b>   |      |       |      |      |      |      |        |
| cash inflows   |      |       |      |      |      |      |        |
| cash outflows  |      | (104) | (5)  | (10) | (15) | (20) | (154)  |
| <b>Project B :</b>   |      |       |      |      |      |      |        |
| cash inflows   |      |       |      |      |      |      |        |
| cash outflows  |      | (45)  | (30) | (30) | (30) | (30) | (165)  |
| 10% pre cent :<br>Worth Factors  |      | 1.00  | .91  | .83  | .75  | .68  | ....   |
| <b>Present Worth :</b>   |      |       |      |      |      |      |        |
| Project A  |      | (104) | (5)  | (8)  | (11) | (14) | (142)  |
| Project B  |      | (45)  | (27) | (25) | (22) | (20) | (139)  |
| <b>*Equivalent Annual Cost :</b>   |      |       |      |      |      |      |        |
| Project A  |      | ....  | (45) | (45) | (45) | (45) | ...    |
| Project B  |      | ...   | (44) | (44) | (44) | (44) | ...    |
| *These annual amounts are determined by dividing the project present worth by the present worth of a four-year Re.1/- per year annuity. This is the sum of the individual present worth factors .91, .83, .75, .68 which totals Rs 3.17. |      |       |      |      |      |      |        |

The above analysis shows that Project 'B' has the lower uniform annual cost, by a small margin, even though it shows a larger total outlay. The reason for this is that the project outlays take place later under



Project 'B', which reduces its present worth and lowers its annual cost including interest, relative to Project 'A'.

**235 Economic Evaluation.** -As a commercial undertaking, it is incumbent on the Railways to ensure that a proper financial return is earned from every investment subject to the exceptions given in [Para 202](#). At the same time it has to be borne in mind that the Railways are an important instrument of economic and industrial development of backward areas not connected by a reliable transport network. In the case of major projects such as new line constructions, or change of traction from steam to diesel/electric, the benefits likely to be realised by the economy as a whole are assessed by the Economic Adviser to the Railway Board. The principles on which economic evaluation of Railway investments should be carried out as distinct from working out a financial return to the Railways, are indicated in the note (together with an illustration) at [Annexure 'F'](#).

**236 Replacements and Renewals** -The proposal for replacement of an existing asset (whether involving improvement or otherwise) should be examined critically with a view to seeing whether it would not be possible to avoid, or, at least, postpone such replacement by suitable repairing or reconditioning the asset at a cost that could be comparatively justified financially. In all cases in which it is considered necessary to replace an asset, instead of reconditioning it, it should be examined whether the estimated average annual cost of service (i. e. cost of operation and maintenance, sinking fund payment to the depreciation fund, and the interest on the cost of the asset), or the estimated average cost per unit of service of the new asset is likely to be less than that of the old asset after reconditioning. Except when renewals or replacements are inevitable, the expenditure chargeable to the Depreciation Reserve Fund, should be financially justified in the same manner as any other expenditure of capital nature.

**237** Where a replacement is proposed on grounds of economy in operation and maintenance costs, the estimate therefore should justify the outlay on the proposed replacement by showing that the average annual cost of service or the average cost per unit of service, that will be rendered by the new asset, is less than that of the existing asset.

Note.-The above two paragraphs will not apply to cases of casual or programme renewals, not involving any improvement

**238 Reconditioning** – When an as asset is repaired at a comparatively high cost in preference to its being replaced, it is referred to as being ‘reconditioned’. The cost of such reconditioning is chargeable to Ordinary Repairs and Maintenance, for which no detailed estimates are ordinarily necessary. Nevertheless, for all reconditioning works, the estimated cost of each of which exceeds Rs 20,000 detailed estimates should be prepared.

Note:- Detailed estimates should, however, be prepared in respect of reconditioning works of rolling stock, each costing more than the following limits:-

|   |        |
|---|--------|
| Locomotives                                     | 25,000 |
| Carriages (including rail cars and EMUs)        | 12,500 |
| Wagons, tenders, boilers and service motor-cars | 5,000  |

**239 Scrapping, condemning and abandoning assets** - An asset may be scrapped, condemned or abandoned without replacement, when the service rendered by it is no longer required. If the service rendered by it is still necessary and if it is proposed to make other arrangements for such service, it should be definitely established that it is more economical to scrap, condemn or abandon the existing asset and obtain the required service from the new arrangement than to continue to obtain the required service from the existing asset. Here also the relative economics of the two proposals should be assessed on the basis of the average annual cost of service or the average cost per unit of service, as the case may be.

**Note :** The preparation of financial justification as contemplated in this paragraph is not necessary for condemning rolling stock in the following cases:-

- i) Overaged stock due to be replaced by virtue of their age but condemned before replacement.
- ii) Under or overage stock involved in accidents and certified to be irreparable (not included under the category of “beyond economical repairs”).
- iii) Non I.R.S. type coaches and wagons of inherently weak design proposed to be condemned on condition basis whether under or overage.

**240** Example are given in [Annexure ‘G’](#) illustrating the method of financial justification to be adopted in the case of replacement, reconditioning or abandonment of existing assets. The data used in the illustrations are hypothetical and the methods adopted are not to be regarded as exhaustive or as precluding the use of other methods that may be found to be more appropriate. The D.C.F. method can be conveniently used in some cases as has been shown in Example (1) of [Annexure ‘G’](#).

**241 Second-hand Value-** The second-hand value of an asset is what it is presently worth and has often to be distinguished from its scrap value. For purposes of financial justification of transfer, purchase or sales, the second-hand value of assets may, except in certain cases (e.g. rails, locomotives, boilers, etc.) where separate rules have been prescribed for the determination of the second-hand value, be determined as provided below:-

- i) The first cost of an asset (based on which its second-hand value has to be computed) should be taken as the value of a similar asset at present day prices and not the value actually paid for the asset when it was originally purchased.
- ii) The second-hand value of an asset that does not depreciate is the same as the first cost.
- iii) The second-hand value of a depreciating asset should be so appraised that the average annual cost of service or the average cost per unit of service, as the case may be, of the second-hand asset is equal to that of the same or similar asset while new.

**242** Examples illustrating the application of the principles enunciated in the preceding paragraph are given in [Annexure ‘H’](#).

**243 Post project appraisal -** It is important that an investment proposal is subjected to proper financial appraisal not only before it is sanctioned but also a certain period of time after the project has been in operation. Whether the financial return anticipated from a project at the estimate stage is actually realised in due course or not should be determined by conducting a ‘Productivity test’ in respect of all major works. For any such comparison to be meaningful and realistic, it is important that the computation of the actual additional earnings and working expenses is done on the same lines as at the project estimate stage. As commercial profitability is liable to be affected by escalation in prices or any other extraneous development, in order to have a more reliable and accurate evaluation wherever relevant, a comparison in terms of physical units of throughput may be carried out. Such a comparison should preferably be done classwise in the case of passenger traffic and commodity-wise in the case of goods traffic.

**244 New Lines -** In respect of each new line opened for traffic, the railway administration should submit to the Railway Board a statement, showing the financial results of its working in Form No. 244 shown below. The statement should reach the Railway Board not later than the 31<sup>st</sup> December following the financial year to which it refers and should be accompanied by a covering memorandum in which brief explanations should be given of important variations between the actual realisation and the estimated earnings, together with a Note by the General Manager indicating how the actual net cash flow compares with what was estimated at the project stage. The Note should also bring out the probable traffic prospects of the line in the sixth and the eleventh year of opening.

**Statement showing Financial Results of working of New Branch Lines.**

Form No.F.244

Railway -----

Name of branch -----

Length in Kilometres-----

Gauge -----Opened on-----

| Year  | Cost on 31 <sup>st</sup> March<br>plus calculated<br>interest during<br>construction. |          | Earnings of Branch<br>line proper |          | Actual expenditure<br>of branch assessed<br>on the basis of<br>costing/financial<br>data applied to the<br>traffic over the<br>branch line |         | Net earning of<br>branch proper<br>(Col.3-4) |         |
|---|---|----------|-----------------------------------|----------|--|---------|--|---------|
|   |   |          |                                   |          | Working expenses<br>(excluding<br>depreciation &<br>interest)  |         |  |         |
|   | As<br>originally<br>Estimated.  | Actuals. | As<br>originally<br>Estimated.    | Actuals. | As<br>originally<br>Estimated  | Actuals | As<br>originally<br>Estimated.               | Actuals |
| (1)   | (2)   |          | (3)                               |          | (4)  |         | (5)  |         |
| Actuals after<br>opening --<br>1 <sup>st</sup> year ..<br>2 <sup>nd</sup> year ..<br>3 <sup>rd</sup> year ..<br>4 <sup>th</sup> year ..<br>5 <sup>th</sup> year ..<br>6 <sup>th</sup> year ..<br>7 <sup>th</sup> year ..<br>8 <sup>th</sup> year ..<br>9 <sup>th</sup> year ..<br>10 <sup>th</sup> year and<br>so on upto 30<br>years |   |          |                                   |          |  |         |  |         |

| Main line   |          |   |          | Additional net earnings(Col.6-7). |         | Total net earnings (Col.5+8) |         | Return on total cost Col.9x 100 |  | Remarks |
|---|----------|---|----------|-----------------------------------|---------|------------------------------|---------|---------------------------------|--|---------|
| Additional earnings minus any loss due to short circuiting or diversion of traffic. |          | Additional expenses calculated on the basis of costing/ financial data applied to traffic from the existing line to branch line and vice-versa. |          |                                   |         |                              |         | Col.2                           |  |         |
|   |          | Working expenses (excluding depreciation & interest)  |          |                                   |         |                              |         |                                 |  |         |
| As  | Actuals. | As  | Actuals. | As                                | Actuals | As                           | Actuals |                                 |  |         |

|                         |  |                          |  |                         |  |                         |  |    |    |
|-------------------------|--|--------------------------|--|-------------------------|--|-------------------------|--|----|----|
| originally<br>Estimated |  | originally<br>Estimated. |  | originally<br>Estimated |  | originally<br>Estimated |  |    |    |
| 6                       |  | 7                        |  | 8                       |  | 9                       |  | 9A | 10 |

Foot notes to Form No. F. 244.-

- 1). Actuals will be actuals to end of the year for which accounts have been closed, and fresh estimates for the years thereafter.
- 2). Special steps taken in the course of the year:-

(a) To develop the traffic earnings-

(b) To reduce the expenses

- (i)
- (ii)
- (iii)
- (iv)

- (i)
- (ii)
- (iii)
- (iv)

- (3). Probable future development of traffic and possibility of the line paying its way (short note)--

Head of Traffic Department.

Head of Account Department

**Note:-** The traffic data required to be maintained vide [Para 245](#) should be used for costing purposes so as to arrive at the expenditure of the Branch proper and of traffic moving from the existing line to the Branch line and vice versa.

**245** The following statistics should be maintained from year to year in respect of all new lines opened for traffic and submitted to the Railway Board by 1st August of each year :-

- (i) (a) Passenger earnings from traffic local to the branch line.
- (b) Other coaching earnings from traffic local to the branch line.
- (ii) (a) Passenger earnings from traffic from the new line to the existing lines and vice versa.
- (b) Other coaching earnings from traffic from the new line to the existing lines and vice versa.
- (iii) (a) Tonnage of goods traffic local to the branch line.
- (b) Tonnage of goods traffic inter-changed with the existing lines
- (iv) (a) Earnings from goods traffic local to the branch line.
- (b) Earnings from goods traffic interchanged with the existing lines.

**246** The following instructions should be followed in preparing the statement F-244 :-

(i) Column 3 should indicate the earnings of the branch from all traffic originating therein, whether local or foreign (Proportion due to the branch) and all traffic received from the main line.

(ii) Columns 4 & 5 should be worked out on the basis of the costing/financial data under Group 'C'([see Annexure 'A'](#)) in respect of the traffic referred to in (i) above.

(iii) The additional or new traffic interchanged to be shown in column 6 should include only that portion of the traffic received by the main line from the new branch and of the traffic from the main line to the branch, which arises solely from the construction of the new branch line. In the absence of actual figures of additional traffic interchanged with the existing lines, a reasonably approximate figure may be adopted. In the case of chord line short-circuiting a previously existing route, figures relating to cross traffic which would have been carried by the previously existing route, if the chord line had not been constructed, may be omitted from this statement and a proportionate reduction in the working expenses on the branch line made. Column 7 should be worked out on the basis of costing financial data under group 'C' ([See Annexure 'A'](#) and [para 217](#)).

**247** The statements vide Paras [244](#) & [245](#) should be submitted for every completed financial year after the date of opening of the new line for a period of 11 years. The actuals for the years to end of which accounts have been closed and the cash flows for the remaining years of the assumed project life should be arrived at on the basis of the best possible estimation. The entire series of net cash flows should then be discounted to arrive at the rate of return compared to the originally expected return. In case the actual cash flows shown in statement F.244 indicate a fair degree of proximity to the original estimates, it may be assumed that the cash flows for the remaining years of the project life will also follow the same trend unless definite foreknowledge is available to the contrary. If a review of the annual cash flows for a sufficiently long period (say 5 to 7 years) indicates that the cash flows have settled down, within limits, to a 'uniform' series, the Railway Board may decide that submission of the Statements F. 244 & F. 245 for future years in the case of a particular new line be discontinued.

**248 Open Line Works** - For the purpose of applying the productivity tests to open line works, i. e. works undertaken with the definite object of increasing earnings or reducing expenditure and to which such tests can be applied within five to seven years of their completion, selection will be made out of these works sanctioned (and/or charged to Capital) on grounds of remunerativeness. All such works costing over Rs. 1 crore will invariably be subjected to this test. The result of the test should be reported by the General Managers to the Railway Board. In the case of works costing between Rs. 20 lakhs and Rs.1 crore charged to Capital and sanctioned by the General Manager within his powers 'of sanction, selection for the purpose of productivity test will be made by him in consultation with his Financial Adviser and Chief Accounts Officer. As stated earlier in the preceding para in the case of New Lines, the actual net cash inflow for each year, to end of the 5<sup>th</sup>/7<sup>th</sup> year from the date of commissioning should be recorded for each open line work to be subjected to the productivity test, and the cash flows for the rest of the project life assessed on the basis of the latest estimate. The whole series of net cash flow should then be discounted to arrive at the rate of return compared to the return originally expected.

**249** In addition to productivity test to be conducted as provided in [paragraph 248](#) above, a productivity review should also be undertaken in respect of selected works costing over Rs.10 lakhs which are estimated to fetch some return, even though not the return prescribed for a work being classified as remunerative and as such charged to O. L. W. R. or Development Fund. The methodology to be followed will be the same as prescribed in the preceding para in respect of works costing over Rs.1 crore each. The Railway Board will be selecting works which are sanctioned by them. The selection made by the Railway Board out of such works sanctioned by them will be notified through letters conveying sanction to the estimates for such works. For works costing over Rs. 10 lakhs and upto Rs. 1 crore each, sanctioned by the General Manager within his own powers of sanction, selection for the purpose of productivity review will be made by him in consultation with his Financial Adviser and Chief Accounts officer.

Note.-Justification for works or part of a scheme should show the probable period, that will elapse between the completion of the works and the time when the productivity review can be made. This note equally applies to paragraph 248.

**250** The fact that productivity tests are to be applied to a particular work should be intimated to the authorities entrusted with its execution as also to the Accounts and Audit officers. In respect of all such

selected works, the Financial Adviser and Chief Accounts Officer should keep such statistics as would be necessary for the application of the tests, in addition to those usually available.

**251** In order to ensure that a work selected either by the Railway Board or by the General Manager for the application of productivity tests or review is not lost sight of, Railway Administrations and Accounts Officers should maintain a register containing a list showing the following particulars :-

- (i) Reference to sanction of the estimate.
- (ii) Brief particulars of work selected for the application of productivity tests or review.
- (iii) Total estimated expenditure.
- (iv) Nature and extent of "productivity" claimed in the estimate.
- (v) When the test or review is to be applied.
- (vi) Brief remarks about the results of the test or review.

This list should be reviewed half-yearly and timely action taken to apply the test or review to all works due for examination during each half-year.

**252** When, in due course, the tests or reviews are actually applied or carried out, the Financial Adviser and Chief Accounts Officer should submit a report embodying the results of the test or review to the General Manager. In the case of works selected by the Railway Board, the General Manager will submit the Financial Adviser and Chief Accounts Officer's report to the Railway Board with his own comments. The object of these reports is not only to furnish information as to the results actually achieved to the authority who sanctioned the expenditure but also to serve as a lesson for the future.

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**ANNEXURE 'A'**  
(Ref. [paras 216](#) and [217](#))

**CHECK LIST WITH DETAILED NOTES FOR GUIDANCE OF ZONAL RAILWAYS AND  
CONCERNED BRANCHES IN RAILWAY BOARD'S OFFICE, IN THE PREPARATION OF  
PROJECT ESTIMATES**

The procedures and methodology to be adopted for a proper financial appraisal of projects are laid down in the Engineering Code and in the Report of the Committee on Technique of Financial Appraisal of Railway Projects as well as the circulars issued by the Railway Board from time to time.

2. Some of the survey reports submitted by the Zonal Railways were scrutinised by the Cost Analysis Cell of the Board's office. It was found that the estimates of working expenses have been substantially understated owing to many important elements such as empty haulage, number of marshallings, tare tonne kilometres, etc., not having been taken into account by the Zonal Railways. In some cases, instead of applying the unit costs the Railways have adopted the operating ratio to estimate the working expenses. The operating ratio is only an end figure and should not, therefore, be used for estimating working expenses. Further, the revenues depend on the product mix, i. e., the proportion of the high-rated, low-rated commodities or short lead or long-lead traffic and the estimate made thereof should be reasonably correct.

3. In order to ensure that no item of cost is excluded and no item of cost is over stated / understated, a check list, together with detailed notes, has been prepared for the guidance of the Zonal Railways and the concerned staff of the Railway Board's office (E.A. Branch F (X) Branch and Planning Branch). The more common mistakes and deficiencies noted in the calculations at present can be avoided if the check list is adhered to.

4. Unit costs are worked out for the broad and metre gauge systems of each of the Zonal Railways under 3 main groups-

*Group 'A'* – Gives the unit costs applicable for all- traction movement. These unit costs include the direct costs as well as the element of overheads.

*Group 'B'* - Gives unit costs for particular facets, as cost per shunting engine hour, train engine hour, engine hour etc., for each traction. The unit costs in this group include the element of overheads.

*Group 'C'*- Gives unit costs traction-wise. The wagon provision costs which include the element of repairs and maintenance, interest and depreciation, are separately shown. The overheads and the central charges are separately indicated.

Unit costs of line haul are worked out separately for through trains and van and shunting trains under both groups 'A' and 'C'.

All the unit costs are furnished separately under 3 heads - Working Expenses, Depreciation and Interest, so that the rate of return can be worked out both under the conventional method or D.C.F. technique.

Group 'A' and Group 'C' costs are more widely used for assessing the costs of specific flows or streams of traffic. If the traction is known, the Group 'C' costs are adopted. If the traction of line haul is not defined or specific, then all-traction figures in Group 'A' are adopted. Group 'C' costs are much more refined and specific and, therefore, by taking note of special characteristics of operation the costs may be estimated with a higher degree of accuracy. Group 'B' costs are generally used for estimating the savings in monetary terms of engine hours, wagon hours and shunting engine hours.

5. A study has been made to estimate broadly the variability of different items of expenditure with appropriate units of performance. The results of the study are summarised at the end of this Annexure.

6. In estimating the expenditure in respect of additional traffic the variability factors mentioned above should be adopted to arrive at the long- term variable costs. In estimating the expenditure in respect of existing traffic, however, the fully distributed cost should be used.

7. **Check list** -The check list and procedures/steps for estimating the costs are detailed below :-

|                                    |   | Existing line    |                    | Project line     |                    |
|------------------------------------|---|------------------|--------------------|------------------|--------------------|
|                                    |   | Existing traffic | Additional traffic | Existing traffic | Additional traffic |
| <b>Freight Traffic-</b>            |   |                  |                    |                  |                    |
| (a)                                | Tonnage loaded under specific commodities   |                  |                    |                  |                    |
| (b)                                | Tonnage unloaded under specific commodities |                  |                    |                  |                    |
| (c)                                | Tonnage transhipped                         |                  |                    |                  |                    |
| (d)                                | Tonnage repacked                            |                  |                    |                  |                    |
| (e)                                | Tonnage of cross traffic                    |                  |                    |                  |                    |
| (f)                                | Load of specific traffic                    |                  |                    |                  |                    |
| (g)                                | Net tonne kilometres                        |                  |                    |                  |                    |
| (h)                                | Loaded wagon kms.                           |                  |                    |                  |                    |
| (i)                                | Empty wagon kms.                            |                  |                    |                  |                    |
| (j)                                | Tare tonne Kilometres                       |                  |                    |                  |                    |
| (k)                                | Gross tonne Kilometres                      |                  |                    |                  |                    |
| (l)                                | Engine Kilometres                           |                  |                    |                  |                    |
| (m)                                | Train Kilometres                            |                  |                    |                  |                    |
| (n)                                | No. and name of marshalling yards.          |                  |                    |                  |                    |
| (o)                                | No. and name of Repacking points.           |                  |                    |                  |                    |
| (p)                                | No. and name of Transshipment points        |                  |                    |                  |                    |
| <b>Coaching/Passenger traffic-</b> |   |                  |                    |                  |                    |
| a)                                 | No. of Passengers-                          |                  |                    |                  |                    |
|                                    | (i) Originating                             |                  |                    |                  |                    |
|                                    | (ii) incoming                               |                  |                    |                  |                    |
| b)                                 | Train Kilometres                            |                  |                    |                  |                    |
| c)                                 | Engine Kilometres                           |                  |                    |                  |                    |
| d)                                 | Vehicle Kilometres.                         |                  |                    |                  |                    |

8. The Traffic Survey Report should give in detail the quantum of existing freight traffic (originating, terminating, transhipped, cross, etc.) under Important commodity groups, the pattern of movement (origin and destination of the important flows), the quantum assessed, both in terms of tonnes and in terms of B.G. or M.G.4-wheeler wagons. The additional traffic should also be assessed in a similar fashion. In case any difficulty is experienced in converting the tonnes into wagons, the figures of average starting loads (separately for originating and transhipped traffic) shown in the monthly wagon loading statements may be adopted. Otherwise, the minimum weight condition as per goods tariff may be taken into account.

9. Empty haulage should be carefully calculated taking into account the outward and inward traffic commodity-wise and equipment-wise. The source of empties should also be indicated so that the empty haulage may be reasonably assessed. Otherwise, following norms may be adopted :-

|   |      |
|---|------|
| BFRs, Oil tanks, BOBs , BOI and Special types, etc. (B.G. and M.G.)                       | 100% |
| POL Traffic, iron ore traffic, industrial raw material to steel plants, etc.(B.G. & M.G.) | 100% |



|                         |      |
|-------------------------|------|
| Coal--Average B. G.     | 80 % |
| Other commodities -B.G. | 23 % |
| M. G. (including coal)  | 33 % |

The correct estimate of empty haulage is very essential as this element appears in the calculation of –

- (i) Wagon kilometres,
- (ii) Gross tonne kilometres,
- (iii) Engine kilometres,
- (iv) Train kilometres,
- (v) Wagon days,
- (vi) Engine days, and
- (vii) Number of marshalling yards.

**10. Marshalling yards.** --The survey report should specify the Inward, outward and cross traffic dealt with at different marshalling yards on the project line and the existing main line. This should be separately assessed for the existing traffic and the additional traffic. We should take into account not only the loaded journeys but also the empty journeys of wagons. In case traffic bypasses the marshalling yard, detention to stock for carriage and wagons/train examination for engine changing and crew changing should be taken into account.

There are at least 2 marshalling yards for any movement irrespective of distance. The study reveals frequency of marshalling as indicated below:

|                | Broad Gauge | Metre Gauge |
|----------------|-------------|-------------|
| 1-40 Kms.      | 2.00        | 2.00        |
| 41-120 Kms.    | 3.00        | 3.00        |
| 121-240 Kms.   | 3.50        | 3.50        |
| 241-500 Kms.   | 4.00        | 4.00        |
| 501-800 Kms.   | 4.50        | 5.00        |
| 801-1300 Kms.  | 5.00        | 6.50        |
| 1301 and above | 5.50        | 7.50        |

The above is only for wagons moving in piece-meal. Where the wagons are moving in a specific stream of Traffic, the actual marshalling requirements should be assessed on the concerned route.

**11. Terminal:-** Documentation charges are calculated on the basis of one invoice per 4-wheeler wagon in the case of wagon load traffic and one invoice for 0.54 tonne of smalls traffic.

In the case of train load movement, one invoice may be adopted for 10 four-wheeler wagons.

There are cases under which one-end terminal documentation is performed by the staff employed by the consignee or the consignor. In those cases, this element of cost for one end may be omitted.

Two terminal costs should be taken, one for the originating end and the other for the destination end.

12. A special study has been made in the case of coal traffic. The coal terminal costs at the originating end for 1970-71 are given below :-

| Railway                      | Cost per wagon |  |             |                                  |
|------------------------------|----------------|--|-------------|----------------------------------|
|                              | Terminal Cost  | Trip haul between base yard and collieries | Other costs | Total originating Terminal costs |
|                              | Rs.            | Rs.  | Rs.         | Rs.                              |
| Central                      | 15.485         | 8.046                                      | 24.649      | 48.180                           |
| Eastern                      | 17.436         | 8.307                                      | 19.870      | 45.613                           |
| South Central                | 8.605          | 4.918                                      | 17.210      | 30.733                           |
| South Eastern                | 19.118         | 11.101                                     | 19.514      | 49.733                           |
| Total Indian Railways (B.G.) | 17.202         | 8.803                                      | 19.917      | 45.922                           |

At the destination end, the average unit costs would apply even in the case of coal traffic.

13. **Wagon days.** - It is not correct to adopt wagon kilometres per wagon day for assessing the wagon requirements. To illustrate this point, the example of a short distance traffic of lead of 40 kilometres with an empty return ratio of 100% may be considered. The wagon requirement on the basis of wagon kilometres per wagon day would work out to only one wagon day. It is common knowledge that it would take at least 3 days for the wagon to be loaded, unloaded and brought back to the loading point for the subsequent loading, if the detention to stock at the originating end, terminating end, transit time and contiguous marshalling yards were properly taken into account. In the case of fairly long-lead traffic, the wagon user index may be adopted.

14. **Engine kilometres** - After calculating the train kilometres on the basis of the permissible load (in terms of BOX or 4-wheelers and the gross load) on various sections, the engine kilometres should be assessed on the basis of --

- (i) Single engine operation or multiple engine operation,
- (ii) Banking engines over gradient sections; and
- (iii) Light engines.

Figures of engine kilometres per engine day used for goods traffic are readily available in the Annual Reports and Statistical Pamphlets for each traction. It should be possible to work out engine days required on this basis after giving due allowance for the element of repairs and spares.

For example, 4 million tonnes of iron ore are to be moved over a section 100 kms. in length. The movement will be in BOX wagons with load of 55 tonnes each. The section is heavily graded and the trains will run triple headed (diesel traction) with a load of 40 BOX's plus an additional banking engine over a section of 8 kms. Estimates of engine km/engine days will be as follows :-

|     |  |          |
|-----|--|----------|
| (1) | No. of trains each way                                       | 1,818    |
| (2) | Train kms. both ways with 100% empty return (1818 x 2 x 100) | 3,63,600 |
| (3) | Assisting required and Assisting not required Engine km.     | 7,27,200 |
| (4) | Banking engine kms. (1818 x 2 x 8)                           | 29,088   |
| (5) | Light engine kms. (say 6% of train kms.)                     | 21,816   |
|     |  | 1,41,704 |

|     |  |                       |
|-----|--|-----------------------|
| (6) | Bare-engine days required @ say 360 km. per engine day in use (goods). | 3172                  |
| (7) | Total engine days required (add 16% for POH, spares, etc.)             | 3680 or<br>10 engines |

The nature of movement should also be taken into account, i. e., whether the traffic is carried by shunting and van train or by through trains. The cost characteristics are different and separate unit costs are available.

**15.** Fuel and lubrication costs are calculated on the basis of GTKms.

Other operating costs (line haul) are calculated on the basis of train kilometres/engine kilometres.

**16. Track and signalling line haul** -This is calculated on the basis of GTKms. The average unit costs are not adopted for estimating the cost under track and signalling. A slight refinement is made taking into account the variability of this item of expenditure with reference to GTKms. The variability studies reveal that 50% of this expenditure is variable with GTKms. The average unit costs applicable to B.G. or M. G. systems of an individual Railway are adjusted by taking into account the specific density of traffic on the route or sections involved and the average density of the Zonal Railway system. As an illustration, a section with an average density of 18,000 tonnes per day as against the average density of 12,000 tonnes per day on the gauge may be considered. If the average unit cost for the gauge is Rs. 6.00 per 1000 GTKms., then the average unit cost for the section will be

$$= \text{Rs.}3 + \left[ \frac{\text{Rs.}3 \times 12000}{18000} \right] \text{ or Rs.}5 \text{ per } 1000\text{G.T.Kms.}$$

Particulars of Service for which unit costs of freight services are worked out on Indian Railways (See para 4 of Annexure A).

| Line No. | Particulars  |
|----------|--|
|          | <b>GROUP A</b>   |
| 1.       | Terminal Cost per Tonne-Small.   |
| 2.       | Terminal Cost per Tonne-Full Loads.  |
| 3.       | Total Terminal Cost per Wagon-Full Loads.  |
| 4.       | Repacking Cost of smalls per tonne per handling.                                 |
| 5.       | Transshipment Cost at Break of Gauge per tonne per transshipment.                |
| 6.       | Marshalling Cost per Wagon per yard handled.                                     |
| 7.       | Line Haul Cost -per train kilometre.   |
| 8.       | Line Haul Cost-per Wagon kilometre (Rev.)  |
| 9.       | Line Haul Cost-per net tonne kilometre (Pay Load).                               |
| 10.      | Line Haul Cost-per Wagon kilometre (Carrying Unit).<br>(i) Through Goods Trains. |
| 11.      | Line haul Cost per train Km.   |
| 12.      | Line haul Cost per Wagon Km. (Rev.)  |
| 13.      | Line haul Cost per NTKm (Pay Load).  |
| 14.      | Line haul Cost per Wagon Km. (Carrying units).<br>(ii) Van and Shunting Goods.   |

|                |  |  |
|----------------|--|--|
| 15.            | Line haul Cost per train Km.                                       |  |
| 16.            | Line haul Cost per Wagon Km. (Rev.)                                |  |
| 17.            | Line haul Cost per NTKm. (pay load).                               |  |
| 18.            | Line haul Cost per Wagon Km. (Carrying Units).                     |  |
| <b>GROUP B</b> |  |  |
| 19.            | Cost of Documentation per Invoice.                                 |  |
| 20.            | Cost of Traction per Engine Hour (Other than Shunting and Siding). | Steam (Total).                                     |
| 21.            | ” ” ” ” ” ”  | Diesel (Total).                                    |
| 22.            | ” ” ” ” ” ”  | Electric (Total).                                  |
| 23.            | ” ” ” ” ” ”  | Steam (Fuel, Water, Oil, Tallow and Stores).       |
| 24.            | ” ” ” ” ” ”  | Diesel (Fuel and stores)                           |
| 25.            | ” ” ” ” ” ”  | Electric (Electric current consumed)               |
| 26.            | Cost of Traction per Train Engine Hour.                            | Steam (Total).                                     |
| 27.            | ” ”  | Diesel (Total)                                     |
| 28.            | ” ”  | Electric (Total).                                  |
| 29.            | ” ”  | Steam (Fuel, Water, Oil, Tallow and Stores).       |
| 30.            | ” ”  | Diesel (Fuel and Stores).                          |
| 31.            | ” ”  | Electric (Electric current consumed).              |
| 32.            | Cost of Traction per 1000G.T.Kms..                                 | Steam (Total).                                     |
| 33.            | ” ”  | Diesel (Total)                                     |
| 34.            | ” ”  | Electric (Total).                                  |
| 35.            | ” ”  | Steam (Fuel, Water, Oil, Tallow and Stores).       |
| 36.            | Cost of Traction per 1000G.T.Kms..                                 | Diesel (Fuel and Stores).                          |
| 37.            | ” ”  | Electric (Electric current consumed).              |
| 38.            | Cost of Traction per Shunting Hour (Shunting Engines).             | Steam (Total).                                     |
| 39.            | ” ”  | Diesel (Total)                                     |
| 40.            | ” ”  | Electric (Total).                                  |
| 41.            | ” ”  | Steam (Fuel, Water, Oil, Tallow and Stores).       |
| 42.            | Cost of Traction per Shunting Hour (Shunting Engines).             | Diesel (Fuel and Stores).                          |
| 43.            | ” ”  | Electric (Electric current consumed).              |
| 44.            | Track and Signalling   | Provision and Maintenance Cost per train Kilometre |
| 45.            | ” ”  | Provision and Maintenance Cost per.1000 G.T Kms.   |

| Group C |   |   |   |   |   |   |   |           |  |
|---------|---|---|---|---|---|---|---|-----------|--|
| 46.     | Terminal Services-Cost of Documentation per Invoice.  |   |   |   |   |   |   |           |  |
| 47.     | Terminal Services-Cost of Handling per tonne.   |   |   |   |   |   |   |           |  |
| 48.     | Terminal Services-Cost of other Terminal Services per tonne-Small.  |   |   |   |   |   |   |           |  |
| 49.     | Terminal Services-Cost of other Terminal Services per tonne-Full Loads.   |   |   |   |   |   |   |           |  |
| 50.     | Terminal Services-Cost of other Terminal Services per wagon (Full Loads).   |   |   |   |   |   |   |           |  |
| 51.     | Cost of Repacking of Small per tonne per handling.  |   |   |   |   |   |   |           |  |
| 52.     | Cost of Transhipment at Break. of Gauge per tonne per Transhipment.   |   |   |   |   |   |   |           |  |
| 53.     | Cost of Marshalling per Wagon per yard handled.   |   |   |   |   |   |   |           |  |
| 54.     | Carrying Units-Provision and Maintenance per wagon day.   |   |   |   |   |   |   |           |  |
| 55.     | Line Haul (Movement) Service-Traction Cost- Steam<br>per 1000 G. T. Kms.  |   |   |   |   |   |   |           |  |
| 56.     | ”   | ” | ” | ” | ” | ” | ” | Diesel.   |  |
| 57.     | ”   | ” | ” | ” | ” | ” | ” | Electric. |  |
| 58.     | Line Haul (Movement) Service-Other Transportation expenses including Train Passing Staff<br>per Train kilometre.    |   |   |   |   |   |   |           |  |
| 59.     | Line Haul (Movement) Service-Other Transportation Expenses including Train Passing Staff<br>per 1000 G. T. Kms.     |   |   |   |   |   |   |           |  |
| 60.     | Line Haul (Movement) Service-Cost of Track and Signalling per train kilometre.                                      |   |   |   |   |   |   |           |  |
| 61.     | Line Haul (Movement) Service-Cost of Track and signalling per 1000 G. T. Kms.                                       |   |   |   |   |   |   |           |  |
| 62.     | General Overhead Charges-Percentage of Direct Costs.  |   |   |   |   |   |   |           |  |
| 63.     | Central Charges (Cost of Railway Board, Audit etc.)- Percentage of the total expenses.<br>(i) Through Goods Trains. |   |   |   |   |   |   |           |  |
| 64.     | Cost of traction per 1000 G. T. Km. (Diesel).   |   |   |   |   |   |   |           |  |
| 65.     | Cost of Traction per 1000 G. T. Km. (Steam).  |   |   |   |   |   |   |           |  |
| 66.     | Cost of Traction per 1000 G. T. Km. (Electric).   |   |   |   |   |   |   |           |  |
| 67.     | Other Transportation Expenses per 1000 G. T. Km.<br>(ii) Van and Shunting Goods.                                    |   |   |   |   |   |   |           |  |
| 68.     | Cost of Traction per 1000 G. T. Km. (Steam).  |   |   |   |   |   |   |           |  |
| 69.     | Cost of Traction per 1000 G. T. Km. (Diesel).   |   |   |   |   |   |   |           |  |
| 70.     | Cost of Traction per 1000 G. T. Km. (Electric).   |   |   |   |   |   |   |           |  |
| 71.     | Other Transportation Expenses per 1000 G.T.Km.  |   |   |   |   |   |   |           |  |

| Percentage of 'variable costs' to total costs average-all Railways. |                           |              |     |          |         |              |     |           |          |
|---|---------------------------|--------------|-----|----------|---------|--------------|-----|-----------|----------|
| S. No.  | Facets of operation       | BROAD GAUGE  |     |          |         | METER GAUGE  |     |           |          |
|   |                           | Working exp. | DRF | Interest | Overall | Working exp. | DRF | Inter-est | Over-all |
|   | (i) For cost in group A - |              |     |          |         |              |     |           |          |
| 1.  | Terminal                  | 76           | 75  | 77       | 76      | 75           | 70  | 70        | 74       |
| 2.  | Marshalling               | 74           | 83  | 85       | 78      | 74           | 80  | 80        | 77       |

|    |                                       |     |     |     |     |     |     |     |     |
|----|---------------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|
| 3. | Transshipment at break-of-gauge point | 80  | 70  | 74  | 79  | 80  | 70  | 74  | 79  |
| 4. | Repacking of Smalls                   | 84  | 70  | 74  | 82  | 79  | 70  | 70  | 78  |
| 5. | Line Haul-                            |     |     |     |     |     |     |     |     |
|    | (a) Pay load                          | 74  | 46  | 50  | 67  | 73  | 45  | 45  | 67  |
|    | (b) Carrying Unit                     | 72  | 70  | 72  | 72  | 61  | 65  | 70  | 62  |
|    | (ii) For costs in Group 'C<br>-@      |     |     |     |     |     |     |     |     |
| 1. | Terminal                              | 87  | 50  | 50  | 80  | 85  | 50  | 50  | 80  |
| 2. | Marshalling                           | 88  | 55  | 55  | 80  | 85  | 50  | 60  | 80  |
| 3. | Transshipment at break of gauge point | 91  | 55  | 57  | 86  | 91  | 55  | 57  | 86  |
| 4. | Repacking of small                    | 91  | 54  | 60  | 87  | 90  | 50  | 55  | 85  |
| 5. | Line Haul---                          |     |     |     |     |     |     |     |     |
|    | (i) Traction :                        |     |     |     |     |     |     |     |     |
|    | (a) Steam                             | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
|    | (b) Diesel                            | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
|    | (c ) Electric*                        | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
|    | (ii) Other Transportation             | 85  | 45  | 45  | 70  | 85  | 45  | 45  | 77  |
|    | (iii) Tracks Signalling               | 90  | 45  | 45  | 47  | 48  | 45  | 45  | 47  |

|    |   |
|----|---|
| @- | (1) Variability factors indicated for different facets of operation in Group Care exclusive of costs of provision and maintenance of wagons. The variability for provision and maintenance of wagons is 100% for D.R.F. and interest charge for both B.G. & M. G. |
|    | (2) Variability factors for overhead expenses will be in the ratio of constant and variable expenses as worked out about to the total expenses under these heads.   |
|    | (3) For a quick and broad analysis, a variability of 78.5% may be taken as representing working expenses.   |
|    | * The variability factor relates to total cost including cost on overhead equipment.  |

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| ANNEXURE 'B'                     |        |        |        |        |        |        |        |        |        |        |        |        |        |
|----------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| SINKING FUND PAYMENT TABLE       |        |        |        |        |        |        |        |        |        |        |        |        |        |
| N-Normal life of assets in years |        |        |        |        |        |        |        |        |        |        |        |        |        |
| N                                | 2%     | 2-1/2% | 3%     | 3-1/4% | 3-1/2% | 3-3/4% | 4%     | 4-1/4% | 4-1/2% | 5%     | 6%     | 7%     | 8%     |
| 1                                | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| 2                                | 0.4950 | 0.4938 | 0.4926 | 0.4920 | 0.4914 | 0.4908 | 0.4902 | 0.4896 | 0.4890 | 0.4878 | 0.4854 | 0.4831 | 0.4804 |
| 3                                | 0.3268 | 0.3251 | 0.3235 | 0.3227 | 0.3219 | 0.3211 | 0.3203 | 0.3196 | 0.3188 | 0.3172 | 0.3141 | 0.3111 | 0.3080 |
| 4                                | 0.2426 | 0.2408 | 0.2390 | 0.2381 | 0.2373 | 0.2364 | 0.2355 | 0.2346 | 0.2337 | 0.2320 | 0.2286 | 0.2252 | 0.2219 |
| 5                                | 0.1922 | 0.1902 | 0.1884 | 0.1874 | 0.1865 | 0.1856 | 0.1846 | 0.1837 | 0.1828 | 0.1810 | 0.1774 | 0.1739 | 0.1705 |
| 6                                | 0.1585 | 0.1565 | 0.1546 | 0.1536 | 0.1527 | 0.1517 | 0.1508 | 0.1498 | 0.1489 | 0.1470 | 0.1434 | 0.1398 | 0.1363 |
| 7                                | 0.1345 | 0.1325 | 0.1305 | 0.1295 | 0.1285 | 0.1276 | 0.1266 | 0.1257 | 0.1247 | 0.1228 | 0.1191 | 0.1156 | 0.1121 |
| 8                                | 0.1165 | 0.1145 | 0.1125 | 0.1115 | 0.1105 | 0.1095 | 0.1085 | 0.1076 | 0.1066 | 0.1047 | 0.1010 | 0.0975 | 0.0940 |
| 9                                | 0.1025 | 0.1005 | 0.0984 | 0.0974 | 0.0964 | 0.0955 | 0.0945 | 0.0935 | 0.0926 | 0.0907 | 0.0870 | 0.0835 | 0.0801 |

## ANNEXURE 'B'

**SINKING FUND PAYMENT TABLE**

N-Normal life of assets in years

| N  | 2%     | 2-1/2% | 3%     | 3-1/4% | 3-1/2% | 3-3/4% | 4%     | 4-1/4% | 4-1/2% | 5%     | 6%     | 7%     | 8%     |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 10 | 0.0913 | 0.0893 | 0.0872 | 0.0862 | 0.0852 | 0.0843 | 0.0833 | 0.0823 | 0.0814 | 0.0795 | 0.0759 | 0.0724 | 0.0690 |
| 11 | 0.0822 | 0.0801 | 0.0781 | 0.0771 | 0.0761 | 0.0751 | 0.0741 | 0.0732 | 0.0722 | 0.0704 | 0.0668 | 0.0634 | 0.0601 |
| 12 | 0.0746 | 0.0725 | 0.0705 | 0.0695 | 0.0685 | 0.0675 | 0.0666 | 0.0656 | 0.0647 | 0.0628 | 0.0593 | 0.0559 | 0.0527 |
| 13 | 0.0681 | 0.0660 | 0.0640 | 0.0630 | 0.0621 | 0.0611 | 0.0601 | 0.0592 | 0.0583 | 0.0565 | 0.0530 | 0.0497 | 0.0465 |
| 14 | 0.0626 | 0.0605 | 0.0585 | 0.0575 | 0.0566 | 0.0556 | 0.0547 | 0.0537 | 0.0528 | 0.0510 | 0.0476 | 0.0443 | 0.0413 |
| 15 | 0.0578 | 0.0558 | 0.0538 | 0.0528 | 0.0518 | 0.0509 | 0.0499 | 0.0490 | 0.0481 | 0.0463 | 0.0430 | 0.0398 | 0.0368 |
| 16 | 0.0537 | 0.0516 | 0.0496 | 0.0486 | 0.0477 | 0.0467 | 0.0458 | 0.0449 | 0.0440 | 0.0423 | 0.0390 | 0.0359 | 0.0330 |
| 17 | 0.0500 | 0.0479 | 0.0460 | 0.0450 | 0.0440 | 0.0431 | 0.0422 | 0.0413 | 0.0404 | 0.0387 | 0.0354 | 0.0324 | 0.0296 |
| 18 | 0.0467 | 0.0447 | 0.0427 | 0.0418 | 0.0408 | 0.0399 | 0.0390 | 0.0381 | 0.0372 | 0.0355 | 0.0324 | 0.0294 | 0.0267 |
| 19 | 0.0438 | 0.0418 | 0.0398 | 0.0389 | 0.0379 | 0.0370 | 0.0361 | 0.0353 | 0.0344 | 0.0327 | 0.0296 | 0.0268 | 0.0241 |
| 20 | 0.0412 | 0.0391 | 0.0372 | 0.0363 | 0.0354 | 0.0345 | 0.0336 | 0.0327 | 0.0319 | 0.0302 | 0.0272 | 0.0244 | 0.0219 |
| 21 | 0.0388 | 0.0368 | 0.0349 | 0.0339 | 0.0330 | 0.0321 | 0.0313 | 0.0304 | 0.0296 | 0.0280 | 0.0250 | 0.0223 | 0.0198 |
| 22 | 0.0366 | 0.0346 | 0.0327 | 0.0318 | 0.0309 | 0.0301 | 0.0292 | 0.0284 | 0.0275 | 0.0260 | 0.0230 | 0.0204 | 0.0180 |
| 23 | 0.0347 | 0.0327 | 0.0308 | 0.0299 | 0.0290 | 0.0282 | 0.0273 | 0.0265 | 0.0257 | 0.0241 | 0.0213 | 0.0187 | 0.0164 |
| 24 | 0.0329 | 0.0309 | 0.0290 | 0.0281 | 0.0273 | 0.0264 | 0.0256 | 0.0248 | 0.0240 | 0.0225 | 0.0197 | 0.0172 | 0.0150 |
| 25 | 0.0312 | 0.0293 | 0.0274 | 0.0265 | 0.0257 | 0.0248 | 0.0240 | 0.0232 | 0.0224 | 0.0210 | 0.0182 | 0.0158 | 0.0137 |
| 26 | 0.0297 | 0.0278 | 0.0259 | 0.0251 | 0.0242 | 0.0234 | 0.0226 | 0.0218 | 0.0210 | 0.0196 | 0.0169 | 0.0146 | 0.0125 |
| 27 | 0.0283 | 0.0264 | 0.0246 | 0.0237 | 0.0229 | 0.0220 | 0.0212 | 0.0205 | 0.0197 | 0.0183 | 0.0157 | 0.0134 | 0.0114 |
| 28 | 0.0270 | 0.0251 | 0.0233 | 0.0224 | 0.0216 | 0.0208 | 0.0200 | 0.0193 | 0.0185 | 0.0171 | 0.0149 | 0.0124 | 0.0105 |
| 29 | 0.0258 | 0.0239 | 0.0221 | 0.0213 | 0.0204 | 0.0197 | 0.0189 | 0.0181 | 0.0174 | 0.0160 | 0.0136 | 0.0114 | 0.0096 |
| 30 | 0.0246 | 0.0228 | 0.0210 | 0.0202 | 0.0194 | 0.0186 | 0.0178 | 0.0171 | 0.0164 | 0.0151 | 0.0126 | 0.0106 | 0.0088 |
| 31 | 0.0236 | 0.0217 | 0.0200 | 0.0192 | 0.0184 | 0.0176 | 0.0169 | 0.0161 | 0.0154 | 0.0141 | 0.0118 | 0.0098 | 0.0080 |
| 32 | 0.0226 | 0.0208 | 0.0190 | 0.0182 | 0.0174 | 0.0167 | 0.0159 | 0.0152 | 0.0146 | 0.0133 | 0.0110 | 0.0091 | 0.0075 |
| 33 | 0.0217 | 0.0199 | 0.0182 | 0.0173 | 0.0166 | 0.0158 | 0.0151 | 0.0144 | 0.0137 | 0.0125 | 0.0103 | 0.0084 | 0.0069 |
| 34 | 0.0208 | 0.0190 | 0.0173 | 0.0165 | 0.0158 | 0.0150 | 0.0143 | 0.0136 | 0.0130 | 0.0118 | 0.0096 | 0.0078 | 0.0063 |
| 35 | 0.0200 | 0.0182 | 0.0165 | 0.0158 | 0.0150 | 0.0143 | 0.0136 | 0.0129 | 0.0123 | 0.0111 | 0.0090 | 0.0072 | 0.0058 |
| 36 | 0.0192 | 0.0175 | 0.0158 | 0.0150 | 0.0143 | 0.0136 | 0.0129 | 0.0122 | 0.0116 | 0.0104 | 0.0084 | 0.0067 | 0.0053 |
| 37 | 0.0185 | 0.0167 | 0.0151 | 0.0143 | 0.0136 | 0.0129 | 0.0122 | 0.0116 | 0.0110 | 0.0098 | 0.0079 | 0.0062 | 0.0049 |
| 38 | 0.0178 | 0.0161 | 0.0145 | 0.0137 | 0.0130 | 0.0123 | 0.0116 | 0.0110 | 0.0104 | 0.0093 | 0.0074 | 0.0058 | 0.0045 |
| 39 | 0.0172 | 0.0154 | 0.0138 | 0.0131 | 0.0124 | 0.0117 | 0.0111 | 0.0104 | 0.0099 | 0.0088 | 0.0069 | 0.0054 | 0.0042 |
| 40 | 0.0166 | 0.0148 | 0.0133 | 0.0125 | 0.0118 | 0.0112 | 0.0105 | 0.0099 | 0.0093 | 0.0083 | 0.0065 | 0.0050 | 0.0039 |
| 41 | 0.0160 | 0.0143 | 0.0127 | 0.0120 | 0.0113 | 0.0106 | 0.0100 | 0.0094 | 0.0089 | 0.0078 | 0.0061 | 0.0047 | 0.0036 |
| 42 | 0.0154 | 0.0137 | 0.0122 | 0.0115 | 0.0108 | 0.0102 | 0.0095 | 0.0090 | 0.0084 | 0.0074 | 0.0057 | 0.0043 | 0.0033 |
| 43 | 0.0149 | 0.0132 | 0.0117 | 0.0110 | 0.0103 | 0.0097 | 0.0091 | 0.0085 | 0.0080 | 0.0070 | 0.0053 | 0.0040 | 0.0030 |
| 44 | 0.0144 | 0.0127 | 0.0112 | 0.0105 | 0.0099 | 0.0093 | 0.0087 | 0.0081 | 0.0076 | 0.0066 | 0.0050 | 0.0038 | 0.0028 |
| 45 | 0.0139 | 0.0123 | 0.0108 | 0.0101 | 0.0095 | 0.0088 | 0.0083 | 0.0077 | 0.0072 | 0.0063 | 0.0047 | 0.0035 | 0.0026 |
| 46 | 0.0135 | 0.0118 | 0.0104 | 0.0097 | 0.0091 | 0.0084 | 0.0079 | 0.0073 | 0.0068 | 0.0059 | 0.0044 | 0.0033 | 0.0024 |
| 47 | 0.0130 | 0.0114 | 0.0100 | 0.0093 | 0.0087 | 0.0081 | 0.0075 | 0.0070 | 0.0065 | 0.0056 | 0.0041 | 0.0030 | 0.0022 |
| 48 | 0.0126 | 0.0110 | 0.0096 | 0.0089 | 0.0083 | 0.0077 | 0.0072 | 0.0067 | 0.0062 | 0.0053 | 0.0039 | 0.0028 | 0.0002 |
| 49 | 0.0122 | 0.0106 | 0.0092 | 0.0086 | 0.0080 | 0.0074 | 0.0069 | 0.0064 | 0.0059 | 0.0050 | 0.0037 | 0.0026 | 0.0019 |
| 50 | 0.0118 | 0.0103 | 0.0089 | 0.0082 | 0.0076 | 0.0071 | 0.0066 | 0.0061 | 0.0056 | 0.0048 | 0.0034 | 0.0025 | 0.0017 |

| ANNEXURE 'B'                     |        |        |        |        |        |        |        |        |        |        |        |        |        |
|----------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| SINKING FUND PAYMENT TABLE       |        |        |        |        |        |        |        |        |        |        |        |        |        |
| N-Normal life of assets in years |        |        |        |        |        |        |        |        |        |        |        |        |        |
| N                                | 2%     | 2-1/2% | 3%     | 3-1/4% | 3-1/2% | 3-3/4% | 4%     | 4-1/4% | 4-1/2% | 5%     | 6%     | 7%     | 8%     |
| 55                               | 0.0101 | 0.0087 | 0.0073 | 0.0068 | 0.0062 | 0.0057 | 0.0052 | 0.0048 | 0.0044 | 0.0037 | 0.0025 | 0.0017 | 0.0001 |
| 60                               | 0.0088 | 0.0074 | 0.0061 | 0.0056 | 0.0051 | 0.0046 | 0.0042 | 0.0039 | 0.0035 | 0.0028 | 0.0019 | 0.0012 | 0.0008 |
| 65                               | 0.0076 | 0.0063 | 0.0051 | 0.0046 | 0.0042 | 0.0038 | 0.0034 | 0.0031 | 0.0027 | 0.0022 | 0.0014 | 0.0009 | 0.0005 |
| 70                               | 0.0067 | 0.0054 | 0.0043 | 0.0039 | 0.0035 | 0.0031 | 0.0027 | 0.0025 | 0.0022 | 0.0017 | 0.0010 | 0.0006 | 0.0004 |
| 75                               | 0.0059 | 0.0047 | 0.0037 | 0.0032 | 0.0029 | 0.0025 | 0.0022 | 0.0020 | 0.0017 | 0.0013 | 0.0008 | 0.0004 | 0.0002 |
| 80                               | 0.0025 | 0.0040 | 0.0031 | 0.0027 | 0.0024 | 0.0021 | 0.0018 | 0.0016 | 0.0014 | 0.0010 | 0.0006 | 0.0003 | 0.0002 |
| 85                               | 0.0046 | 0.0036 | 0.0026 | 0.0023 | 0.0020 | 0.0017 | 0.0015 | 0.0013 | 0.0011 | 0.0008 | 0.0004 | 0.0002 | 0.0001 |
| 90                               | 0.0040 | 0.0030 | 0.0023 | 0.0019 | 0.0017 | 0.0014 | 0.0012 | 0.0011 | 0.0009 | 0.0006 | 0.0003 | 0.0002 | 0.0001 |
| 95                               | 0.0036 | 0.0026 | 0.0019 | 0.0016 | 0.0014 | 0.0012 | 0.0010 | 0.0009 | 0.0007 | 0.0005 | 0.0002 | 0.0001 | 0.0000 |
| 100                              | 0.0032 | 0.0023 | 0.0016 | 0.0014 | 0.0012 | 0.0010 | 0.0008 | 0.0007 | 0.0006 | 0.0004 | 0.0002 | 0.0001 | 0.0000 |
| N                                | 2%     | 2-1/2% | 3%     | 3-1/4% | 3-1/2% | 3-3/4% | 4%     | 4-1/4% | 4-1/2% | 5%     | 6%     | 7%     | 8%     |
| 41                               | 0.0160 | 0.0143 | 0.0127 | 0.0120 | 0.0113 | 0.0106 | 0.0100 | 0.0094 | 0.0089 | 0.0078 | 0.0061 | 0.0047 | 0.0036 |
| 42                               | 0.0154 | 0.0137 | 0.0122 | 0.0115 | 0.0108 | 0.0102 | 0.0095 | 0.0090 | 0.0084 | 0.0074 | 0.0057 | 0.0043 | 0.0033 |
| 43                               | 0.0149 | 0.0132 | 0.0117 | 0.0110 | 0.0103 | 0.0097 | 0.0091 | 0.0085 | 0.0080 | 0.0070 | 0.0053 | 0.0040 | 0.0030 |
| 44                               | 0.0144 | 0.0127 | 0.0112 | 0.0105 | 0.0099 | 0.0093 | 0.0087 | 0.0081 | 0.0076 | 0.0066 | 0.0050 | 0.0038 | 0.0028 |
| 45                               | 0.0139 | 0.0123 | 0.0108 | 0.0101 | 0.0095 | 0.0088 | 0.0083 | 0.0077 | 0.0072 | 0.0063 | 0.0047 | 0.0035 | 0.0026 |
| 46                               | 0.0135 | 0.0118 | 0.0104 | 0.0097 | 0.0091 | 0.0084 | 0.0079 | 0.0073 | 0.0068 | 0.0059 | 0.0044 | 0.0033 | 0.0024 |
| 47                               | 0.0130 | 0.0114 | 0.0100 | 0.0093 | 0.0087 | 0.0081 | 0.0075 | 0.0700 | 0.0065 | 0.0056 | 0.0041 | 0.0030 | 0.0022 |
| 48                               | 0.0126 | 0.0110 | 0.0096 | 0.0089 | 0.0083 | 0.0077 | 0.0072 | 0.0067 | 0.0062 | 0.0053 | 0.0039 | 0.0028 | 0.0002 |
| 49                               | 0.0122 | 0.0106 | 0.0092 | 0.0086 | 0.0080 | 0.0074 | 0.0069 | 0.0064 | 0.0059 | 0.0050 | 0.0037 | 0.0026 | 0.0019 |
| 50                               | 0.0118 | 0.0103 | 0.0089 | 0.0082 | 0.0076 | 0.0071 | 0.0066 | 0.0061 | 0.0056 | 0.0048 | 0.0034 | 0.0025 | 0.0017 |
| 55                               | 0.0101 | 0.0087 | 0.0073 | 0.0068 | 0.0062 | 0.0057 | 0.0052 | 0.0048 | 0.0044 | 0.0037 | 0.0025 | 0.0017 | 0.0001 |
| 60                               | 0.0088 | 0.0074 | 0.0061 | 0.0056 | 0.0051 | 0.0046 | 0.0042 | 0.0039 | 0.0035 | 0.0028 | 0.0019 | 0.0012 | 0.0008 |
| 65                               | 0.0076 | 0.0063 | 0.0051 | 0.0046 | 0.0042 | 0.0038 | 0.0034 | 0.0031 | 0.0027 | 0.0022 | 0.0014 | 0.0009 | 0.0005 |
| 70                               | 0.0067 | 0.0054 | 0.0043 | 0.0039 | 0.0035 | 0.0031 | 0.0027 | 0.0025 | 0.0022 | 0.0017 | 0.0010 | 0.0006 | 0.0004 |
| 75                               | 0.0059 | 0.0047 | 0.0037 | 0.0032 | 0.0029 | 0.0025 | 0.0022 | 0.0020 | 0.0017 | 0.0013 | 0.0008 | 0.0004 | 0.0002 |
| 80                               | 0.0025 | 0.0040 | 0.0031 | 0.0027 | 0.0024 | 0.0021 | 0.0018 | 0.0016 | 0.0014 | 0.0010 | 0.0006 | 0.0003 | 0.0002 |
| 85                               | 0.0046 | 0.0036 | 0.0026 | 0.0023 | 0.0020 | 0.0017 | 0.0015 | 0.0013 | 0.0011 | 0.0008 | 0.0004 | 0.0002 | 0.0001 |
| 90                               | 0.0040 | 0.0030 | 0.0023 | 0.0019 | 0.0017 | 0.0014 | 0.0012 | 0.0011 | 0.0009 | 0.0006 | 0.0003 | 0.0002 | 0.0001 |
| 95                               | 0.0036 | 0.0026 | 0.0019 | 0.0016 | 0.0014 | 0.0012 | 0.0010 | 0.0009 | 0.0007 | 0.0005 | 0.0002 | 0.0001 | 0.0000 |
| 100                              | 0.0032 | 0.0023 | 0.0016 | 0.0014 | 0.0012 | 0.0010 | 0.0008 | 0.0007 | 0.0006 | 0.0004 | 0.0002 | 0.0001 | 0.0000 |

The use of the Table – What sum must be paid at the end of each year to Sinking Fund so that the annual payments together with interest therein at 4 per cent compound annually, will at the end of 18 years amount to Rs.2,000/-

Opposite 18 under 4 per cent we find 0.390 which is the annual payment required for Re.1/- so for Rs. 2,000 the annual payment is 2,000 x 0.390 i.e. 78/-

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**ANNEXURE 'C'**  
[\(See Para 227\)](#)  
**INTEREST FORMULAS AND TABLES FOR DISCOUNTED**  
**FLOW TECHNIQUES**

**CASH**

**Interest Formulas**

The interest formula and tables that follow may be found of considerable use in evaluating the financial aspects of Engineering projects.

Symbols:- The symbols used in these formulas and Tables are:

- i represent rate of interest per interest period.
- n represent number of interest periods
- p represent sum of money
- S - do - sum of money that is equivalent to p with interest i, at the end of n
- R - do - the end of period payments/receipt in a uniform series continuing for the coming n periods, the entire series equivalent to p at interest rate i.

**Formulas :-** The interest formulas expressing the relationship between P, S and R in terms of i and n are :-

$$\text{Given P, to find S} \quad S = P (1 + i)^n \quad (1)$$

$$\text{Given S, to find P} \quad P = S \left( \frac{1}{(1 + i)^n} \right) \quad (2)$$

$$\text{Given S, to find R} \quad R = S \left( \frac{1}{(1 + i)^{n-1}} \right) \quad (3)$$

$$\text{Given P, to find R} \quad R = P \left( \frac{i(1 + i)^n}{(1 + i)^{n-1}} \right) \quad (4)$$

$$\text{Given R, to find S} \quad S = R \left( \frac{(1 + i)^{n-1}}{i} \right) \quad (5)$$

$$\text{Given R, to find P} \quad P = R \left( \frac{(1 + i)^{n-1}}{i(1 + i)^n} \right) \quad (6)$$

In the following explanations of these formulas the interest period is taken as one year; the explanations can be made general by substituting "Period" for "year"

**Development of Formulas for Single Payment-** If P is invested at interest rate i, the interest for the first year is iP and the total amount at the end of the first year is P(1+i).

The second year the interest on this is iP(1+i), and the amount at the end of this year is P(1+i)+iP(1+i) = P(1+i)<sup>2</sup>. Similarly at the end of the third year the amount is P(1+i)<sup>3</sup>; at the end of n years it is P(1+i)<sup>n</sup>.

This is the formula for the compound amount, S, obtainable in n years from a principal, P.

$$S = P (1 + i)^n \quad (1)$$

If we express P in terms of S, i and n

$$P = S \left( \frac{1}{(1+i)^n} \right) \quad (2)$$

P may then be thought of as the principal that will give a required amount S in n years; in other words, P is the present worth of a payment S, n years hence.

The expression  $(1+i)^n$  is called the single payment compound amount factor (denoted as cu'). Its reciprocal  $1/(1+i)^n$  is called the single payment present worth factor (denoted as pwf.)

**Formulas for Uniform Annual Series of End-of Year Payments.** - If R is invested at the end of each year for n years, the total amount at the end of n years will be the sum of the compound amounts of the individual investments. The money invested at the end of the first year will earn interest for (n-1) years; its amount will thus be  $R(1+i)^{n-1}$ . The second years payment will amount to  $R(1+i)^{n-2}$ ; the third years to  $R(1+i)^{n-3}$ ; and so on until the last payment, made at the end of n years which has earned no interest. The total sum S is then given by the expression-

$$S = R[(1+i) + (1+i)^2 + \dots + (1+i)^{n-2} + (1+i)^{n-1}] \quad (i)$$

To simplify, multiply both sides of the equation by (1+i),

$$(1+i)S = R[(1+i) + (1+i)^2 + (1+i)^3 + \dots + (1+i)^{n-1} + (1+i)^n] \quad (ii)$$

Subtracting (i) from (ii)

$$iS = R[(1+i)^{n-1}]$$

$$\text{or } S = R \left( \frac{(1+i)^{n-1}}{i} \right)$$

$$\text{And } R = S \left( \frac{i}{(1+i)^{n-1}} \right) \quad (3)$$

A fund established to produce a desired amount at the end of a given period of time by means of a series of payments through out the period is called a sinking fund. The expression—

$$\frac{1}{(1+i)^{n-1}}$$

is called the sinking fund deposit factor (denoted as sff).

To find the uniform end-of year payment, R which can be secured for n years from a present investment P, substitute In equation (3) the value given for S in equation (I)

$$R = S \left( \frac{i}{(1+i)^{n-1}} \right) = P(1+i)^n \left( \frac{i}{(1+i)^{n-1}} \right)$$

$$\text{or } R=P \left( \frac{i(1+i)^n}{(1+i)^{n-1}} \right) \quad (4)$$

The expression—

$$- \frac{i(1+i)^n}{(1+i)^{n-1}}$$

is called the capital recovery factor (denoted as crf).

When multiplied by a present debt (which, from the point of the lender, is a present investment,) it gives the uniform end-of-year payment necessary to repay the debit (the lender's investment) in n years with interest rate i.

Formulas (3) and (4) may be reversed to show S and P in terms of R as follows:

$$S=R \left( \frac{(1+i)^n}{i} \right) \quad (5)$$

$$P=R \left( \frac{(1+i)^{n-1}}{i(1+i)^n} \right) \quad (6)$$

$$\text{The expression—} \left( \frac{(1+i)^{n-1}}{i} \right)$$

is called the uniform series compound amount factor (denoted as caf)

$$\text{The expression} \left( \frac{(1+i)^{n-1}}{i(1+i)^n} \right)$$

is called the uniform series present worth factor (denoted as pwf).

**TABLES 1 TO 19** Give values of the single payment compound amount factor, single payment present worth factor, the sinking fund deposit factor, the capital recovery factor, the uniform series compound amount factor, and the uniform series present worth factor for each value of n from 1 to 35, and for values of n that are multiples of 5 from 40 to 100. Each interest rate has a separate table; the interest rates given are 1%, 1-1/4%, 1-1/2%, 1-3/4%, 2%, 2-1/2%, 3%, 3-1/2%, 4%, 4-1/2%, 5%, 5-1/2%, 6%, 7%, 8%, 10%, 12%, 15%, and 20%. In addition,

**TABLES 20 TO 22** give the capital recovery factors, single payment present worth factors, and series present worth factors for interest rates from 25% to 50%.

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Table 1 - 22

Table-1

| Table -1<br>ANNEXURE 'C'—(Contd.)<br>Interest Tables |                                    |  |  |   |  |   |
|--|------------------------------------|--|--|---|--|---|
| 1% Compound Interest Factors                         |                                    |  |  |   |  |   |
|  | Single Payment                     |  | Uniform Series                                 |   |  |   |
|  | Compound Amount Factor $caf'$      | Present Worth Factor $pwf'$                  | Sinking Fund Factor $sf'$                      | Capital Recovery Factor $crf'$                        | Compound Amount Factor $caf'$                  | Present Worth Factor $pwf'$                       |
|  | Given $P$ To find $S$<br>$(1+i)^n$ | Given $S$ To find $P$<br>$\frac{1}{(1+i)^n}$ | Given $S$ To find $R$<br>$\frac{i}{(1+i)^n-1}$ | Given $P$ To find $R$<br>$\frac{i(1+i)^n}{(1+i)^n-1}$ | Given $R$ To find $S$<br>$\frac{(1+i)^n-1}{i}$ | Given $R$ To find $P$<br>$\frac{1-(1+i)^{-n}}{i}$ |
| 1  | 1.010                              | 0.9901                                       | 1.00000  | 1.01000   | 1.000  | 0.990   |
| 2  | 1.020                              | 0.9803                                       | 0.49751  | 0.50751   | 2.010  | 1.970   |
| 3  | 1.030                              | 0.9706                                       | 0.33002  | 0.34002   | 3.030  | 2.941   |
| 4  | 1.041                              | 0.9610                                       | 0.24628  | 0.25628   | 4.060  | 3.902   |
| 5  | 1.051                              | 0.9515                                       | 0.19604  | 0.20604   | 5.101  | 4.853   |
| 6  | 1.062                              | 0.9420                                       | 0.16255  | 0.17255   | 6.152  | 5.795   |
| 7  | 1.072                              | 0.9327                                       | 0.13863  | 0.14863   | 7.214  | 6.728   |
| 8  | 1.083                              | 0.9235                                       | 0.12069  | 0.13069   | 8.286  | 7.652   |
| 9  | 1.094                              | 0.9143                                       | 0.10674  | 0.11674   | 9.369  | 8.566   |
| 10   | 1.105                              | 0.9053                                       | 0.09558  | 0.10558   | 10.463   | 9.471   |
| 11   | 1.116                              | 0.8963                                       | 0.08645  | 0.09645   | 11.567   | 10.368  |
| 12   | 1.127                              | 0.8874                                       | 0.07885  | 0.08885   | 12.682   | 11.255  |
| 13   | 1.138                              | 0.8787                                       | 0.07241  | 0.08241   | 13.809   | 12.134  |
| 14   | 1.149                              | 0.8700                                       | 0.06690  | 0.07690   | 14.947   | 13.004  |
| 15   | 1.161                              | 0.8613                                       | 0.06212  | 0.07212   | 16.097   | 13.865  |
| 16   | 1.173                              | 0.8528                                       | 0.05794  | 0.06794   | 17.258   | 14.718  |
| 17   | 1.184                              | 0.8444                                       | 0.05426  | 0.06426   | 18.430   | 15.562  |
| 18   | 1.196                              | 0.8360                                       | 0.05098  | 0.06098   | 19.615   | 16.398  |
| 19   | 1.208                              | 0.8277                                       | 0.04805  | 0.05805   | 20.811   | 17.226  |
| 20   | 1.220                              | 0.8195                                       | 0.04542  | 0.05542   | 22.019   | 18.046  |
| 21   | 1.232                              | 0.8114                                       | 0.04303  | 0.05303   | 23.239   | 18.857  |
| 22   | 1.245                              | 0.8034                                       | 0.04086  | 0.05086   | 24.472   | 19.660  |
| 23   | 1.257                              | 0.7954                                       | 0.03889  | 0.04889   | 25.716   | 20.456  |
| 24   | 1.270                              | 0.7876                                       | 0.03707  | 0.04707   | 26.973   | 21.243  |
| 25   | 1.282                              | 0.7798                                       | 0.03541  | 0.04541   | 28.243   | 22.023  |
| 26   | 1.295                              | 0.7720                                       | 0.03387  | 0.04387   | 29.526   | 22.795  |
| 27   | 1.308                              | 0.7644                                       | 0.03245  | 0.04245   | 30.821   | 23.560  |
| 28   | 1.321                              | 0.7568                                       | 0.03112  | 0.04112   | 32.129   | 24.316  |
| 29   | 1.335                              | 0.7493                                       | 0.02990  | 0.03990   | 33.450   | 25.065  |
| 30   | 1.348                              | 0.7419                                       | 0.02875  | 0.03875   | 34.785   | 25.808  |
| 31   | 1.361                              | 0.7346                                       | 0.02768  | 0.03768   | 36.133   | 26.542  |
| 32   | 1.375                              | 0.7273                                       | 0.02667  | 0.03667   | 37.494   | 27.270  |
| 33   | 1.389                              | 0.7201                                       | 0.02573  | 0.03573   | 38.869   | 27.990  |
| 34   | 1.403                              | 0.7130                                       | 0.02484  | 0.03484   | 40.258   | 28.703  |
| 35   | 1.417                              | 0.7059                                       | 0.02400  | 0.03400   | 41.660   | 29.409  |
| 40   | 1.469                              | 0.6717                                       | 0.02046  | 0.03046   | 48.085   | 32.835  |
| 45   | 1.565                              | 0.6371                                       | 0.01771  | 0.02771   | 56.481   | 36.095  |
| 50   | 1.645                              | 0.6080                                       | 0.01551  | 0.02551   | 64.463   | 39.196  |
| 55   | 1.729                              | 0.5785                                       | 0.01373  | 0.02373   | 72.852   | 42.147  |
| 60   | 1.817                              | 0.5504                                       | 0.12224  | 0.02224   | 81.670   | 44.955  |
| 65   | 1.909                              | 0.5237                                       | 0.01100  | 0.02100   | 90.937   | 47.637  |
| 70   | 2.007                              | 0.4983                                       | 0.00993  | 0.01993   | 100.676  | 50.169  |
| 75   | 2.109                              | 0.4741                                       | 0.00902  | 0.01902   | 110.913  | 52.587  |
| 80   | 2.217                              | 0.4511                                       | 0.00822  | 0.01822   | 121.672  | 54.888  |
| 85   | 2.330                              | 0.4292                                       | 0.00752  | 0.01752   | 132.979  | 57.079  |
| 90   | 2.447                              | 0.4084                                       | 0.00690  | 0.01690   | 144.863  | 59.161  |
| 95   | 2.574                              | 0.3886                                       | 0.00636  | 0.01636   | 157.354  | 61.143  |
| 100  | 2.705                              | 0.3697                                       | 0.00587  | 0.01587   | 170.481  | 63.029  |

Table - 2

ANNEXURE 'C'—(Contd.)

TABLE 2

1½% Compound Interest Factors

| n   | Single Payment                |                                       |   | Uniform Series                                 |   |  | n   |
|-----|-------------------------------|---------------------------------------|---|--|---|--|-----|
|     | Compound Amount Factor $cf^1$ | Present Worth Factor $pwf^1$          | Sinking Fund Factor $sf$                | Capital Recovery Factor $crf$                  | Compound Amount Factor $cf^2$           | Present Worth Factor $pwf^2$             |     |
|     | Given P To find S $(1+i)^n$   | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1}{i(1+i)^n-1}$ |     |
| 1   | 1.012                         | 0.9877                                | 1.00000                                 | 1.01250  | 1.000                                   | 0.988                                    | 1   |
| 2   | 1.025                         | 0.9755                                | 0.49689                                 | 0.50929  | 2.012                                   | 1.963                                    | 2   |
| 3   | 1.038                         | 0.9634                                | 0.32920                                 | 0.34170  | 3.038                                   | 2.927                                    | 3   |
| 4   | 1.051                         | 0.9515                                | 0.24536                                 | 0.25706  | 4.076                                   | 3.878                                    | 4   |
| 5   | 1.064                         | 0.9398                                | 0.19206                                 | 0.20756  | 5.127                                   | 4.818                                    | 5   |
| 6   | 1.077                         | 0.9282                                | 0.16153                                 | 0.17403  | 6.191                                   | 5.745                                    | 6   |
| 7   | 1.091                         | 0.9167                                | 0.13759                                 | 0.15099  | 7.268                                   | 6.663                                    | 7   |
| 8   | 1.104                         | 0.9054                                | 0.11963                                 | 0.13213  | 8.359                                   | 7.568                                    | 8   |
| 9   | 1.118                         | 0.8942                                | 0.10567                                 | 0.11817  | 9.463                                   | 8.462                                    | 9   |
| 10  | 1.132                         | 0.8832                                | 0.09450                                 | 0.10700  | 10.582                                  | 9.346                                    | 10  |
| 11  | 1.146                         | 0.8723                                | 0.08537                                 | 0.09787  | 11.714                                  | 10.218                                   | 11  |
| 12  | 1.161                         | 0.8615                                | 0.07776                                 | 0.09026  | 12.860                                  | 11.079                                   | 12  |
| 13  | 1.175                         | 0.8509                                | 0.07132                                 | 0.08382  | 14.021                                  | 11.930                                   | 13  |
| 14  | 1.190                         | 0.8404                                | 0.06581                                 | 0.07831  | 15.196                                  | 12.771                                   | 14  |
| 15  | 1.205                         | 0.8300                                | 0.06103                                 | 0.07353  | 16.386                                  | 13.601                                   | 15  |
| 16  | 1.220                         | 0.8197                                | 0.05685                                 | 0.06935  | 17.591                                  | 14.420                                   | 16  |
| 17  | 1.235                         | 0.8096                                | 0.05316                                 | 0.06566  | 18.811                                  | 15.230                                   | 17  |
| 18  | 1.251                         | 0.7996                                | 0.04988                                 | 0.06238  | 20.046                                  | 16.030                                   | 18  |
| 19  | 1.266                         | 0.7898                                | 0.04696                                 | 0.05946  | 21.297                                  | 16.819                                   | 19  |
| 20  | 1.282                         | 0.7800                                | 0.04432                                 | 0.05680  | 22.563                                  | 17.599                                   | 20  |
| 21  | 1.298                         | 0.7704                                | 0.04194                                 | 0.05444  | 23.845                                  | 18.370                                   | 21  |
| 22  | 1.314                         | 0.7609                                | 0.03977                                 | 0.05227  | 25.143                                  | 19.131                                   | 22  |
| 23  | 1.331                         | 0.7515                                | 0.03780                                 | 0.05030  | 26.457                                  | 19.882                                   | 23  |
| 24  | 1.347                         | 0.7422                                | 0.03599                                 | 0.04849  | 27.788                                  | 20.624                                   | 24  |
| 25  | 1.364                         | 0.7330                                | 0.03432                                 | 0.04682  | 29.135                                  | 21.357                                   | 25  |
| 26  | 1.381                         | 0.7240                                | 0.03279                                 | 0.04529  | 30.500                                  | 22.081                                   | 26  |
| 27  | 1.399                         | 0.7150                                | 0.03137                                 | 0.04387  | 31.881                                  | 22.796                                   | 27  |
| 28  | 1.416                         | 0.7062                                | 0.03005                                 | 0.04255  | 33.279                                  | 23.503                                   | 28  |
| 29  | 1.434                         | 0.6975                                | 0.02882                                 | 0.04132  | 34.695                                  | 24.200                                   | 29  |
| 30  | 1.452                         | 0.6889                                | 0.02768                                 | 0.04018  | 36.129                                  | 24.889                                   | 30  |
| 31  | 1.470                         | 0.6804                                | 0.02661                                 | 0.03911  | 37.581                                  | 25.569                                   | 31  |
| 32  | 1.488                         | 0.6720                                | 0.02561                                 | 0.03811  | 39.050                                  | 26.241                                   | 32  |
| 33  | 1.507                         | 0.6637                                | 0.02467                                 | 0.03717  | 40.539                                  | 26.905                                   | 33  |
| 34  | 1.526                         | 0.6555                                | 0.02378                                 | 0.03628  | 42.045                                  | 27.560                                   | 34  |
| 35  | 1.545                         | 0.6474                                | 0.02295                                 | 0.03545  | 43.571                                  | 28.208                                   | 35  |
| 40  | 1.644                         | 0.6084                                | 0.01942                                 | 0.03192  | 51.490                                  | 31.327                                   | 40  |
| 45  | 1.749                         | 0.5718                                | 0.01669                                 | 0.02919  | 59.916                                  | 34.350                                   | 45  |
| 50  | 1.861                         | 0.5373                                | 0.01452                                 | 0.02702  | 68.882                                  | 37.013                                   | 50  |
| 55  | 1.980                         | 0.5050                                | 0.01275                                 | 0.02525  | 78.422                                  | 39.602                                   | 55  |
| 60  | 2.107                         | 0.4746                                | 0.01129                                 | 0.02379  | 88.575                                  | 42.035                                   | 60  |
| 65  | 2.242                         | 0.4460                                | 0.01006                                 | 0.02256  | 99.377                                  | 44.321                                   | 65  |
| 70  | 2.386                         | 0.4191                                | 0.00902                                 | 0.02152  | 110.872                                 | 46.470                                   | 70  |
| 75  | 2.539                         | 0.3939                                | 0.00812                                 | 0.02062  | 123.103                                 | 48.469                                   | 75  |
| 80  | 2.701                         | 0.3702                                | 0.00735                                 | 0.01985  | 136.119                                 | 50.387                                   | 80  |
| 85  | 2.875                         | 0.3479                                | 0.00667                                 | 0.01917  | 149.968                                 | 52.170                                   | 85  |
| 90  | 3.059                         | 0.3269                                | 0.00607                                 | 0.01857  | 164.705                                 | 53.846                                   | 90  |
| 95  | 3.255                         | 0.3072                                | 0.00554                                 | 0.01804  | 180.336                                 | 55.421                                   | 95  |
| 100 | 3.463                         | 0.2887                                | 0.00507                                 | 0.01757  | 197.072                                 | 56.901                                   | 100 |

Table-3

| ANNEXURE 'C'—(Contd.)         |   |  |  |  |   |   |
|-------------------------------|---|--|--|--|---|---|
| TABLE 3                       |   |  |  |  |   |   |
| 1½% Compound Interest Factors |   |  |  |  |   |   |
| n                             | Single Payment                          |  | Uniform Series                           |  |   |   |
|                               | Compound Amount Factor cal <sup>1</sup> | Present Worth Factor pwf               | Sinking Fund Factor sff                  | Capital Recovery Factor crf            | Compound Amount Factor cal              | Present Worth Factor pwf                |
|                               | Given P To find S (1+i) <sup>n</sup>    | Given S To find P 1/(1+i) <sup>n</sup> | Given S To find R 1/(1+i) <sup>n-1</sup> | Given P To find R i/(1+i) <sup>n</sup> | Given R To find S (1+i) <sup>n</sup> -1 | Given R To find P 1/i(1+i) <sup>n</sup> |
| 1                             | 1.015                                   | 0.9852                                 | 1.02000                                  | 1.01500                                | 1.010                                   | 0.985                                   |
| 2                             | 1.030                                   | 0.9707                                 | 0.49628                                  | 0.51128                                | 2.015                                   | 1.956                                   |
| 3                             | 1.046                                   | 0.9563                                 | 0.83283                                  | 0.34038                                | 3.045                                   | 2.912                                   |
| 4                             | 1.061                                   | 0.9422                                 | 0.24444                                  | 0.25944                                | 4.091                                   | 3.854                                   |
| 5                             | 1.077                                   | 0.9283                                 | 0.19409                                  | 0.20909                                | 5.152                                   | 4.783                                   |
| 6                             | 1.093                                   | 0.9145                                 | 0.16053                                  | 0.17553                                | 6.230                                   | 5.697                                   |
| 7                             | 1.110                                   | 0.9010                                 | 0.13656                                  | 0.15156                                | 7.323                                   | 6.598                                   |
| 8                             | 1.126                                   | 0.8877                                 | 0.11858                                  | 0.13358                                | 8.421                                   | 7.486                                   |
| 9                             | 1.143                                   | 0.8746                                 | 0.10461                                  | 0.11961                                | 9.529                                   | 8.361                                   |
| 10                            | 1.161                                   | 0.8617                                 | 0.09243                                  | 0.10843                                | 10.702                                  | 9.222                                   |
| 11                            | 1.178                                   | 0.8489                                 | 0.08429                                  | 0.09929                                | 11.863                                  | 10.071                                  |
| 12                            | 1.196                                   | 0.8364                                 | 0.07668                                  | 0.09168                                | 13.041                                  | 10.908                                  |
| 13                            | 1.214                                   | 0.8240                                 | 0.07024                                  | 0.08524                                | 14.237                                  | 11.732                                  |
| 14                            | 1.232                                   | 0.8118                                 | 0.06472                                  | 0.07972                                | 15.450                                  | 12.543                                  |
| 15                            | 1.250                                   | 0.7999                                 | 0.05994                                  | 0.07494                                | 16.682                                  | 13.343                                  |
| 16                            | 1.269                                   | 0.7880                                 | 0.05577                                  | 0.07077                                | 17.932                                  | 14.131                                  |
| 17                            | 1.288                                   | 0.7764                                 | 0.05208                                  | 0.06708                                | 19.201                                  | 14.908                                  |
| 18                            | 1.307                                   | 0.7649                                 | 0.04881                                  | 0.06381                                | 20.489                                  | 15.673                                  |
| 19                            | 1.327                                   | 0.7536                                 | 0.04588                                  | 0.06088                                | 21.797                                  | 16.426                                  |
| 20                            | 1.347                                   | 0.7425                                 | 0.04325                                  | 0.05825                                | 23.124                                  | 17.169                                  |
| 21                            | 1.367                                   | 0.7315                                 | 0.04087                                  | 0.05587                                | 24.471                                  | 17.900                                  |
| 22                            | 1.388                                   | 0.7207                                 | 0.03879                                  | 0.05370                                | 25.838                                  | 18.621                                  |
| 23                            | 1.408                                   | 0.7100                                 | 0.03673                                  | 0.05173                                | 27.225                                  | 19.331                                  |
| 24                            | 1.430                                   | 0.6995                                 | 0.03492                                  | 0.04992                                | 28.634                                  | 20.030                                  |
| 25                            | 1.451                                   | 0.6892                                 | 0.03336                                  | 0.04836                                | 30.063                                  | 20.720                                  |
| 26                            | 1.473                                   | 0.6790                                 | 0.03173                                  | 0.04673                                | 31.514                                  | 21.399                                  |
| 27                            | 1.495                                   | 0.6690                                 | 0.03032                                  | 0.04532                                | 32.987                                  | 22.068                                  |
| 28                            | 1.517                                   | 0.6591                                 | 0.02900                                  | 0.04400                                | 34.481                                  | 22.727                                  |
| 29                            | 1.540                                   | 0.6494                                 | 0.02770                                  | 0.04270                                | 35.999                                  | 23.376                                  |
| 30                            | 1.563                                   | 0.6398                                 | 0.02644                                  | 0.04144                                | 37.539                                  | 24.016                                  |
| 31                            | 1.587                                   | 0.6303                                 | 0.02557                                  | 0.04057                                | 39.102                                  | 24.646                                  |
| 32                            | 1.610                                   | 0.6210                                 | 0.02458                                  | 0.03958                                | 40.688                                  | 25.267                                  |
| 33                            | 1.634                                   | 0.6118                                 | 0.02364                                  | 0.03864                                | 42.299                                  | 25.879                                  |
| 34                            | 1.659                                   | 0.6028                                 | 0.02276                                  | 0.03776                                | 43.933                                  | 26.482                                  |
| 35                            | 1.684                                   | 0.5939                                 | 0.02193                                  | 0.03693                                | 45.592                                  | 27.076                                  |
| 40                            | 1.814                                   | 0.5513                                 | 0.01843                                  | 0.03343                                | 54.268                                  | 29.916                                  |
| 45                            | 1.954                                   | 0.5117                                 | 0.01572                                  | 0.03072                                | 63.614                                  | 31.552                                  |
| 50                            | 2.105                                   | 0.4750                                 | 0.01357                                  | 0.02857                                | 73.483                                  | 35.000                                  |
| 55                            | 2.260                                   | 0.4409                                 | 0.01183                                  | 0.02683                                | 84.520                                  | 37.271                                  |
| 60                            | 2.443                                   | 0.4093                                 | 0.01039                                  | 0.02539                                | 96.215                                  | 39.380                                  |
| 65                            | 2.632                                   | 0.3799                                 | 0.00919                                  | 0.02419                                | 108.803                                 | 41.338                                  |
| 70                            | 2.835                                   | 0.3527                                 | 0.00817                                  | 0.02317                                | 122.364                                 | 43.155                                  |
| 75                            | 3.055                                   | 0.3274                                 | 0.00730                                  | 0.02230                                | 136.973                                 | 44.842                                  |
| 80                            | 3.291                                   | 0.3039                                 | 0.00655                                  | 0.02155                                | 152.711                                 | 46.407                                  |
| 85                            | 3.545                                   | 0.2821                                 | 0.00589                                  | 0.02089                                | 169.645                                 | 47.861                                  |
| 90                            | 3.819                                   | 0.2619                                 | 0.00542                                  | 0.02032                                | 187.930                                 | 49.240                                  |
| 95                            | 4.114                                   | 0.2431                                 | 0.00482                                  | 0.01982                                | 207.606                                 | 50.462                                  |
| 100                           | 4.432                                   | 0.2256                                 | 0.00437                                  | 0.01937                                | 228.803                                 | 51.625                                  |



Table - 4

ANNEXURE 'C'—(Contd.)

TABLE 4

1½% Compound Interest Factors

| n   | Single Payment               |                                       |   | Uniform Series                                 |   |  | n   |
|-----|------------------------------|---------------------------------------|---|--|---|--|-----|
|     | Compound Amount Factor $cal$ | Present Worth Factor $pwf$            | Sinking Fund Factor $sf$                | Capital Recovery Factor $crf$                  | Compound Amount Factor $cal$            | Present Worth Factor $pwf$             |     |
|     | Given P To find S $(1+i)^n$  | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1}{i(1+i)^n}$ |     |
| 1   | 1.018                        | 0.9828                                | 1.00000                                 | 1.01750  | 1.000                                   | 0.983                                  | 1   |
| 2   | 1.035                        | 0.9659                                | 0.49566                                 | 0.51316  | 2.018                                   | 1.949                                  | 2   |
| 3   | 1.053                        | 0.9493                                | 0.32757                                 | 0.34507  | 3.053                                   | 2.898                                  | 3   |
| 4   | 1.072                        | 0.9330                                | 0.24353                                 | 0.26103  | 4.104                                   | 3.831                                  | 4   |
| 5   | 1.091                        | 0.9169                                | 0.19312                                 | 0.21062  | 5.178                                   | 4.748                                  | 5   |
| 6   | 1.110                        | 0.9011                                | 0.15952                                 | 0.17792  | 6.269                                   | 5.649                                  | 6   |
| 7   | 1.129                        | 0.8855                                | 0.13553                                 | 0.15303  | 7.378                                   | 6.535                                  | 7   |
| 8   | 1.149                        | 0.8704                                | 0.11754                                 | 0.13304  | 8.508                                   | 7.405                                  | 8   |
| 9   | 1.169                        | 0.8554                                | 0.10356                                 | 0.12106  | 9.656                                   | 8.260                                  | 9   |
| 10  | 1.189                        | 0.8407                                | 0.09238                                 | 0.10988  | 10.825                                  | 9.101                                  | 10  |
| 11  | 1.210                        | 0.8263                                | 0.08323                                 | 0.10073  | 12.015                                  | 9.927                                  | 11  |
| 12  | 1.231                        | 0.8121                                | 0.07561                                 | 0.09311  | 13.225                                  | 10.740                                 | 12  |
| 13  | 1.253                        | 0.7981                                | 0.06917                                 | 0.08667  | 14.457                                  | 11.538                                 | 13  |
| 14  | 1.275                        | 0.7844                                | 0.06366                                 | 0.08116  | 15.710                                  | 12.322                                 | 14  |
| 15  | 1.297                        | 0.7709                                | 0.05888                                 | 0.07638  | 16.984                                  | 13.093                                 | 15  |
| 16  | 1.320                        | 0.7576                                | 0.05470                                 | 0.07220  | 18.282                                  | 13.850                                 | 16  |
| 17  | 1.343                        | 0.7446                                | 0.05102                                 | 0.06852  | 19.602                                  | 14.595                                 | 17  |
| 18  | 1.367                        | 0.7318                                | 0.04774                                 | 0.06524  | 20.945                                  | 15.327                                 | 18  |
| 19  | 1.390                        | 0.7192                                | 0.04482                                 | 0.06232  | 22.311                                  | 16.046                                 | 19  |
| 20  | 1.415                        | 0.7068                                | 0.04219                                 | 0.05969  | 23.702                                  | 16.753                                 | 20  |
| 21  | 1.440                        | 0.6947                                | 0.03981                                 | 0.05731  | 25.116                                  | 17.448                                 | 21  |
| 22  | 1.465                        | 0.6827                                | 0.03766                                 | 0.05516  | 26.556                                  | 18.130                                 | 22  |
| 23  | 1.490                        | 0.6710                                | 0.03569                                 | 0.05319  | 28.021                                  | 18.801                                 | 23  |
| 24  | 1.516                        | 0.6594                                | 0.03389                                 | 0.05139  | 29.511                                  | 19.461                                 | 24  |
| 25  | 1.543                        | 0.6481                                | 0.03223                                 | 0.04973  | 31.027                                  | 20.109                                 | 25  |
| 26  | 1.570                        | 0.6369                                | 0.03070                                 | 0.04820  | 32.570                                  | 20.746                                 | 26  |
| 27  | 1.597                        | 0.6260                                | 0.02929                                 | 0.04679  | 34.140                                  | 21.372                                 | 27  |
| 28  | 1.625                        | 0.6152                                | 0.02798                                 | 0.04548  | 35.738                                  | 21.987                                 | 28  |
| 29  | 1.654                        | 0.6046                                | 0.02676                                 | 0.04426  | 37.363                                  | 22.592                                 | 29  |
| 30  | 1.683                        | 0.5942                                | 0.02563                                 | 0.04313  | 39.017                                  | 23.186                                 | 30  |
| 31  | 1.712                        | 0.5840                                | 0.02457                                 | 0.04207  | 40.700                                  | 23.770                                 | 31  |
| 32  | 1.742                        | 0.5740                                | 0.02358                                 | 0.04108  | 42.412                                  | 24.344                                 | 32  |
| 33  | 1.773                        | 0.5641                                | 0.02265                                 | 0.04015  | 44.154                                  | 24.908                                 | 33  |
| 34  | 1.804                        | 0.5544                                | 0.02177                                 | 0.03927  | 45.927                                  | 25.462                                 | 34  |
| 35  | 1.835                        | 0.5449                                | 0.02095                                 | 0.03845  | 47.731                                  | 26.007                                 | 35  |
| 40  | 2.002                        | 0.4996                                | 0.01747                                 | 0.03497  | 57.234                                  | 28.594                                 | 40  |
| 45  | 2.183                        | 0.4581                                | 0.01479                                 | 0.03229  | 67.599                                  | 30.966                                 | 45  |
| 50  | 2.381                        | 0.4200                                | 0.01267                                 | 0.03017  | 78.902                                  | 33.141                                 | 50  |
| 55  | 2.597                        | 0.3851                                | 0.01096                                 | 0.02846  | 91.230                                  | 35.135                                 | 55  |
| 60  | 2.832                        | 0.3531                                | 0.00955                                 | 0.02705  | 104.675                                 | 36.964                                 | 60  |
| 65  | 3.088                        | 0.3238                                | 0.00838                                 | 0.02588  | 119.339                                 | 38.641                                 | 65  |
| 70  | 3.368                        | 0.2969                                | 0.00739                                 | 0.02489  | 135.331                                 | 40.178                                 | 70  |
| 75  | 3.674                        | 0.2722                                | 0.00655                                 | 0.02405  | 152.772                                 | 41.587                                 | 75  |
| 80  | 4.006                        | 0.2496                                | 0.00582                                 | 0.02332  | 171.794                                 | 42.885                                 | 80  |
| 85  | 4.369                        | 0.2289                                | 0.00519                                 | 0.02269  | 192.539                                 | 44.065                                 | 85  |
| 90  | 4.765                        | 0.2098                                | 0.00465                                 | 0.02215  | 215.165                                 | 45.152                                 | 90  |
| 95  | 5.197                        | 0.1924                                | 0.00417                                 | 0.02167  | 239.840                                 | 46.148                                 | 95  |
| 100 | 5.668                        | 0.1764                                | 0.00375                                 | 0.02125  | 266.752                                 | 47.061                                 | 100 |

Table - 5

| n   | Single Payment               |                                       | Uniform Series                          |  |   |   | n   |
|-----|------------------------------|---------------------------------------|---|--|---|---|-----|
|     | Compound Amount Factor $caf$ | Present Worth Factor $pwf$            | Sinking Fund Factor $sff$               | Capital Recovery Factor $crf$                  | Compound Amount Factor $caf$            | Present Worth Factor $pwf$                  |     |
|     | Given P To find S $(1+i)^n$  | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1-i(1+i)^{-n}}{i}$ |     |
| 1   | 1.020                        | 0.9804                                | 1.00000                                 | 1.02000  | 1.000                                   | 0.980                                       | 1   |
| 2   | 1.040                        | 0.9612                                | 0.49505                                 | 0.51505  | 2.020                                   | 1.942                                       | 2   |
| 3   | 1.061                        | 0.9423                                | 0.32675                                 | 0.34675  | 3.060                                   | 2.884                                       | 3   |
| 4   | 1.082                        | 0.9238                                | 0.24062                                 | 0.26262  | 4.122                                   | 3.808                                       | 4   |
| 5   | 1.104                        | 0.9057                                | 0.19216                                 | 0.21216  | 5.204                                   | 4.719                                       | 5   |
| 6   | 1.126                        | 0.8880                                | 0.15853                                 | 0.17853  | 6.308                                   | 5.601                                       | 6   |
| 7   | 1.149                        | 0.8706                                | 0.13451                                 | 0.15451  | 7.434                                   | 6.472                                       | 7   |
| 8   | 1.172                        | 0.8535                                | 0.11651                                 | 0.13651  | 8.583                                   | 7.325                                       | 8   |
| 9   | 1.195                        | 0.8368                                | 0.10252                                 | 0.12252  | 9.755                                   | 8.162                                       | 9   |
| 10  | 1.219                        | 0.8203                                | 0.09132                                 | 0.11132  | 10.950                                  | 8.983                                       | 10  |
| 11  | 1.243                        | 0.8042                                | 0.08216                                 | 0.10216  | 12.169                                  | 9.787                                       | 11  |
| 12  | 1.268                        | 0.7885                                | 0.07456                                 | 0.09456  | 13.412                                  | 10.575                                      | 12  |
| 13  | 1.294                        | 0.7730                                | 0.06812                                 | 0.08812  | 14.680                                  | 11.348                                      | 13  |
| 14  | 1.319                        | 0.7579                                | 0.06260                                 | 0.08260  | 15.974                                  | 12.106                                      | 14  |
| 15  | 1.346                        | 0.7430                                | 0.05783                                 | 0.07783  | 17.293                                  | 12.849                                      | 15  |
| 16  | 1.373                        | 0.7284                                | 0.05365                                 | 0.07365  | 18.639                                  | 13.578                                      | 16  |
| 17  | 1.400                        | 0.7142                                | 0.04997                                 | 0.06997  | 20.012                                  | 14.292                                      | 17  |
| 18  | 1.428                        | 0.7002                                | 0.04670                                 | 0.06670  | 21.412                                  | 14.992                                      | 18  |
| 19  | 1.457                        | 0.6864                                | 0.04378                                 | 0.06378  | 22.841                                  | 15.678                                      | 19  |
| 20  | 1.486                        | 0.6730                                | 0.04116                                 | 0.06116  | 24.299                                  | 16.351                                      | 20  |
| 21  | 1.516                        | 0.6598                                | 0.03878                                 | 0.05878  | 25.783                                  | 17.011                                      | 21  |
| 22  | 1.546                        | 0.6468                                | 0.03663                                 | 0.05663  | 27.299                                  | 17.658                                      | 22  |
| 23  | 1.577                        | 0.6342                                | 0.03467                                 | 0.05467  | 28.845                                  | 18.292                                      | 23  |
| 24  | 1.608                        | 0.6217                                | 0.03287                                 | 0.05287  | 30.422                                  | 18.914                                      | 24  |
| 25  | 1.641                        | 0.6095                                | 0.03122                                 | 0.05122  | 32.030                                  | 19.523                                      | 25  |
| 26  | 1.673                        | 0.5976                                | 0.02970                                 | 0.04970  | 33.671                                  | 20.121                                      | 26  |
| 27  | 1.707                        | 0.5859                                | 0.02829                                 | 0.04829  | 35.344                                  | 20.707                                      | 27  |
| 28  | 1.741                        | 0.5744                                | 0.02699                                 | 0.04699  | 37.051                                  | 21.281                                      | 28  |
| 29  | 1.776                        | 0.5631                                | 0.02578                                 | 0.04578  | 38.792                                  | 21.844                                      | 29  |
| 30  | 1.811                        | 0.5521                                | 0.02465                                 | 0.04465  | 40.568                                  | 22.396                                      | 30  |
| 31  | 1.848                        | 0.5412                                | 0.02360                                 | 0.04360  | 42.379                                  | 22.938                                      | 31  |
| 32  | 1.885                        | 0.5306                                | 0.02261                                 | 0.04261  | 44.227                                  | 23.468                                      | 32  |
| 33  | 1.922                        | 0.5202                                | 0.02169                                 | 0.04169  | 46.112                                  | 23.989                                      | 33  |
| 34  | 1.961                        | 0.5100                                | 0.02082                                 | 0.04082  | 48.034                                  | 24.499                                      | 34  |
| 35  | 2.000                        | 0.5000                                | 0.02000                                 | 0.04000  | 49.994                                  | 24.999                                      | 35  |
| 40  | 2.208                        | 0.4529                                | 0.01656                                 | 0.03656  | 60.402                                  | 27.355                                      | 40  |
| 45  | 2.438                        | 0.4102                                | 0.01391                                 | 0.03391  | 71.893                                  | 29.490                                      | 45  |
| 50  | 2.692                        | 0.3715                                | 0.01182                                 | 0.03182  | 84.579                                  | 31.424                                      | 50  |
| 55  | 2.972                        | 0.3365                                | 0.01014                                 | 0.03014  | 98.587                                  | 33.175                                      | 55  |
| 60  | 3.281                        | 0.3048                                | 0.00877                                 | 0.02877  | 114.052                                 | 34.761                                      | 60  |
| 65  | 3.623                        | 0.2761                                | 0.00763                                 | 0.02763  | 131.126                                 | 36.197                                      | 65  |
| 70  | 4.000                        | 0.2500                                | 0.00667                                 | 0.02667  | 149.978                                 | 37.499                                      | 70  |
| 75  | 4.416                        | 0.2265                                | 0.00586                                 | 0.02586  | 170.792                                 | 38.677                                      | 75  |
| 80  | 4.875                        | 0.2051                                | 0.00516                                 | 0.02516  | 193.772                                 | 39.745                                      | 80  |
| 85  | 5.383                        | 0.1858                                | 0.00456                                 | 0.02456  | 219.144                                 | 40.711                                      | 85  |
| 90  | 5.943                        | 0.1683                                | 0.00405                                 | 0.02405  | 247.157                                 | 41.587                                      | 90  |
| 95  | 6.562                        | 0.1524                                | 0.00360                                 | 0.02360  | 278.085                                 | 42.380                                      | 95  |
| 100 | 7.245                        | 0.1380                                | 0.00320                                 | 0.02320  | 312.232                                 | 43.098                                      | 100 |



Table- 6

ANNEXURE 'C'—(Contd.)

TABLE 6

2½ % Compound Interest Factors

| n   | Single Payment               |                                       | Uniform Series                          |  |   |   | n   |
|-----|------------------------------|---------------------------------------|---|--|---|---|-----|
|     | Compound Amount Factor $cal$ | Present Worth Factor $pwl$            | Sinking Fund Factor $sfl$               | Capital Recovery Factor $crf$                  | Compound Amount Factor $cal$            | Present Worth Factor $pwl$                  |     |
|     | Given P To find S $(1+i)^n$  | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1-i(1+i)^{-n}}{i}$ |     |
| 1   | 1.025                        | 0.9756                                | 1.00000                                 | 1.02500  | 1.000                                   | 0.975                                       | 1   |
| 2   | 1.051                        | 0.9518                                | 0.49383                                 | 0.51883  | 2.025                                   | 1.927                                       | 2   |
| 3   | 1.077                        | 0.9286                                | 0.32514                                 | 0.35014  | 3.076                                   | 2.856                                       | 3   |
| 4   | 1.104                        | 0.9060                                | 0.24083                                 | 0.26582  | 4.153                                   | 3.762                                       | 4   |
| 5   | 1.131                        | 0.8839                                | 0.19025                                 | 0.21525  | 5.256                                   | 4.646                                       | 5   |
| 6   | 1.160                        | 0.8623                                | 0.15655                                 | 0.18155  | 6.388                                   | 5.508                                       | 6   |
| 7   | 1.189                        | 0.8413                                | 0.13250                                 | 0.15750  | 7.547                                   | 6.349                                       | 7   |
| 8   | 1.219                        | 0.8207                                | 0.11447                                 | 0.13947  | 8.736                                   | 7.170                                       | 8   |
| 9   | 1.249                        | 0.8007                                | 0.10046                                 | 0.12546  | 9.955                                   | 7.971                                       | 9   |
| 10  | 1.280                        | 0.7812                                | 0.08926                                 | 0.11426  | 11.203                                  | 8.752                                       | 10  |
| 11  | 1.312                        | 0.7621                                | 0.08011                                 | 0.10511  | 12.483                                  | 9.514                                       | 11  |
| 12  | 1.345                        | 0.7436                                | 0.07249                                 | 0.09749  | 13.796                                  | 10.258                                      | 12  |
| 13  | 1.379                        | 0.7254                                | 0.06605                                 | 0.09105  | 15.140                                  | 10.983                                      | 13  |
| 14  | 1.413                        | 0.7077                                | 0.06054                                 | 0.08554  | 16.519                                  | 11.691                                      | 14  |
| 15  | 1.448                        | 0.6905                                | 0.05577                                 | 0.08077  | 17.932                                  | 12.381                                      | 15  |
| 16  | 1.485                        | 0.6736                                | 0.05160                                 | 0.07660  | 19.380                                  | 13.055                                      | 16  |
| 17  | 1.522                        | 0.6572                                | 0.04793                                 | 0.07293  | 20.865                                  | 13.712                                      | 17  |
| 18  | 1.560                        | 0.6412                                | 0.04467                                 | 0.06967  | 22.386                                  | 14.353                                      | 18  |
| 19  | 1.599                        | 0.6255                                | 0.04176                                 | 0.06676  | 23.946                                  | 14.979                                      | 19  |
| 20  | 1.639                        | 0.6103                                | 0.03915                                 | 0.06415  | 25.545                                  | 15.589                                      | 20  |
| 21  | 1.680                        | 0.5954                                | 0.03679                                 | 0.06179  | 27.183                                  | 16.185                                      | 21  |
| 22  | 1.722                        | 0.5808                                | 0.03465                                 | 0.05945  | 28.863                                  | 16.765                                      | 22  |
| 23  | 1.765                        | 0.5667                                | 0.03270                                 | 0.05770  | 30.584                                  | 17.332                                      | 23  |
| 24  | 1.809                        | 0.5529                                | 0.03091                                 | 0.05591  | 32.349                                  | 17.885                                      | 24  |
| 25  | 1.854                        | 0.5394                                | 0.02930                                 | 0.05428  | 34.158                                  | 18.424                                      | 25  |
| 26  | 1.900                        | 0.5262                                | 0.02777                                 | 0.05277  | 36.012                                  | 18.951                                      | 26  |
| 27  | 1.948                        | 0.5134                                | 0.02638                                 | 0.05138  | 37.912                                  | 19.464                                      | 27  |
| 28  | 1.996                        | 0.5009                                | 0.02509                                 | 0.05009  | 39.860                                  | 19.965                                      | 28  |
| 29  | 2.046                        | 0.4887                                | 0.02389                                 | 0.04889  | 41.856                                  | 20.454                                      | 29  |
| 30  | 2.098                        | 0.4767                                | 0.02278                                 | 0.04778  | 43.903                                  | 20.930                                      | 30  |
| 31  | 2.150                        | 0.4651                                | 0.02174                                 | 0.04674  | 46.000                                  | 21.395                                      | 31  |
| 32  | 2.204                        | 0.4538                                | 0.02077                                 | 0.04577  | 48.150                                  | 21.849                                      | 32  |
| 33  | 2.259                        | 0.4427                                | 0.01986                                 | 0.04486  | 50.354                                  | 22.292                                      | 33  |
| 34  | 2.315                        | 0.4319                                | 0.01901                                 | 0.04401  | 52.613                                  | 22.724                                      | 34  |
| 35  | 2.373                        | 0.4214                                | 0.01821                                 | 0.04321  | 54.928                                  | 23.145                                      | 35  |
| 40  | 2.685                        | 0.3724                                | 0.01484                                 | 0.03984  | 67.403                                  | 25.103                                      | 40  |
| 45  | 3.038                        | 0.3292                                | 0.01227                                 | 0.03727  | 81.516                                  | 26.833                                      | 45  |
| 50  | 3.437                        | 0.2909                                | 0.01026                                 | 0.03526  | 97.404                                  | 28.342                                      | 50  |
| 55  | 3.889                        | 0.2572                                | 0.00865                                 | 0.03365  | 115.551                                 | 29.714                                      | 55  |
| 60  | 4.400                        | 0.2273                                | 0.00735                                 | 0.03235  | 135.992                                 | 30.909                                      | 60  |
| 65  | 4.978                        | 0.2009                                | 0.00628                                 | 0.03128  | 159.118                                 | 31.965                                      | 65  |
| 70  | 5.632                        | 0.1776                                | 0.00540                                 | 0.03040  | 185.384                                 | 32.898                                      | 70  |
| 75  | 6.372                        | 0.1569                                | 0.00465                                 | 0.02965  | 214.888                                 | 33.728                                      | 75  |
| 80  | 7.210                        | 0.1387                                | 0.00403                                 | 0.02903  | 248.383                                 | 34.452                                      | 80  |
| 85  | 8.157                        | 0.1226                                | 0.00349                                 | 0.02849  | 286.379                                 | 35.096                                      | 85  |
| 90  | 9.329                        | 0.1084                                | 0.00304                                 | 0.02804  | 329.154                                 | 35.664                                      | 90  |
| 95  | 10.642                       | 0.0958                                | 0.00265                                 | 0.02765  | 377.644                                 | 36.169                                      | 95  |
| 100 | 11.814                       | 0.0846                                | 0.00231                                 | 0.02731  | 432.549                                 | 36.614                                      | 100 |

Table - 7

| ANNEXURE 'C'—(Contd.)        |                             |                                       |   |  |   |  |
|------------------------------|-----------------------------|---------------------------------------|---|--|---|--|
| TABLE 7                      |                             |                                       |   |  |   |  |
| 3% Compound Interest Factors |                             |                                       |   |  |   |  |
| n                            | Single Payment              |                                       | Uniform Series                          |  |   |  |
|                              | Compound Amount Factor cal  | Present Worth Factor pwt              | Sinking Fund Factor sff                 | Capital Recovery Factor crf                    | Compound Amount Factor cal              | Present Worth Factor pwt   |
|                              | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1}{i} \left[ 1 - \frac{1}{(1+i)^n} \right]$ |
| 1                            | 1.030                       | 0.9709                                | 1.00000                                 | 1.03000  | 1.000                                   | 0.971  |
| 2                            | 1.061                       | 0.9426                                | 0.49261                                 | 0.52361  | 2.030                                   | 1.913  |
| 3                            | 1.093                       | 0.9151                                | 0.32353                                 | 0.35353  | 3.091                                   | 2.809  |
| 4                            | 1.126                       | 0.8885                                | 0.23903                                 | 0.26903  | 4.184                                   | 3.717  |
| 5                            | 1.159                       | 0.8636                                | 0.18035                                 | 0.21035  | 5.309                                   | 4.580  |
| 6                            | 1.194                       | 0.8375                                | 0.15460                                 | 0.18460  | 6.468                                   | 5.417  |
| 7                            | 1.230                       | 0.8131                                | 0.13051                                 | 0.16051  | 7.662                                   | 6.230  |
| 8                            | 1.267                       | 0.7894                                | 0.11246                                 | 0.14246  | 8.892                                   | 7.025  |
| 9                            | 1.305                       | 0.7664                                | 0.09843                                 | 0.12843  | 10.159                                  | 7.795  |
| 10                           | 1.344                       | 0.7441                                | 0.08723                                 | 0.11723  | 11.464                                  | 8.530  |
| 11                           | 1.384                       | 0.7224                                | 0.07808                                 | 0.10808  | 12.808                                  | 9.233  |
| 12                           | 1.426                       | 0.7014                                | 0.07046                                 | 0.10046  | 14.192                                  | 9.904  |
| 13                           | 1.469                       | 0.6810                                | 0.06403                                 | 0.09403  | 15.618                                  | 10.635   |
| 14                           | 1.513                       | 0.6611                                | 0.05853                                 | 0.08853  | 17.086                                  | 11.326   |
| 15                           | 1.558                       | 0.6419                                | 0.05377                                 | 0.08377  | 18.599                                  | 11.938   |
| 16                           | 1.605                       | 0.6232                                | 0.04961                                 | 0.07961  | 20.157                                  | 12.561   |
| 17                           | 1.653                       | 0.6050                                | 0.04595                                 | 0.07595  | 21.762                                  | 13.166   |
| 18                           | 1.702                       | 0.5874                                | 0.04271                                 | 0.07271  | 23.414                                  | 13.754   |
| 19                           | 1.754                       | 0.5703                                | 0.03981                                 | 0.06981  | 25.117                                  | 14.324   |
| 20                           | 1.806                       | 0.5537                                | 0.03722                                 | 0.06722  | 26.870                                  | 14.877   |
| 21                           | 1.860                       | 0.5375                                | 0.03487                                 | 0.06487  | 28.676                                  | 15.415   |
| 22                           | 1.916                       | 0.5219                                | 0.03275                                 | 0.06275  | 30.537                                  | 15.937   |
| 23                           | 1.974                       | 0.5067                                | 0.03081                                 | 0.06081  | 32.453                                  | 16.444   |
| 24                           | 2.033                       | 0.4919                                | 0.02903                                 | 0.05903  | 34.426                                  | 16.936   |
| 25                           | 2.094                       | 0.4776                                | 0.02743                                 | 0.05743  | 36.459                                  | 17.413   |
| 26                           | 2.157                       | 0.4637                                | 0.02594                                 | 0.05594  | 38.553                                  | 17.877   |
| 27                           | 2.221                       | 0.4502                                | 0.02456                                 | 0.05456  | 40.710                                  | 18.327   |
| 28                           | 2.288                       | 0.4371                                | 0.02329                                 | 0.05329  | 42.931                                  | 18.764   |
| 29                           | 2.357                       | 0.4243                                | 0.02211                                 | 0.05211  | 45.219                                  | 19.188   |
| 30                           | 2.427                       | 0.4120                                | 0.02102                                 | 0.05102  | 47.575                                  | 19.600   |
| 31                           | 2.500                       | 0.4000                                | 0.02000                                 | 0.05000  | 50.000                                  | 20.000   |
| 32                           | 2.575                       | 0.3883                                | 0.01905                                 | 0.04905  | 52.503                                  | 20.389   |
| 33                           | 2.652                       | 0.3770                                | 0.01814                                 | 0.04814  | 55.078                                  | 20.766   |
| 34                           | 2.732                       | 0.3660                                | 0.01732                                 | 0.04732  | 57.730                                  | 21.132   |
| 35                           | 2.814                       | 0.3554                                | 0.01654                                 | 0.04654  | 60.462                                  | 21.487   |
| 40                           | 3.362                       | 0.3066                                | 0.01308                                 | 0.04308  | 75.401                                  | 23.115   |
| 45                           | 3.782                       | 0.2644                                | 0.01079                                 | 0.04079  | 92.720                                  | 24.519   |
| 50                           | 4.384                       | 0.2281                                | 0.00867                                 | 0.03867  | 112.797                                 | 25.730   |
| 55                           | 5.082                       | 0.1968                                | 0.00735                                 | 0.03735  | 136.072                                 | 26.774   |
| 60                           | 5.892                       | 0.1697                                | 0.00613                                 | 0.03613  | 163.053                                 | 27.676   |
| 65                           | 6.830                       | 0.1464                                | 0.00515                                 | 0.03515  | 194.333                                 | 28.453   |
| 70                           | 7.918                       | 0.1263                                | 0.00434                                 | 0.03434  | 230.294                                 | 29.123   |
| 75                           | 9.179                       | 0.1089                                | 0.00367                                 | 0.03367  | 272.631                                 | 29.702   |
| 80                           | 10.641                      | 0.0940                                | 0.00311                                 | 0.03311  | 321.363                                 | 30.201   |
| 85                           | 12.336                      | 0.0811                                | 0.00265                                 | 0.03265  | 377.857                                 | 30.631   |
| 90                           | 14.300                      | 0.0699                                | 0.00226                                 | 0.03226  | 443.349                                 | 31.002   |
| 95                           | 16.578                      | 0.0603                                | 0.00193                                 | 0.03193  | 519.272                                 | 31.323   |
| 100                          | 19.219                      | 0.0520                                | 0.00165                                 | 0.03165  | 607.288                                 | 31.599   |

Table - 8

| n   | Single Payment              |                                       |   | Uniform Series                                 |   |  | n   |
|-----|-----------------------------|---------------------------------------|---|--|---|--|-----|
|     | Compound Amount Factor $cf$ | Present Worth Factor $pwf$            | Sinking Fund Factor $sf$                | Capital Recovery Factor $crf$                  | Compound Amount Factor $cf$             | Present Worth Factor $pwf$             |     |
|     | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1}{i(1+i)^n}$ |     |
| 1   | 1.035                       | 0.9662                                | 1.00000                                 | 1.03500  | 1.000                                   | 0.966                                  | 1   |
| 2   | 1.071                       | 0.9335                                | 0.49140                                 | 0.52640  | 2.035                                   | 1.900                                  | 2   |
| 3   | 1.109                       | 0.9019                                | 0.32193                                 | 0.35693  | 3.106                                   | 2.802                                  | 3   |
| 4   | 1.148                       | 0.8714                                | 0.23725                                 | 0.27725  | 4.315                                   | 3.673                                  | 4   |
| 5   | 1.188                       | 0.8420                                | 0.18640                                 | 0.22148  | 5.362                                   | 4.515                                  | 5   |
| 6   | 1.229                       | 0.8135                                | 0.15267                                 | 0.18767  | 6.550                                   | 5.329                                  | 6   |
| 7   | 1.272                       | 0.7860                                | 0.12854                                 | 0.16354  | 7.779                                   | 6.115                                  | 7   |
| 8   | 1.317                       | 0.7594                                | 0.11048                                 | 0.14548  | 9.052                                   | 6.874                                  | 8   |
| 9   | 1.363                       | 0.7337                                | 0.09645                                 | 0.13145  | 10.368                                  | 7.608                                  | 9   |
| 10  | 1.411                       | 0.7089                                | 0.08524                                 | 0.12024  | 11.731                                  | 8.317                                  | 10  |
| 11  | 1.460                       | 0.6849                                | 0.07609                                 | 0.11109  | 13.142                                  | 9.002                                  | 11  |
| 12  | 1.511                       | 0.6618                                | 0.06848                                 | 0.10348  | 14.602                                  | 9.663                                  | 12  |
| 13  | 1.564                       | 0.6394                                | 0.06206                                 | 0.09706  | 16.113                                  | 10.303                                 | 13  |
| 14  | 1.619                       | 0.6178                                | 0.05657                                 | 0.09157  | 17.677                                  | 10.921                                 | 14  |
| 15  | 1.675                       | 0.5969                                | 0.05183                                 | 0.08683  | 19.296                                  | 11.517                                 | 15  |
| 16  | 1.734                       | 0.5767                                | 0.04768                                 | 0.08268  | 20.971                                  | 12.094                                 | 16  |
| 17  | 1.795                       | 0.5572                                | 0.04404                                 | 0.07904  | 22.705                                  | 12.651                                 | 17  |
| 18  | 1.857                       | 0.5384                                | 0.04082                                 | 0.07582  | 24.500                                  | 13.120                                 | 18  |
| 19  | 1.923                       | 0.5202                                | 0.03794                                 | 0.07294  | 26.357                                  | 13.710                                 | 19  |
| 20  | 1.990                       | 0.5026                                | 0.03536                                 | 0.07036  | 28.280                                  | 14.212                                 | 20  |
| 21  | 2.059                       | 0.4854                                | 0.03304                                 | 0.06804  | 30.269                                  | 14.698                                 | 21  |
| 22  | 2.132                       | 0.4689                                | 0.03093                                 | 0.06593  | 32.329                                  | 15.167                                 | 22  |
| 23  | 2.206                       | 0.4533                                | 0.02902                                 | 0.06402  | 34.460                                  | 15.620                                 | 23  |
| 24  | 2.283                       | 0.4380                                | 0.02727                                 | 0.06227  | 36.667                                  | 16.058                                 | 24  |
| 25  | 2.363                       | 0.4231                                | 0.02567                                 | 0.06067  | 38.950                                  | 16.482                                 | 25  |
| 26  | 2.446                       | 0.4088                                | 0.02421                                 | 0.05921  | 41.313                                  | 16.890                                 | 26  |
| 27  | 2.532                       | 0.3950                                | 0.02285                                 | 0.05785  | 43.759                                  | 17.285                                 | 27  |
| 28  | 2.620                       | 0.3817                                | 0.02160                                 | 0.05660  | 46.291                                  | 17.667                                 | 28  |
| 29  | 2.712                       | 0.3687                                | 0.02045                                 | 0.05545  | 48.911                                  | 18.036                                 | 29  |
| 30  | 2.807                       | 0.3563                                | 0.01937                                 | 0.05437  | 51.623                                  | 18.393                                 | 30  |
| 31  | 2.905                       | 0.3442                                | 0.01837                                 | 0.05337  | 54.429                                  | 18.736                                 | 31  |
| 32  | 3.007                       | 0.3326                                | 0.01744                                 | 0.05244  | 57.325                                  | 19.069                                 | 32  |
| 33  | 3.112                       | 0.3213                                | 0.01657                                 | 0.05157  | 60.341                                  | 19.390                                 | 33  |
| 34  | 3.221                       | 0.3105                                | 0.01576                                 | 0.05076  | 63.453                                  | 19.701                                 | 34  |
| 35  | 3.334                       | 0.3000                                | 0.01500                                 | 0.05000  | 66.674                                  | 20.001                                 | 35  |
| 40  | 3.959                       | 0.2524                                | 0.01183                                 | 0.04683  | 84.550                                  | 21.355                                 | 40  |
| 45  | 4.702                       | 0.2127                                | 0.00945                                 | 0.04445  | 105.782                                 | 22.495                                 | 45  |
| 50  | 5.585                       | 0.1791                                | 0.00763                                 | 0.04263  | 130.798                                 | 23.456                                 | 50  |
| 55  | 6.633                       | 0.1508                                | 0.00621                                 | 0.04121  | 160.747                                 | 24.264                                 | 55  |
| 60  | 7.878                       | 0.1269                                | 0.00509                                 | 0.04009  | 196.517                                 | 24.945                                 | 60  |
| 65  | 9.357                       | 0.1069                                | 0.00419                                 | 0.03917  | 238.763                                 | 25.518                                 | 65  |
| 70  | 11.113                      | 0.0900                                | 0.00346                                 | 0.03846  | 288.938                                 | 26.000                                 | 70  |
| 75  | 13.199                      | 0.0758                                | 0.00287                                 | 0.03787  | 348.530                                 | 26.407                                 | 75  |
| 80  | 15.676                      | 0.0638                                | 0.00238                                 | 0.03738  | 419.307                                 | 26.749                                 | 80  |
| 85  | 18.618                      | 0.0537                                | 0.00199                                 | 0.03699  | 503.367                                 | 27.037                                 | 85  |
| 90  | 22.112                      | 0.0452                                | 0.00164                                 | 0.03664  | 603.205                                 | 27.279                                 | 90  |
| 95  | 26.262                      | 0.0381                                | 0.00139                                 | 0.03639  | 721.701                                 | 27.484                                 | 95  |
| 100 | 31.191                      | 0.0321                                | 0.00114                                 | 0.03614  | 862.612                                 | 27.655                                 | 100 |

Table - 9

ANNEXURE 'C'—(Contd.)

TABLE 9

4% Compound Interest Factors

| n   | Single Payment              |                                       | Uniform Series                          |  |   |  | n   |
|-----|-----------------------------|---------------------------------------|---|--|---|--|-----|
|     | Compound Amount Factor cal  | Present Worth Factor pwf              | Sinking Fund Factor sff                 | Capital Recovery Factor crf                    | Compound Amount Factor cal              | Present Worth Factor pwf                 |     |
|     | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1}{i(1+i)^n-1}$ |     |
| 1   | 1.040                       | 0.9615                                | 1.00000                                 | 1.04000  | 1.000                                   | 0.961                                    | 1   |
| 2   | 1.082                       | 0.9246                                | 0.49020                                 | 0.53020  | 2.040                                   | 1.886                                    | 2   |
| 3   | 1.125                       | 0.8890                                | 0.32035                                 | 0.36035  | 3.122                                   | 2.775                                    | 3   |
| 4   | 1.170                       | 0.8548                                | 0.23549                                 | 0.27549  | 4.244                                   | 3.630                                    | 4   |
| 5   | 1.217                       | 0.8219                                | 0.18463                                 | 0.22463  | 5.416                                   | 4.452                                    | 5   |
| 6   | 1.265                       | 0.7903                                | 0.15076                                 | 0.19076  | 6.633                                   | 5.242                                    | 6   |
| 7   | 1.316                       | 0.7599                                | 0.12661                                 | 0.16661  | 7.899                                   | 6.002                                    | 7   |
| 8   | 1.369                       | 0.7307                                | 0.10853                                 | 0.14853  | 9.214                                   | 6.733                                    | 8   |
| 9   | 1.423                       | 0.7026                                | 0.09449                                 | 0.13449  | 10.583                                  | 7.435                                    | 9   |
| 10  | 1.480                       | 0.6756                                | 0.08329                                 | 0.12329  | 12.006                                  | 8.111                                    | 10  |
| 11  | 1.539                       | 0.6496                                | 0.07415                                 | 0.11415  | 13.486                                  | 8.760                                    | 11  |
| 12  | 1.601                       | 0.6246                                | 0.06645                                 | 0.10655  | 15.026                                  | 9.385                                    | 12  |
| 13  | 1.665                       | 0.6006                                | 0.06014                                 | 0.10014  | 16.627                                  | 9.986                                    | 13  |
| 14  | 1.732                       | 0.5775                                | 0.05467                                 | 0.09467  | 18.292                                  | 10.563                                   | 14  |
| 15  | 1.801                       | 0.5553                                | 0.04994                                 | 0.08994  | 20.024                                  | 11.118                                   | 15  |
| 16  | 1.873                       | 0.5339                                | 0.04582                                 | 0.08582  | 21.825                                  | 11.652                                   | 16  |
| 17  | 1.948                       | 0.5134                                | 0.04220                                 | 0.08220  | 23.698                                  | 12.166                                   | 17  |
| 18  | 2.026                       | 0.4936                                | 0.03899                                 | 0.07899  | 25.645                                  | 12.659                                   | 18  |
| 19  | 2.107                       | 0.4746                                | 0.03614                                 | 0.07614  | 27.671                                  | 13.134                                   | 19  |
| 20  | 2.191                       | 0.4564                                | 0.03358                                 | 0.07358  | 29.778                                  | 13.590                                   | 20  |
| 21  | 2.279                       | 0.4388                                | 0.03128                                 | 0.07128  | 31.969                                  | 14.029                                   | 21  |
| 22  | 2.370                       | 0.4220                                | 0.02920                                 | 0.06920  | 34.248                                  | 14.451                                   | 22  |
| 23  | 2.465                       | 0.4057                                | 0.02731                                 | 0.06731  | 36.618                                  | 14.857                                   | 23  |
| 24  | 2.563                       | 0.3901                                | 0.02559                                 | 0.06559  | 39.083                                  | 15.247                                   | 24  |
| 25  | 2.664                       | 0.3751                                | 0.02401                                 | 0.06401  | 41.644                                  | 15.622                                   | 25  |
| 26  | 2.772                       | 0.3607                                | 0.02257                                 | 0.06257  | 44.312                                  | 15.983                                   | 26  |
| 27  | 2.883                       | 0.3468                                | 0.02124                                 | 0.06124  | 47.084                                  | 16.330                                   | 27  |
| 28  | 2.999                       | 0.3335                                | 0.02001                                 | 0.06001  | 49.968                                  | 16.663                                   | 28  |
| 29  | 3.119                       | 0.3207                                | 0.01888                                 | 0.05888  | 52.966                                  | 16.984                                   | 29  |
| 30  | 3.243                       | 0.3083                                | 0.01783                                 | 0.05783  | 56.085                                  | 17.292                                   | 30  |
| 31  | 3.373                       | 0.2965                                | 0.01686                                 | 0.05686  | 59.328                                  | 17.588                                   | 31  |
| 32  | 3.508                       | 0.2851                                | 0.01595                                 | 0.05595  | 62.701                                  | 17.874                                   | 32  |
| 33  | 3.648                       | 0.2741                                | 0.01510                                 | 0.05510  | 66.210                                  | 18.148                                   | 33  |
| 34  | 3.794                       | 0.2636                                | 0.01431                                 | 0.05431  | 69.858                                  | 18.411                                   | 34  |
| 35  | 3.946                       | 0.2534                                | 0.01358                                 | 0.05358  | 73.652                                  | 18.665                                   | 35  |
| 40  | 4.801                       | 0.2083                                | 0.01052                                 | 0.05052  | 95.024                                  | 19.793                                   | 40  |
| 45  | 5.841                       | 0.1712                                | 0.00826                                 | 0.04826  | 121.029                                 | 20.720                                   | 45  |
| 50  | 7.107                       | 0.1407                                | 0.00655                                 | 0.04655  | 152.667                                 | 21.482                                   | 50  |
| 55  | 8.646                       | 0.1157                                | 0.00523                                 | 0.04523  | 191.159                                 | 22.109                                   | 55  |
| 60  | 10.520                      | 0.0951                                | 0.00420                                 | 0.04420  | 237.991                                 | 22.623                                   | 60  |
| 65  | 12.799                      | 0.0781                                | 0.00339                                 | 0.04339  | 294.968                                 | 23.047                                   | 65  |
| 70  | 15.572                      | 0.0642                                | 0.00275                                 | 0.04275  | 364.290                                 | 23.395                                   | 70  |
| 75  | 18.945                      | 0.0528                                | 0.00223                                 | 0.04223  | 448.631                                 | 23.680                                   | 75  |
| 80  | 23.030                      | 0.0434                                | 0.00181                                 | 0.04181  | 551.245                                 | 23.915                                   | 80  |
| 85  | 28.044                      | 0.0357                                | 0.00148                                 | 0.04148  | 676.090                                 | 24.107                                   | 85  |
| 90  | 34.119                      | 0.0293                                | 0.00121                                 | 0.04121  | 827.983                                 | 24.267                                   | 90  |
| 95  | 41.511                      | 0.0241                                | 0.00099                                 | 0.04099  | 1012.785                                | 24.398                                   | 95  |
| 100 | 50.505                      | 0.0198                                | 0.00081                                 | 0.04081  | 1237.624                                | 24.505                                   | 100 |



Table - 10

| ANNEXURE 'C'—(Contd.)         |                                  |  |   |  |                                  |  |     |
|-------------------------------|----------------------------------|--|---|--|----------------------------------|--|-----|
| TABLE 10                      |                                  |  |   |  |                                  |  |     |
| 4½% Compound Interest Factors |                                  |  |   |  |                                  |  |     |
| n                             | Single Payment                   |  |   | Uniform Series   |                                  |  | n   |
|                               | Compound Amount Factor $(1+i)^n$ | Present Worth Factor $\frac{1}{(1+i)^n}$ | Sinking Fund Factor $\frac{i}{(1+i)^n - 1}$ | Capital Recovery Factor $\frac{i(1+i)^n}{(1+i)^n - 1}$ | Compound Amount Factor $(1+i)^n$ | Present Worth Factor $\frac{1}{(1+i)^n}$ |     |
|                               | Given P To find S $(1+i)^n$      | Given S To find P $\frac{1}{(1+i)^n}$    | Given S To find R $\frac{i}{(1+i)^n - 1}$   | Given P To find R $\frac{i(1+i)^n}{(1+i)^n - 1}$       | Given R To find S $(1+i)^n$      | Given R To find P $\frac{1}{(1+i)^n}$    |     |
| 1                             | 1.045                            | 0.9569                                   | 1.00000                                     | 1.04500  | 1.000                            | 0.957                                    | 1   |
| 2                             | 1.092                            | 0.9157                                   | 0.48920                                     | 0.53400  | 2.045                            | 1.873                                    | 2   |
| 3                             | 1.141                            | 0.8763                                   | 0.31877                                     | 0.36377  | 3.137                            | 2.749                                    | 3   |
| 4                             | 1.193                            | 0.8386                                   | 0.23374                                     | 0.27674  | 4.278                            | 3.588                                    | 4   |
| 5                             | 1.246                            | 0.8025                                   | 0.18279                                     | 0.22719  | 5.471                            | 4.390                                    | 5   |
| 6                             | 1.302                            | 0.7679                                   | 0.14888                                     | 0.19388  | 6.717                            | 5.158                                    | 6   |
| 7                             | 1.361                            | 0.7348                                   | 0.12470                                     | 0.16970  | 8.019                            | 5.893                                    | 7   |
| 8                             | 1.422                            | 0.7032                                   | 0.10661                                     | 0.15161  | 9.380                            | 6.596                                    | 8   |
| 9                             | 1.486                            | 0.6729                                   | 0.09357                                     | 0.13757  | 10.802                           | 7.269                                    | 9   |
| 10                            | 1.553                            | 0.6439                                   | 0.08138                                     | 0.12638  | 12.288                           | 7.913                                    | 10  |
| 11                            | 1.623                            | 0.6162                                   | 0.07225                                     | 0.11725  | 13.841                           | 8.529                                    | 11  |
| 12                            | 1.696                            | 0.5897                                   | 0.06467                                     | 0.10967  | 15.464                           | 9.119                                    | 12  |
| 13                            | 1.772                            | 0.5643                                   | 0.05828                                     | 0.10328  | 17.160                           | 9.683                                    | 13  |
| 14                            | 1.852                            | 0.5400                                   | 0.05282                                     | 0.09782  | 18.932                           | 10.223                                   | 14  |
| 15                            | 1.935                            | 0.5167                                   | 0.04811                                     | 0.09311  | 20.784                           | 10.740                                   | 15  |
| 16                            | 2.022                            | 0.4945                                   | 0.04402                                     | 0.08902  | 22.719                           | 11.234                                   | 16  |
| 17                            | 2.113                            | 0.4732                                   | 0.04042                                     | 0.08542  | 24.743                           | 11.707                                   | 17  |
| 18                            | 2.208                            | 0.4528                                   | 0.03724                                     | 0.08224  | 26.855                           | 12.160                                   | 18  |
| 19                            | 2.308                            | 0.4333                                   | 0.03441                                     | 0.07941  | 29.064                           | 12.593                                   | 19  |
| 20                            | 2.412                            | 0.4146                                   | 0.03188                                     | 0.07688  | 31.371                           | 13.008                                   | 20  |
| 21                            | 2.520                            | 0.3968                                   | 0.02960                                     | 0.07460  | 33.783                           | 13.405                                   | 21  |
| 22                            | 2.634                            | 0.3797                                   | 0.02755                                     | 0.07255  | 36.303                           | 13.784                                   | 22  |
| 23                            | 2.752                            | 0.3634                                   | 0.02568                                     | 0.07068  | 38.937                           | 14.148                                   | 23  |
| 24                            | 2.876                            | 0.3477                                   | 0.02399                                     | 0.06899  | 41.689                           | 14.495                                   | 24  |
| 25                            | 3.006                            | 0.3327                                   | 0.02244                                     | 0.06744  | 44.565                           | 14.826                                   | 25  |
| 26                            | 3.141                            | 0.3184                                   | 0.02102                                     | 0.06602  | 47.571                           | 15.147                                   | 26  |
| 27                            | 3.282                            | 0.3047                                   | 0.01972                                     | 0.06472  | 50.711                           | 15.451                                   | 27  |
| 28                            | 3.430                            | 0.2916                                   | 0.01852                                     | 0.06352  | 53.993                           | 15.743                                   | 28  |
| 29                            | 3.584                            | 0.2790                                   | 0.01741                                     | 0.06241  | 57.423                           | 16.022                                   | 29  |
| 30                            | 3.745                            | 0.2670                                   | 0.01639                                     | 0.06139  | 61.007                           | 16.289                                   | 30  |
| 31                            | 3.914                            | 0.2555                                   | 0.01544                                     | 0.06044  | 64.752                           | 16.544                                   | 31  |
| 32                            | 4.090                            | 0.2445                                   | 0.01456                                     | 0.05956  | 68.666                           | 16.789                                   | 32  |
| 33                            | 4.274                            | 0.2340                                   | 0.01374                                     | 0.05874  | 72.756                           | 17.023                                   | 33  |
| 34                            | 4.466                            | 0.2239                                   | 0.01298                                     | 0.05798  | 77.030                           | 17.247                                   | 34  |
| 35                            | 4.667                            | 0.2143                                   | 0.01227                                     | 0.05727  | 81.497                           | 17.461                                   | 35  |
| 40                            | 5.816                            | 0.1719                                   | 0.00934                                     | 0.05434  | 107.030                          | 18.402                                   | 40  |
| 45                            | 7.248                            | 0.1380                                   | 0.00720                                     | 0.05220  | 138.850                          | 19.156                                   | 45  |
| 50                            | 9.033                            | 0.1107                                   | 0.00560                                     | 0.05060  | 178.503                          | 19.762                                   | 50  |
| 55                            | 11.256                           | 0.0888                                   | 0.00439                                     | 0.04939  | 227.916                          | 20.248                                   | 55  |
| 60                            | 14.027                           | 0.0713                                   | 0.00345                                     | 0.04845  | 289.498                          | 20.638                                   | 60  |
| 65                            | 17.481                           | 0.0572                                   | 0.00273                                     | 0.04773  | 366.238                          | 20.951                                   | 65  |
| 70                            | 21.784                           | 0.0459                                   | 0.00217                                     | 0.04717  | 461.870                          | 21.202                                   | 70  |
| 75                            | 27.147                           | 0.0368                                   | 0.00172                                     | 0.04672  | 581.044                          | 21.404                                   | 75  |
| 80                            | 33.830                           | 0.0296                                   | 0.00137                                     | 0.04637  | 729.558                          | 21.565                                   | 80  |
| 85                            | 42.158                           | 0.0237                                   | 0.00109                                     | 0.04609  | 914.432                          | 21.695                                   | 85  |
| 90                            | 52.537                           | 0.0190                                   | 0.00087                                     | 0.04587  | 1145.269                         | 21.799                                   | 90  |
| 95                            | 65.471                           | 0.0153                                   | 0.00070                                     | 0.04570  | 1432.684                         | 21.883                                   | 95  |
| 100                           | 81.589                           | 0.0123                                   | 0.00056                                     | 0.04556  | 1790.856                         | 21.950                                   | 100 |

Table - 11

| n   | Single Payment                       |                                       |   | Uniform Series                           |   |                                       | n   |
|-----|--------------------------------------|---------------------------------------|---|--|---|---------------------------------------|-----|
|     | Compound Amount Factor $\frac{F}{P}$ | Present Worth Factor $\frac{P}{F}$    | Sinking Fund Factor $\frac{R}{P}$       | Capital Recovery Factor $\frac{R}{P}$    | Compound Amount Factor $\frac{F}{P}$    | Present Worth Factor $\frac{P}{F}$    |     |
|     | Given P To find F $(1+i)^n$          | Given F To find P $\frac{1}{(1+i)^n}$ | Given F To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{iP}{(1+i)^n-1}$ | Given R To find F $\frac{(1+i)^n-1}{i}$ | Given F To find P $\frac{1}{(1+i)^n}$ |     |
| 1   | 1.050                                | 0.9524                                | 1.00000                                 | 1.05000                                  | 1.000                                   | 0.952                                 | 1   |
| 2   | 1.103                                | 0.9070                                | 0.48780                                 | 0.53780                                  | 2.050                                   | 0.887                                 | 2   |
| 3   | 1.158                                | 0.8638                                | 0.31721                                 | 0.36721                                  | 3.153                                   | 0.823                                 | 3   |
| 4   | 1.214                                | 0.8227                                | 0.23261                                 | 0.28261                                  | 4.310                                   | 0.769                                 | 4   |
| 5   | 1.276                                | 0.7835                                | 0.18097                                 | 0.23097                                  | 5.526                                   | 0.725                                 | 5   |
| 6   | 1.340                                | 0.7462                                | 0.14702                                 | 0.19702                                  | 6.802                                   | 0.686                                 | 6   |
| 7   | 1.407                                | 0.7107                                | 0.12282                                 | 0.17282                                  | 8.142                                   | 0.651                                 | 7   |
| 8   | 1.477                                | 0.6768                                | 0.10472                                 | 0.15472                                  | 9.549                                   | 0.618                                 | 8   |
| 9   | 1.551                                | 0.6446                                | 0.09069                                 | 0.14069                                  | 11.027                                  | 0.586                                 | 9   |
| 10  | 1.629                                | 0.6139                                | 0.07950                                 | 0.12950                                  | 12.578                                  | 0.556                                 | 10  |
| 11  | 1.710                                | 0.5847                                | 0.07039                                 | 0.12039                                  | 14.207                                  | 0.526                                 | 11  |
| 12  | 1.796                                | 0.5568                                | 0.06283                                 | 0.11283                                  | 15.917                                  | 0.500                                 | 12  |
| 13  | 1.886                                | 0.5303                                | 0.05646                                 | 0.10646                                  | 17.713                                  | 0.474                                 | 13  |
| 14  | 1.980                                | 0.5051                                | 0.05102                                 | 0.10102                                  | 19.599                                  | 0.450                                 | 14  |
| 15  | 2.079                                | 0.4810                                | 0.04634                                 | 0.09634                                  | 21.579                                  | 0.427                                 | 15  |
| 16  | 2.183                                | 0.4581                                | 0.04227                                 | 0.09227                                  | 23.657                                  | 0.405                                 | 16  |
| 17  | 2.292                                | 0.4363                                | 0.03870                                 | 0.08870                                  | 25.840                                  | 0.384                                 | 17  |
| 18  | 2.407                                | 0.4155                                | 0.03555                                 | 0.08555                                  | 28.132                                  | 0.364                                 | 18  |
| 19  | 2.527                                | 0.3957                                | 0.03275                                 | 0.08275                                  | 30.539                                  | 0.345                                 | 19  |
| 20  | 2.653                                | 0.3769                                | 0.03024                                 | 0.08024                                  | 33.066                                  | 0.326                                 | 20  |
| 21  | 2.786                                | 0.3589                                | 0.02800                                 | 0.07800                                  | 35.719                                  | 0.308                                 | 21  |
| 22  | 2.925                                | 0.3418                                | 0.02597                                 | 0.07597                                  | 38.505                                  | 0.291                                 | 22  |
| 23  | 3.072                                | 0.3256                                | 0.02414                                 | 0.07414                                  | 41.430                                  | 0.274                                 | 23  |
| 24  | 3.225                                | 0.3101                                | 0.02247                                 | 0.07247                                  | 44.502                                  | 0.258                                 | 24  |
| 25  | 3.386                                | 0.2953                                | 0.02095                                 | 0.07095                                  | 47.727                                  | 0.243                                 | 25  |
| 26  | 3.556                                | 0.2812                                | 0.01956                                 | 0.06956                                  | 51.113                                  | 0.228                                 | 26  |
| 27  | 3.733                                | 0.2678                                | 0.01829                                 | 0.06829                                  | 54.669                                  | 0.214                                 | 27  |
| 28  | 3.920                                | 0.2551                                | 0.01712                                 | 0.06712                                  | 58.403                                  | 0.200                                 | 28  |
| 29  | 4.116                                | 0.2429                                | 0.01605                                 | 0.06605                                  | 62.323                                  | 0.187                                 | 29  |
| 30  | 4.322                                | 0.2314                                | 0.01505                                 | 0.06505                                  | 66.439                                  | 0.174                                 | 30  |
| 31  | 4.538                                | 0.2204                                | 0.01412                                 | 0.06412                                  | 70.761                                  | 0.162                                 | 31  |
| 32  | 4.765                                | 0.2099                                | 0.01324                                 | 0.06324                                  | 75.299                                  | 0.150                                 | 32  |
| 33  | 5.003                                | 0.1999                                | 0.01249                                 | 0.06249                                  | 80.064                                  | 0.139                                 | 33  |
| 34  | 5.253                                | 0.1904                                | 0.01176                                 | 0.06176                                  | 85.067                                  | 0.128                                 | 34  |
| 35  | 5.516                                | 0.1813                                | 0.01107                                 | 0.06107                                  | 90.320                                  | 0.118                                 | 35  |
| 40  | 7.940                                | 0.1430                                | 0.00838                                 | 0.05838                                  | 120.800                                 | 0.090                                 | 40  |
| 45  | 8.985                                | 0.1113                                | 0.00636                                 | 0.05636                                  | 158.700                                 | 0.070                                 | 45  |
| 50  | 11.467                               | 0.0872                                | 0.00478                                 | 0.05478                                  | 209.348                                 | 0.055                                 | 50  |
| 55  | 14.634                               | 0.0683                                | 0.00367                                 | 0.05367                                  | 272.713                                 | 0.043                                 | 55  |
| 60  | 18.679                               | 0.0535                                | 0.00283                                 | 0.05283                                  | 353.584                                 | 0.035                                 | 60  |
| 65  | 23.840                               | 0.0419                                | 0.00215                                 | 0.05219                                  | 456.798                                 | 0.028                                 | 65  |
| 70  | 30.426                               | 0.0325                                | 0.00170                                 | 0.05170                                  | 588.529                                 | 0.022                                 | 70  |
| 75  | 38.833                               | 0.0258                                | 0.00132                                 | 0.05132                                  | 756.654                                 | 0.018                                 | 75  |
| 80  | 49.561                               | 0.0202                                | 0.00103                                 | 0.05103                                  | 971.229                                 | 0.015                                 | 80  |
| 85  | 63.254                               | 0.0158                                | 0.00080                                 | 0.05080                                  | 1245.087                                | 0.012                                 | 85  |
| 90  | 80.730                               | 0.0124                                | 0.00063                                 | 0.05063                                  | 1594.607                                | 0.010                                 | 90  |
| 95  | 103.035                              | 0.0097                                | 0.00049                                 | 0.05049                                  | 2040.654                                | 0.008                                 | 95  |
| 100 | 131.501                              | 0.0076                                | 0.00038                                 | 0.05038                                  | 2610.025                                | 0.006                                 | 100 |

Table - 12  
ANNEXURE 'C'—(Contd.)

TABLE 12  
5½ % Compound Interest Factors

| n   | Single Payment                   |  | Uniform Series                              |  |                                  |  | n   |
|-----|----------------------------------|--|---|--|----------------------------------|--|-----|
|     | Compound Amount Factor $(1+i)^n$ | Present Worth Factor $\frac{1}{(1+i)^n}$ | Sinking Fund Factor $\frac{i}{(1+i)^n - 1}$ | Capital Recovery Factor $\frac{i(1+i)^n}{(1+i)^n - 1}$ | Compound Amount Factor $(1+i)^n$ | Present Worth Factor $\frac{1}{(1+i)^n}$ |     |
|     | Given P To find S $(1+i)^n$      | Given S To find P $\frac{1}{(1+i)^n}$    | Given S To find R $\frac{i}{(1+i)^n - 1}$   | Given P To find R $\frac{i(1+i)^n}{(1+i)^n - 1}$       | Given R To find S $(1+i)^n$      | Given R To find P $\frac{1}{(1+i)^n}$    |     |
| 1   | 1.055                            | 0.9479                                   | 1.0000                                      | 1.0550   | 1.000                            | 0.948                                    | 1   |
| 2   | 1.113                            | 0.8965                                   | 0.48662                                     | 0.54162  | 2.035                            | 0.896                                    | 2   |
| 3   | 1.174                            | 0.8516                                   | 0.31565                                     | 0.37065  | 3.148                            | 0.852                                    | 3   |
| 4   | 1.239                            | 0.8072                                   | 0.23029                                     | 0.28529  | 4.343                            | 0.807                                    | 4   |
| 5   | 1.307                            | 0.7651                                   | 0.17918                                     | 0.23418  | 5.581                            | 0.765                                    | 5   |
| 6   | 1.379                            | 0.7252                                   | 0.14518                                     | 0.20018  | 6.888                            | 0.725                                    | 6   |
| 7   | 1.455                            | 0.6874                                   | 0.12096                                     | 0.17596  | 8.267                            | 0.687                                    | 7   |
| 8   | 1.535                            | 0.6516                                   | 0.10286                                     | 0.15786  | 9.722                            | 0.652                                    | 8   |
| 9   | 1.619                            | 0.6176                                   | 0.08889                                     | 0.14389  | 11.256                           | 0.618                                    | 9   |
| 10  | 1.708                            | 0.5854                                   | 0.07767                                     | 0.13267  | 12.875                           | 0.585                                    | 10  |
| 11  | 1.802                            | 0.5549                                   | 0.06857                                     | 0.12357  | 14.583                           | 0.555                                    | 11  |
| 12  | 1.901                            | 0.5260                                   | 0.06103                                     | 0.11603  | 16.386                           | 0.526                                    | 12  |
| 13  | 2.005                            | 0.4986                                   | 0.05469                                     | 0.10969  | 18.287                           | 0.499                                    | 13  |
| 14  | 2.115                            | 0.4725                                   | 0.04928                                     | 0.10428  | 20.293                           | 0.473                                    | 14  |
| 15  | 2.232                            | 0.4479                                   | 0.04463                                     | 0.09963  | 22.409                           | 0.448                                    | 15  |
| 16  | 2.355                            | 0.4246                                   | 0.04058                                     | 0.09558  | 24.641                           | 0.425                                    | 16  |
| 17  | 2.485                            | 0.4024                                   | 0.03704                                     | 0.09204  | 26.996                           | 0.402                                    | 17  |
| 18  | 2.621                            | 0.3815                                   | 0.03392                                     | 0.08892  | 29.481                           | 0.382                                    | 18  |
| 19  | 2.764                            | 0.3616                                   | 0.03115                                     | 0.08615  | 32.103                           | 0.362                                    | 19  |
| 20  | 2.918                            | 0.3427                                   | 0.02863                                     | 0.08363  | 34.868                           | 0.343                                    | 20  |
| 21  | 3.078                            | 0.3249                                   | 0.02646                                     | 0.08146  | 37.786                           | 0.325                                    | 21  |
| 22  | 3.248                            | 0.3079                                   | 0.02447                                     | 0.07947  | 40.864                           | 0.308                                    | 22  |
| 23  | 3.426                            | 0.2919                                   | 0.02267                                     | 0.07767  | 44.112                           | 0.292                                    | 23  |
| 24  | 3.615                            | 0.2767                                   | 0.02104                                     | 0.07604  | 47.538                           | 0.277                                    | 24  |
| 25  | 3.813                            | 0.2622                                   | 0.01955                                     | 0.07455  | 51.153                           | 0.262                                    | 25  |
| 26  | 4.023                            | 0.2486                                   | 0.01819                                     | 0.07319  | 54.966                           | 0.249                                    | 26  |
| 27  | 4.244                            | 0.2356                                   | 0.01695                                     | 0.07195  | 58.989                           | 0.236                                    | 27  |
| 28  | 4.476                            | 0.2232                                   | 0.01581                                     | 0.07081  | 63.234                           | 0.223                                    | 28  |
| 29  | 4.724                            | 0.2117                                   | 0.01477                                     | 0.06977  | 67.711                           | 0.212                                    | 29  |
| 30  | 4.984                            | 0.2006                                   | 0.01381                                     | 0.06881  | 72.435                           | 0.201                                    | 30  |
| 31  | 5.258                            | 0.1902                                   | 0.01292                                     | 0.06792  | 77.419                           | 0.190                                    | 31  |
| 32  | 5.547                            | 0.1803                                   | 0.01210                                     | 0.06710  | 82.677                           | 0.180                                    | 32  |
| 33  | 5.852                            | 0.1709                                   | 0.01133                                     | 0.06633  | 88.225                           | 0.171                                    | 33  |
| 34  | 6.174                            | 0.1620                                   | 0.01063                                     | 0.06563  | 94.077                           | 0.162                                    | 34  |
| 35  | 6.514                            | 0.1535                                   | 0.00997                                     | 0.06497  | 100.251                          | 0.154                                    | 35  |
| 40  | 8.512                            | 0.1175                                   | 0.00732                                     | 0.06232  | 136.606                          | 0.118                                    | 40  |
| 45  | 11.127                           | 0.0899                                   | 0.00543                                     | 0.06043  | 184.119                          | 0.090                                    | 45  |
| 50  | 14.542                           | 0.0688                                   | 0.00406                                     | 0.05906  | 246.217                          | 0.069                                    | 50  |
| 55  | 19.006                           | 0.0526                                   | 0.00305                                     | 0.05805  | 327.377                          | 0.053                                    | 55  |
| 60  | 24.840                           | 0.0403                                   | 0.00231                                     | 0.05731  | 432.450                          | 0.040                                    | 60  |
| 65  | 32.465                           | 0.0308                                   | 0.00175                                     | 0.05675  | 572.043                          | 0.031                                    | 65  |
| 70  | 42.430                           | 0.0236                                   | 0.00133                                     | 0.05633  | 753.271                          | 0.024                                    | 70  |
| 75  | 55.454                           | 0.0180                                   | 0.00101                                     | 0.05601  | 990.876                          | 0.018                                    | 75  |
| 80  | 72.476                           | 0.0138                                   | 0.00077                                     | 0.05577  | 1299.571                         | 0.014                                    | 80  |
| 85  | 94.724                           | 0.0106                                   | 0.00059                                     | 0.05559  | 1704.069                         | 0.011                                    | 85  |
| 90  | 123.800                          | 0.0081                                   | 0.00045                                     | 0.05545  | 2232.731                         | 0.008                                    | 90  |
| 95  | 161.802                          | 0.0062                                   | 0.00034                                     | 0.05534  | 2923.671                         | 0.006                                    | 95  |
| 100 | 211.469                          | 0.0047                                   | 0.00026                                     | 0.05526  | 3828.702                         | 0.005                                    | 100 |

Table - 13

| n   | Single Payment              |                                       | Uniform Series                          |  |   |  | n   |
|-----|-----------------------------|---------------------------------------|---|--|---|--|-----|
|     | Compound Amount Factor cal  | Present Worth Factor pwt              | Sinking Fund Factor sft                 | Capital Recovery Factor crrl                   | Compound Amount Factor cal              | Present Worth Factor pwt                 |     |
|     | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1-i}{i(1+i)^n}$ |     |
| 1   | 1.060                       | 0.9434                                | 1.00000                                 | 1.06000  | 1.060                                   | 0.943                                    | 1   |
| 2   | 1.124                       | 0.8900                                | 0.48544                                 | 0.94544  | 2.060                                   | 1.833                                    | 2   |
| 3   | 1.191                       | 0.8396                                | 0.31411                                 | 0.87411  | 3.184                                   | 2.673                                    | 3   |
| 4   | 1.262                       | 0.7921                                | 0.22857                                 | 0.78857  | 4.375                                   | 3.465                                    | 4   |
| 5   | 1.338                       | 0.7473                                | 0.17740                                 | 0.71740  | 5.637                                   | 4.212                                    | 5   |
| 6   | 1.419                       | 0.7050                                | 0.14336                                 | 0.65336  | 6.975                                   | 4.917                                    | 6   |
| 7   | 1.504                       | 0.6651                                | 0.11914                                 | 0.59914  | 8.394                                   | 5.582                                    | 7   |
| 8   | 1.594                       | 0.6274                                | 0.10104                                 | 0.55104  | 9.897                                   | 6.210                                    | 8   |
| 9   | 1.689                       | 0.5919                                | 0.08702                                 | 0.50702  | 11.491                                  | 6.802                                    | 9   |
| 10  | 1.791                       | 0.5584                                | 0.07587                                 | 0.46587  | 13.181                                  | 7.360                                    | 10  |
| 11  | 1.898                       | 0.5268                                | 0.06679                                 | 0.42679  | 14.972                                  | 7.887                                    | 11  |
| 12  | 2.012                       | 0.4970                                | 0.05928                                 | 0.3928   | 16.870                                  | 8.384                                    | 12  |
| 13  | 2.133                       | 0.4688                                | 0.05296                                 | 0.36296  | 18.882                                  | 8.853                                    | 13  |
| 14  | 2.261                       | 0.4423                                | 0.04758                                 | 0.33558  | 21.015                                  | 9.295                                    | 14  |
| 15  | 2.397                       | 0.4173                                | 0.04296                                 | 0.31036  | 23.276                                  | 9.712                                    | 15  |
| 16  | 2.540                       | 0.3936                                | 0.03895                                 | 0.28695  | 25.673                                  | 10.104                                   | 16  |
| 17  | 2.691                       | 0.3714                                | 0.03544                                 | 0.26544  | 28.213                                  | 10.477                                   | 17  |
| 18  | 2.851                       | 0.3503                                | 0.03236                                 | 0.24536  | 30.906                                  | 10.828                                   | 18  |
| 19  | 3.026                       | 0.3305                                | 0.02962                                 | 0.22662  | 33.760                                  | 11.158                                   | 19  |
| 20  | 3.207                       | 0.3118                                | 0.02718                                 | 0.20918  | 36.786                                  | 11.470                                   | 20  |
| 21  | 3.400                       | 0.2942                                | 0.02500                                 | 0.19300  | 39.993                                  | 11.764                                   | 21  |
| 22  | 3.604                       | 0.2775                                | 0.02305                                 | 0.17805  | 43.392                                  | 12.043                                   | 22  |
| 23  | 3.820                       | 0.2618                                | 0.02128                                 | 0.16428  | 46.996                                  | 12.307                                   | 23  |
| 24  | 4.049                       | 0.2470                                | 0.01968                                 | 0.15168  | 50.816                                  | 12.559                                   | 24  |
| 25  | 4.293                       | 0.2330                                | 0.01823                                 | 0.14023  | 54.865                                  | 12.793                                   | 25  |
| 26  | 4.549                       | 0.2196                                | 0.01690                                 | 0.12990  | 59.156                                  | 13.003                                   | 26  |
| 27  | 4.822                       | 0.2074                                | 0.01570                                 | 0.12070  | 63.706                                  | 13.211                                   | 27  |
| 28  | 5.112                       | 0.1956                                | 0.01459                                 | 0.11259  | 68.538                                  | 13.406                                   | 28  |
| 29  | 5.418                       | 0.1846                                | 0.01358                                 | 0.10538  | 73.660                                  | 13.591                                   | 29  |
| 30  | 5.743                       | 0.1741                                | 0.01265                                 | 0.09905  | 79.088                                  | 13.763                                   | 30  |
| 31  | 6.088                       | 0.1643                                | 0.01179                                 | 0.09379  | 84.832                                  | 13.929                                   | 31  |
| 32  | 6.453                       | 0.1550                                | 0.01100                                 | 0.08900  | 90.890                                  | 14.084                                   | 32  |
| 33  | 6.841                       | 0.1462                                | 0.01027                                 | 0.08467  | 97.273                                  | 14.230                                   | 33  |
| 34  | 7.251                       | 0.1379                                | 0.00960                                 | 0.08060  | 104.004                                 | 14.368                                   | 34  |
| 35  | 7.686                       | 0.1301                                | 0.00897                                 | 0.07687  | 111.115                                 | 14.498                                   | 35  |
| 40  | 10.286                      | 0.0972                                | 0.00646                                 | 0.05646  | 154.732                                 | 15.046                                   | 40  |
| 45  | 12.765                      | 0.0772                                | 0.00470                                 | 0.04070  | 212.744                                 | 15.456                                   | 45  |
| 50  | 16.470                      | 0.0543                                | 0.00344                                 | 0.02944  | 290.336                                 | 15.762                                   | 50  |
| 55  | 24.650                      | 0.0406                                | 0.00254                                 | 0.02154  | 394.172                                 | 15.991                                   | 55  |
| 60  | 32.988                      | 0.0303                                | 0.00188                                 | 0.01588  | 536.129                                 | 16.161                                   | 60  |
| 65  | 47.145                      | 0.0223                                | 0.00139                                 | 0.01139  | 719.263                                 | 16.289                                   | 65  |
| 70  | 59.076                      | 0.0169                                | 0.00103                                 | 0.00803  | 967.932                                 | 16.385                                   | 70  |
| 75  | 79.057                      | 0.0126                                | 0.00077                                 | 0.00607  | 1300.949                                | 16.456                                   | 75  |
| 80  | 105.796                     | 0.0095                                | 0.00057                                 | 0.00457  | 1746.600                                | 16.509                                   | 80  |
| 85  | 141.579                     | 0.0071                                | 0.00043                                 | 0.00343  | 2343.992                                | 16.549                                   | 85  |
| 90  | 189.465                     | 0.0053                                | 0.00032                                 | 0.00262  | 3141.075                                | 16.579                                   | 90  |
| 95  | 253.546                     | 0.0039                                | 0.00024                                 | 0.00204  | 4209.104                                | 16.601                                   | 95  |
| 100 | 339.302                     | 0.0029                                | 0.00018                                 | 0.00158  | 5616.368                                | 16.618                                   | 100 |



Table - 14

46

## ANNEXURE C—(Contd.)

TABLE 14

7% Compound Interest Factors

| n   | Single Payment                |                                       | Uniform Series                          |  |                               |  | n   |
|-----|-------------------------------|---------------------------------------|---|--|-------------------------------|--|-----|
|     | Compound Amount Factor $cf^1$ | Present Worth Factor $pwf^1$          | Sinking Fund Factor $sf^1$              | Capital Recovery Factor $cr^1$                 | Compound Amount Factor $cf^2$ | Present Worth Factor $pwf^2$             |     |
|     | Given P To find S $(1+i)^n$   | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given P To find S $(1+i)^n-1$ | Given R To find P $\frac{1-i}{i(1+i)^n}$ |     |
| 1   | 1.070                         | 0.9346                                | 1.00000                                 | 1.07000  | 1.000                         | 0.935                                    | 1   |
| 2   | 1.145                         | 0.8734                                | 0.48029                                 | 0.55209  | 2.070                         | 1.808                                    | 2   |
| 3   | 1.325                         | 0.8163                                | 0.31165                                 | 0.38105  | 3.215                         | 2.634                                    | 3   |
| 4   | 1.411                         | 0.7639                                | 0.23533                                 | 0.29533  | 4.440                         | 3.387                                    | 4   |
| 5   | 1.483                         | 0.7130                                | 0.17389                                 | 0.24389  | 5.731                         | 4.100                                    | 5   |
| 6   | 1.561                         | 0.6643                                | 0.13980                                 | 0.20980  | 7.153                         | 4.767                                    | 6   |
| 7   | 1.606                         | 0.6227                                | 0.11555                                 | 0.18555  | 8.654                         | 5.389                                    | 7   |
| 8   | 1.718                         | 0.5820                                | 0.09747                                 | 0.16747  | 10.260                        | 5.971                                    | 8   |
| 9   | 1.828                         | 0.5439                                | 0.08349                                 | 0.15349  | 11.978                        | 6.515                                    | 9   |
| 10  | 1.947                         | 0.5083                                | 0.07236                                 | 0.14236  | 13.816                        | 7.024                                    | 10  |
| 11  | 2.095                         | 0.4751                                | 0.06336                                 | 0.13336  | 15.784                        | 7.499                                    | 11  |
| 12  | 2.252                         | 0.4440                                | 0.05590                                 | 0.12590  | 17.888                        | 7.943                                    | 12  |
| 13  | 2.410                         | 0.4150                                | 0.04965                                 | 0.11965  | 20.141                        | 8.358                                    | 13  |
| 14  | 2.579                         | 0.3878                                | 0.04434                                 | 0.11434  | 22.550                        | 8.745                                    | 14  |
| 15  | 2.759                         | 0.3634                                | 0.03979                                 | 0.10979  | 25.129                        | 9.106                                    | 15  |
| 16  | 2.952                         | 0.3387                                | 0.03586                                 | 0.10586  | 27.888                        | 9.447                                    | 16  |
| 17  | 3.159                         | 0.3166                                | 0.03243                                 | 0.10243  | 30.840                        | 9.763                                    | 17  |
| 18  | 3.380                         | 0.2959                                | 0.02941                                 | 0.09941  | 33.999                        | 10.059                                   | 18  |
| 19  | 3.617                         | 0.2765                                | 0.02675                                 | 0.09675  | 37.379                        | 10.336                                   | 19  |
| 20  | 3.870                         | 0.2584                                | 0.02439                                 | 0.09439  | 40.985                        | 10.594                                   | 20  |
| 21  | 4.141                         | 0.2415                                | 0.02229                                 | 0.09229  | 44.865                        | 10.836                                   | 21  |
| 22  | 4.430                         | 0.2257                                | 0.02041                                 | 0.09041  | 48.956                        | 11.061                                   | 22  |
| 23  | 4.741                         | 0.2109                                | 0.01871                                 | 0.08871  | 53.336                        | 11.272                                   | 23  |
| 24  | 5.075                         | 0.1971                                | 0.01719                                 | 0.08719  | 58.077                        | 11.469                                   | 24  |
| 25  | 5.437                         | 0.1840                                | 0.01581                                 | 0.08581  | 63.249                        | 11.654                                   | 25  |
| 26  | 5.827                         | 0.1722                                | 0.01456                                 | 0.08456  | 68.876                        | 11.826                                   | 26  |
| 27  | 6.244                         | 0.1609                                | 0.01343                                 | 0.08343  | 74.984                        | 11.987                                   | 27  |
| 28  | 6.689                         | 0.1504                                | 0.01239                                 | 0.08239  | 81.606                        | 12.137                                   | 28  |
| 29  | 7.164                         | 0.1406                                | 0.01145                                 | 0.08145  | 88.787                        | 12.278                                   | 29  |
| 30  | 7.672                         | 0.1314                                | 0.01059                                 | 0.08059  | 96.461                        | 12.409                                   | 30  |
| 31  | 8.215                         | 0.1228                                | 0.00980                                 | 0.07980  | 104.673                       | 12.532                                   | 31  |
| 32  | 8.795                         | 0.1147                                | 0.00907                                 | 0.07907  | 113.478                       | 12.647                                   | 32  |
| 33  | 9.415                         | 0.1072                                | 0.00841                                 | 0.07841  | 122.923                       | 12.754                                   | 33  |
| 34  | 9.978                         | 0.1002                                | 0.00780                                 | 0.07780  | 133.259                       | 12.854                                   | 34  |
| 35  | 10.677                        | 0.0937                                | 0.00723                                 | 0.07723  | 144.537                       | 12.948                                   | 35  |
| 40  | 16.974                        | 0.0666                                | 0.00501                                 | 0.07501  | 199.435                       | 13.332                                   | 40  |
| 45  | 21.992                        | 0.0456                                | 0.00350                                 | 0.07350  | 285.749                       | 13.606                                   | 45  |
| 50  | 29.457                        | 0.0338                                | 0.00246                                 | 0.07246  | 406.539                       | 13.801                                   | 50  |
| 55  | 41.315                        | 0.0242                                | 0.00174                                 | 0.07174  | 575.929                       | 13.940                                   | 55  |
| 60  | 57.946                        | 0.0173                                | 0.00123                                 | 0.07123  | 813.520                       | 14.029                                   | 60  |
| 65  | 81.273                        | 0.0123                                | 0.00087                                 | 0.07087  | 1146.755                      | 14.119                                   | 65  |
| 70  | 113.989                       | 0.0088                                | 0.00062                                 | 0.07062  | 1614.134                      | 14.160                                   | 70  |
| 75  | 159.876                       | 0.0063                                | 0.00044                                 | 0.07044  | 2249.487                      | 14.196                                   | 75  |
| 80  | 224.334                       | 0.0045                                | 0.00031                                 | 0.07031  | 3109.063                      | 14.223                                   | 80  |
| 85  | 314.500                       | 0.0032                                | 0.00022                                 | 0.07022  | 4276.576                      | 14.240                                   | 85  |
| 90  | 441.153                       | 0.0023                                | 0.00016                                 | 0.07016  | 6287.185                      | 14.253                                   | 90  |
| 95  | 618.673                       | 0.0016                                | 0.00011                                 | 0.07011  | 8623.854                      | 14.263                                   | 95  |
| 100 | 847.714                       | 0.0012                                | 0.00008                                 | 0.07008  | 12281.662                     | 14.269                                   | 100 |

36

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Table - 15

| n   | Single Payment                          |                                       | Uniform Series                          |  |   |  | n   |
|-----|---|---------------------------------------|---|--|---|--|-----|
|     | Compound Amount Factor cal <sup>a</sup> | Present Worth Factor pwf <sup>b</sup> | Sinking Fund Factor sff <sup>c</sup>    | Capital Recovery Factor crf <sup>d</sup> | Compound Amount Factor cal <sup>e</sup> | Present Worth Factor pwf <sup>f</sup>    |     |
|     | Given P To find S (1+i) <sup>n</sup>    | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given R To find S $\frac{1}{i}(1+i)^n-1$ | Given R To find S (1+i) <sup>n</sup> -1 | Given R To find P $\frac{1}{i(1+i)^n-1}$ |     |
| 1   | 1.080                                   | 0.9259                                | 1.00000                                 | 1.08000                                  | 1.000                                   | 0.926                                    | 1   |
| 2   | 1.166                                   | 0.8573                                | 0.48077                                 | 0.56077                                  | 2.080                                   | 1.783                                    | 2   |
| 3   | 1.260                                   | 0.7938                                | 0.30803                                 | 0.38803                                  | 3.246                                   | 2.577                                    | 3   |
| 4   | 1.360                                   | 0.7350                                | 0.22192                                 | 0.30192                                  | 4.506                                   | 3.312                                    | 4   |
| 5   | 1.469                                   | 0.6806                                | 0.17046                                 | 0.25546                                  | 5.867                                   | 3.993                                    | 5   |
| 6   | 1.587                                   | 0.6302                                | 0.13632                                 | 0.21632                                  | 7.336                                   | 4.623                                    | 6   |
| 7   | 1.714                                   | 0.5835                                | 0.11207                                 | 0.19207                                  | 8.923                                   | 5.206                                    | 7   |
| 8   | 1.851                                   | 0.5403                                | 0.09401                                 | 0.17401                                  | 10.637                                  | 5.747                                    | 8   |
| 9   | 1.999                                   | 0.5002                                | 0.08068                                 | 0.16068                                  | 12.488                                  | 6.247                                    | 9   |
| 10  | 2.159                                   | 0.4632                                | 0.06903                                 | 0.14903                                  | 14.487                                  | 6.710                                    | 10  |
| 11  | 2.332                                   | 0.4289                                | 0.06008                                 | 0.14008                                  | 16.645                                  | 7.139                                    | 11  |
| 12  | 2.518                                   | 0.3971                                | 0.05270                                 | 0.13270                                  | 18.977                                  | 7.536                                    | 12  |
| 13  | 2.720                                   | 0.3677                                | 0.04652                                 | 0.12652                                  | 21.495                                  | 7.904                                    | 13  |
| 14  | 2.937                                   | 0.3405                                | 0.04130                                 | 0.12130                                  | 24.215                                  | 8.244                                    | 14  |
| 15  | 3.172                                   | 0.3152                                | 0.03683                                 | 0.11683                                  | 27.152                                  | 8.559                                    | 15  |
| 16  | 3.426                                   | 0.2919                                | 0.03298                                 | 0.11298                                  | 30.324                                  | 8.851                                    | 16  |
| 17  | 3.700                                   | 0.2703                                | 0.02963                                 | 0.10963                                  | 33.750                                  | 9.122                                    | 17  |
| 18  | 3.996                                   | 0.2502                                | 0.02670                                 | 0.10670                                  | 37.450                                  | 9.372                                    | 18  |
| 19  | 4.316                                   | 0.2317                                | 0.02413                                 | 0.10413                                  | 41.446                                  | 9.604                                    | 19  |
| 20  | 4.661                                   | 0.2145                                | 0.02185                                 | 0.10185                                  | 45.762                                  | 9.818                                    | 20  |
| 21  | 5.034                                   | 0.1987                                | 0.01983                                 | 0.09983                                  | 50.423                                  | 10.017                                   | 21  |
| 22  | 5.437                                   | 0.1839                                | 0.01803                                 | 0.09803                                  | 55.457                                  | 10.201                                   | 22  |
| 23  | 5.871                                   | 0.1703                                | 0.01642                                 | 0.09642                                  | 60.893                                  | 10.371                                   | 23  |
| 24  | 6.341                                   | 0.1577                                | 0.01498                                 | 0.09498                                  | 66.765                                  | 10.529                                   | 24  |
| 25  | 6.848                                   | 0.1460                                | 0.01368                                 | 0.09368                                  | 73.106                                  | 10.675                                   | 25  |
| 26  | 7.396                                   | 0.1352                                | 0.01251                                 | 0.09251                                  | 79.954                                  | 10.810                                   | 26  |
| 27  | 7.988                                   | 0.1252                                | 0.01145                                 | 0.09145                                  | 87.351                                  | 10.935                                   | 27  |
| 28  | 8.627                                   | 0.1159                                | 0.01049                                 | 0.09049                                  | 95.339                                  | 11.051                                   | 28  |
| 29  | 9.317                                   | 0.1073                                | 0.00962                                 | 0.08962                                  | 103.966                                 | 11.158                                   | 29  |
| 30  | 10.063                                  | 0.0994                                | 0.00883                                 | 0.08883                                  | 113.283                                 | 11.258                                   | 30  |
| 31  | 10.868                                  | 0.0920                                | 0.00811                                 | 0.08811                                  | 123.346                                 | 11.350                                   | 31  |
| 32  | 11.737                                  | 0.0852                                | 0.00745                                 | 0.08745                                  | 134.214                                 | 11.435                                   | 32  |
| 33  | 12.676                                  | 0.0789                                | 0.00685                                 | 0.08685                                  | 145.951                                 | 11.514                                   | 33  |
| 34  | 13.690                                  | 0.0730                                | 0.00630                                 | 0.08630                                  | 158.627                                 | 11.587                                   | 34  |
| 35  | 14.785                                  | 0.0676                                | 0.00580                                 | 0.08580                                  | 172.317                                 | 11.655                                   | 35  |
| 40  | 21.725                                  | 0.0460                                | 0.00386                                 | 0.08386                                  | 259.057                                 | 11.925                                   | 40  |
| 45  | 31.920                                  | 0.0313                                | 0.00259                                 | 0.08259                                  | 386.506                                 | 12.108                                   | 45  |
| 50  | 46.902                                  | 0.0213                                | 0.00174                                 | 0.08174                                  | 573.770                                 | 12.233                                   | 50  |
| 55  | 68.914                                  | 0.0145                                | 0.00118                                 | 0.08118                                  | 848.923                                 | 12.319                                   | 55  |
| 60  | 101.257                                 | 0.0099                                | 0.00080                                 | 0.08080                                  | 1253.213                                | 12.377                                   | 60  |
| 65  | 148.790                                 | 0.0067                                | 0.00054                                 | 0.08054                                  | 1847.248                                | 12.416                                   | 65  |
| 70  | 218.606                                 | 0.0046                                | 0.00037                                 | 0.08037                                  | 2720.080                                | 12.443                                   | 70  |
| 75  | 321.205                                 | 0.0031                                | 0.00025                                 | 0.08025                                  | 4002.557                                | 12.461                                   | 75  |
| 80  | 471.955                                 | 0.0021                                | 0.00017                                 | 0.08017                                  | 5886.935                                | 12.474                                   | 80  |
| 85  | 693.456                                 | 0.0014                                | 0.00012                                 | 0.08012                                  | 8655.706                                | 12.482                                   | 85  |
| 90  | 1018.915                                | 0.0010                                | 0.00008                                 | 0.08008                                  | 12723.939                               | 12.488                                   | 90  |
| 95  | 1497.121                                | 0.0007                                | 0.00005                                 | 0.08005                                  | 18701.507                               | 12.492                                   | 95  |
| 100 | 2199.761                                | 0.0005                                | 0.00004                                 | 0.08004                                  | 27484.516                               | 12.494                                   | 100 |

Table - 16

| n   | Single Payments                |                                       |   | Uniform Series                                 |   |   | n   |
|-----|--------------------------------|---------------------------------------|---|--|---|---|-----|
|     | Compound Amount Factor $cal^n$ | Present Worth Factor $pwf^n$          | Sinking Fund Factor $slf^n$             | Capital Recovery Factor $crl^n$                | Compound Amount Factor $cal^n$          | Present Worth Factor $pwf^n$                |     |
|     | Given P To find S $(1+i)^n$    | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1-i(1+i)^{-n}}{i}$ |     |
|     |                                |                                       |   |  |   |   |     |
| 1   | 1.100                          | 0.9091                                | 1.00000                                 | 1.10000  | 1.000                                   | 0.909                                       | 1   |
| 2   | 1.210                          | 0.8264                                | 0.47619                                 | 0.57619  | 2.100                                   | 1.736                                       | 2   |
| 3   | 1.331                          | 0.7513                                | 0.30211                                 | 0.40211  | 3.310                                   | 2.487                                       | 3   |
| 4   | 1.464                          | 0.6830                                | 0.21547                                 | 0.31547  | 4.641                                   | 3.170                                       | 4   |
| 5   | 1.611                          | 0.6209                                | 0.16100                                 | 0.26100  | 6.105                                   | 3.791                                       | 5   |
| 6   | 1.772                          | 0.5645                                | 0.12961                                 | 0.22961  | 7.716                                   | 4.355                                       | 6   |
| 7   | 1.949                          | 0.5132                                | 0.10541                                 | 0.20541  | 9.497                                   | 4.868                                       | 7   |
| 8   | 2.144                          | 0.4665                                | 0.08744                                 | 0.18744  | 11.436                                  | 5.335                                       | 8   |
| 9   | 2.358                          | 0.4241                                | 0.07364                                 | 0.17364  | 13.579                                  | 5.759                                       | 9   |
| 10  | 2.594                          | 0.3855                                | 0.06275                                 | 0.16275  | 15.937                                  | 6.144                                       | 10  |
| 11  | 2.851                          | 0.3505                                | 0.05396                                 | 0.15396  | 18.531                                  | 6.495                                       | 11  |
| 12  | 3.138                          | 0.3186                                | 0.04676                                 | 0.14676  | 21.384                                  | 6.814                                       | 12  |
| 13  | 3.452                          | 0.2897                                | 0.04078                                 | 0.14078  | 24.523                                  | 7.103                                       | 13  |
| 14  | 3.797                          | 0.2633                                | 0.03575                                 | 0.13575  | 27.975                                  | 7.367                                       | 14  |
| 15  | 4.177                          | 0.2394                                | 0.03147                                 | 0.13147  | 31.772                                  | 7.606                                       | 15  |
| 16  | 4.595                          | 0.2176                                | 0.02782                                 | 0.12782  | 35.950                                  | 7.824                                       | 16  |
| 17  | 5.054                          | 0.1978                                | 0.02466                                 | 0.12466  | 40.545                                  | 8.022                                       | 17  |
| 18  | 5.560                          | 0.1799                                | 0.02193                                 | 0.12193  | 45.599                                  | 8.191                                       | 18  |
| 19  | 6.116                          | 0.1635                                | 0.01955                                 | 0.11955  | 51.159                                  | 8.345                                       | 19  |
| 20  | 6.727                          | 0.1486                                | 0.01746                                 | 0.11746  | 57.275                                  | 8.514                                       | 20  |
| 21  | 7.400                          | 0.1351                                | 0.01562                                 | 0.11562  | 64.002                                  | 8.649                                       | 21  |
| 22  | 8.140                          | 0.1228                                | 0.01401                                 | 0.11401  | 71.403                                  | 8.772                                       | 22  |
| 23  | 8.954                          | 0.1117                                | 0.01257                                 | 0.11257  | 79.543                                  | 8.883                                       | 23  |
| 24  | 9.850                          | 0.1015                                | 0.01130                                 | 0.11130  | 88.497                                  | 8.985                                       | 24  |
| 25  | 10.835                         | 0.0923                                | 0.01017                                 | 0.11017  | 98.247                                  | 9.077                                       | 25  |
| 26  | 11.918                         | 0.0839                                | 0.00916                                 | 0.10916  | 108.82                                  | 9.161                                       | 26  |
| 27  | 13.110                         | 0.0763                                | 0.00826                                 | 0.10826  | 120.100                                 | 9.237                                       | 27  |
| 28  | 14.421                         | 0.0693                                | 0.00745                                 | 0.10745  | 132.210                                 | 9.307                                       | 28  |
| 29  | 15.863                         | 0.0630                                | 0.00673                                 | 0.10673  | 145.161                                 | 9.370                                       | 29  |
| 30  | 17.449                         | 0.0573                                | 0.00608                                 | 0.10608  | 159.044                                 | 9.427                                       | 30  |
| 31  | 19.194                         | 0.0521                                | 0.00550                                 | 0.10550  | 173.842                                 | 9.479                                       | 31  |
| 32  | 21.114                         | 0.0474                                | 0.00497                                 | 0.10497  | 189.569                                 | 9.526                                       | 32  |
| 33  | 23.225                         | 0.0431                                | 0.00450                                 | 0.10450  | 206.222                                 | 9.569                                       | 33  |
| 34  | 25.548                         | 0.0391                                | 0.00407                                 | 0.10407  | 223.897                                 | 9.609                                       | 34  |
| 35  | 28.102                         | 0.0356                                | 0.00369                                 | 0.10369  | 242.699                                 | 9.644                                       | 35  |
| 40  | 45.259                         | 0.0221                                | 0.00228                                 | 0.10228  | 442.593                                 | 9.779                                       | 40  |
| 45  | 72.890                         | 0.0137                                | 0.00139                                 | 0.10139  | 718.905                                 | 9.863                                       | 45  |
| 50  | 117.391                        | 0.0085                                | 0.00086                                 | 0.10086  | 1163.969                                | 9.915                                       | 50  |
| 55  | 189.059                        | 0.0053                                | 0.00053                                 | 0.10053  | 1886.591                                | 9.947                                       | 55  |
| 60  | 304.482                        | 0.0033                                | 0.00033                                 | 0.10033  | 3034.816                                | 9.967                                       | 60  |
| 65  | 490.371                        | 0.0020                                | 0.00020                                 | 0.10020  | 4893.707                                | 9.980                                       | 65  |
| 70  | 789.747                        | 0.0013                                | 0.00013                                 | 0.10013  | 7887.670                                | 9.987                                       | 70  |
| 75  | 127.895                        | 0.0008                                | 0.00008                                 | 0.10008  | 12708.954                               | 9.992                                       | 75  |
| 80  | 2048.400                       | 0.0005                                | 0.00005                                 | 0.10005  | 20474.002                               | 9.995                                       | 80  |
| 85  | 3259.949                       | 0.0003                                | 0.00003                                 | 0.10003  | 32579.690                               | 9.997                                       | 85  |
| 90  | 5313.523                       | 0.0002                                | 0.00002                                 | 0.10002  | 53120.326                               | 9.998                                       | 90  |
| 95  | 8554.676                       | 0.0001                                | 0.00001                                 | 0.10001  | 85556.740                               | 9.999                                       | 95  |
| 100 | 13700.612                      | 0.0001                                | 0.00001                                 | 0.10001  | 137796.123                              | 9.999                                       | 100 |

Table - 17

ANNEXURE 'C'— (Contd.)

TABLE 17

12% Compound Interest Factors

| n  | Single Payment              |                                       |   | Uniform Series                                 |   |  | n  |
|----|-----------------------------|---------------------------------------|---|--|---|--|----|
|    | Compound Amount Factor cal  | Present Worth Factor pwf              | Sinking Fund Factor sff                 | Capital Recovery Factor crf                    | Compound Amount Factor cal              | Present Worth Factor pwf                 |    |
|    | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1-i}{i(1+i)^n}$ |    |
| 1  | 1.120                       | 0.8929                                | 1.0000                                  | 1.12000  | 1.000                                   | 0.893                                    | 1  |
| 2  | 1.254                       | 0.7972                                | 0.47170                                 | 0.59170  | 2.120                                   | 1.690                                    | 2  |
| 3  | 1.405                       | 0.7118                                | 0.29635                                 | 0.41635  | 3.374                                   | 2.402                                    | 3  |
| 4  | 1.574                       | 0.6355                                | 0.20923                                 | 0.32923  | 4.779                                   | 3.037                                    | 4  |
| 5  | 1.762                       | 0.5674                                | 0.15741                                 | 0.27741  | 6.353                                   | 3.605                                    | 5  |
| 6  | 1.974                       | 0.5066                                | 0.12323                                 | 0.24323  | 8.115                                   | 4.111                                    | 6  |
| 7  | 2.211                       | 0.4523                                | 0.09912                                 | 0.21912  | 10.089                                  | 4.564                                    | 7  |
| 8  | 2.476                       | 0.4039                                | 0.08130                                 | 0.20130  | 12.300                                  | 4.968                                    | 8  |
| 9  | 2.773                       | 0.3606                                | 0.06768                                 | 0.18768  | 14.776                                  | 5.328                                    | 9  |
| 10 | 3.106                       | 0.3220                                | 0.05698                                 | 0.17698  | 17.549                                  | 5.650                                    | 10 |
| 11 | 3.479                       | 0.2875                                | 0.04842                                 | 0.16842  | 20.655                                  | 5.938                                    | 11 |
| 12 | 3.896                       | 0.2567                                | 0.04144                                 | 0.16144  | 24.133                                  | 6.194                                    | 12 |
| 13 | 4.363                       | 0.2292                                | 0.03568                                 | 0.15568  | 28.029                                  | 6.424                                    | 13 |
| 14 | 4.887                       | 0.2046                                | 0.03087                                 | 0.15087  | 32.393                                  | 6.628                                    | 14 |
| 15 | 5.474                       | 0.1827                                | 0.02682                                 | 0.14682  | 37.280                                  | 6.811                                    | 15 |
| 16 | 6.130                       | 0.1631                                | 0.02339                                 | 0.14339  | 42.753                                  | 6.974                                    | 16 |
| 17 | 6.866                       | 0.1456                                | 0.02046                                 | 0.14046  | 48.884                                  | 7.120                                    | 17 |
| 18 | 7.690                       | 0.1300                                | 0.01794                                 | 0.13794  | 55.790                                  | 7.250                                    | 18 |
| 19 | 8.613                       | 0.1161                                | 0.01576                                 | 0.13576  | 63.440                                  | 7.366                                    | 19 |
| 20 | 9.646                       | 0.1037                                | 0.01388                                 | 0.13388  | 72.052                                  | 7.469                                    | 20 |
| 21 | 10.804                      | 0.0926                                | 0.01224                                 | 0.13224  | 81.699                                  | 7.562                                    | 21 |
| 22 | 12.100                      | 0.0826                                | 0.01081                                 | 0.13081  | 92.502                                  | 7.645                                    | 22 |
| 23 | 13.552                      | 0.0738                                | 0.00956                                 | 0.12956  | 104.603                                 | 7.718                                    | 23 |
| 24 | 15.179                      | 0.0659                                | 0.00846                                 | 0.12846  | 118.155                                 | 7.784                                    | 24 |
| 25 | 17.000                      | 0.0588                                | 0.00750                                 | 0.12750  | 133.334                                 | 7.843                                    | 25 |
| 26 | 19.040                      | 0.0525                                | 0.00665                                 | 0.12665  | 150.134                                 | 7.896                                    | 26 |
| 27 | 21.325                      | 0.0469                                | 0.00590                                 | 0.12590  | 169.374                                 | 7.943                                    | 27 |
| 28 | 23.884                      | 0.0419                                | 0.00524                                 | 0.12524  | 190.699                                 | 7.984                                    | 28 |
| 29 | 26.750                      | 0.0374                                | 0.00466                                 | 0.12466  | 214.582                                 | 8.022                                    | 29 |
| 30 | 29.960                      | 0.0334                                | 0.00414                                 | 0.12414  | 241.332                                 | 8.055                                    | 30 |
| 31 | 33.555                      | 0.0298                                | 0.00369                                 | 0.12369  | 271.292                                 | 8.085                                    | 31 |
| 32 | 37.582                      | 0.0266                                | 0.00328                                 | 0.12328  | 304.847                                 | 8.112                                    | 32 |
| 33 | 42.091                      | 0.0238                                | 0.00292                                 | 0.12292  | 342.429                                 | 8.135                                    | 33 |
| 34 | 47.142                      | 0.0212                                | 0.00260                                 | 0.12260  | 384.520                                 | 8.157                                    | 34 |
| 35 | 52.799                      | 0.0189                                | 0.00232                                 | 0.12232  | 431.663                                 | 8.176                                    | 35 |
| 40 | 93.051                      | 0.0107                                | 0.00130                                 | 0.12130  | 767.088                                 | 8.244                                    | 40 |
| 45 | 163.987                     | 0.0061                                | 0.00074                                 | 0.12074  | 1358.224                                | 8.283                                    | 45 |
| 50 | 289.001                     | 0.0035                                | 0.00042                                 | 0.12042  | 2400.008                                | 8.305                                    | 50 |
| ∞  |                             |                                       |   | 0.12000  |   | 8.333                                    | ∞  |

Table - 18

| ANNEXURE 'C'—(Contd.)         |                             |                                       |   |  |   |   |
|-------------------------------|-----------------------------|---------------------------------------|---|--|---|---|
| TABLE 18                      |                             |                                       |   |  |   |   |
| 15% Compound Interest Factors |                             |                                       |   |  |   |   |
| n                             | Single Payments             |                                       | Uniform Series                          |  |   |   |
|                               | Compound Amount Factor cal' | Present Worth Factor pwf'             | Sinking Fund Factor sff                 | Capital Recovery Factor crf                    | Compound Amount Factor cal              | Present Worth Factor pwf                    |
|                               | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1-i(1+i)^{-n}}{i}$ |
| 1                             | 1.125                       | 0.8696                                | 1.00000                                 | 1.15000  | 1.000                                   | 0.870                                       |
| 2                             | 1.222                       | 0.7561                                | 0.46312                                 | 0.61512  | 2.150                                   | 1.626                                       |
| 3                             | 1.321                       | 0.6575                                | 0.28798                                 | 0.43798  | 3.472                                   | 2.283                                       |
| 4                             | 1.749                       | 0.5718                                | 0.20926                                 | 0.35027  | 4.993                                   | 2.855                                       |
| 5                             | 2.011                       | 0.4972                                | 0.14832                                 | 0.29832  | 6.742                                   | 3.352                                       |
| 6                             | 2.313                       | 0.4323                                | 0.11424                                 | 0.26424  | 8.754                                   | 3.784                                       |
| 7                             | 2.660                       | 0.3759                                | 0.09036                                 | 0.24036  | 11.067                                  | 4.160                                       |
| 8                             | 3.059                       | 0.3269                                | 0.07285                                 | 0.22285  | 13.727                                  | 4.487                                       |
| 9                             | 3.518                       | 0.2843                                | 0.05957                                 | 0.20957  | 16.786                                  | 4.772                                       |
| 10                            | 4.046                       | 0.2472                                | 0.04925                                 | 0.19925  | 20.304                                  | 5.019                                       |
| 11                            | 4.652                       | 0.2149                                | 0.04107                                 | 0.19107  | 24.249                                  | 5.234                                       |
| 12                            | 5.350                       | 0.1869                                | 0.03448                                 | 0.18448  | 29.092                                  | 5.421                                       |
| 13                            | 6.151                       | 0.1625                                | 0.02911                                 | 0.17911  | 34.352                                  | 5.583                                       |
| 14                            | 7.076                       | 0.1413                                | 0.02469                                 | 0.17469  | 40.505                                  | 5.724                                       |
| 15                            | 8.137                       | 0.1229                                | 0.02102                                 | 0.17102  | 47.580                                  | 5.847                                       |
| 16                            | 9.358                       | 0.1069                                | 0.01759                                 | 0.16705  | 55.717                                  | 5.954                                       |
| 17                            | 10.761                      | 0.0929                                | 0.01537                                 | 0.16337  | 65.075                                  | 6.047                                       |
| 18                            | 12.375                      | 0.0808                                | 0.01319                                 | 0.16019  | 75.836                                  | 6.128                                       |
| 19                            | 14.232                      | 0.0703                                | 0.01134                                 | 0.15734  | 88.212                                  | 6.198                                       |
| 20                            | 16.367                      | 0.0611                                | 0.00976                                 | 0.15476  | 102.443                                 | 6.259                                       |
| 21                            | 18.821                      | 0.0531                                | 0.00842                                 | 0.15242  | 118.810                                 | 6.312                                       |
| 22                            | 21.645                      | 0.0462                                | 0.00727                                 | 0.15027  | 137.631                                 | 6.359                                       |
| 23                            | 24.891                      | 0.0402                                | 0.00628                                 | 0.14828  | 159.276                                 | 6.399                                       |
| 24                            | 28.625                      | 0.0349                                | 0.00543                                 | 0.14643  | 184.167                                 | 6.434                                       |
| 25                            | 32.919                      | 0.0304                                | 0.00470                                 | 0.14470  | 212.793                                 | 6.464                                       |
| 26                            | 37.857                      | 0.0264                                | 0.00407                                 | 0.14307  | 245.711                                 | 6.491                                       |
| 27                            | 43.536                      | 0.0230                                | 0.00353                                 | 0.14153  | 283.560                                 | 6.514                                       |
| 28                            | 50.065                      | 0.0200                                | 0.00306                                 | 0.14006  | 327.103                                 | 6.534                                       |
| 29                            | 57.575                      | 0.0174                                | 0.00265                                 | 0.13865  | 377.169                                 | 6.551                                       |
| 30                            | 66.212                      | 0.0151                                | 0.00230                                 | 0.13730  | 434.744                                 | 6.564                                       |
| 31                            | 76.143                      | 0.0131                                | 0.00200                                 | 0.13600  | 500.956                                 | 6.579                                       |
| 32                            | 87.565                      | 0.0114                                | 0.00173                                 | 0.13473  | 577.099                                 | 6.591                                       |
| 33                            | 100.700                     | 0.0099                                | 0.00150                                 | 0.13350  | 664.664                                 | 6.600                                       |
| 34                            | 115.805                     | 0.0086                                | 0.00131                                 | 0.13131  | 765.364                                 | 6.609                                       |
| 35                            | 133.175                     | 0.0075                                | 0.00113                                 | 0.13113  | 881.168                                 | 6.617                                       |
| 40                            | 247.863                     | 0.0037                                | 0.00054                                 | 0.13054  | 1779.1                                  | 6.642                                       |
| 45                            | 538.767                     | 0.0019                                | 0.00028                                 | 0.13028  | 3585.1                                  | 6.654                                       |
| 50                            | 1083.652                    | 0.0009                                | 0.00014                                 | 0.13014  | 7217.7                                  | 6.661                                       |
| ∞                             |                             |                                       |   | 0.15000  |   | 6.667                                       |



Table - 19

ANNEXURE 'C'—(Contd.)

TABLE 19

20% Compound Interest Factors

| n  | Single Payment              |                                       |   | Uniform Series                                 |   |   | n  |
|----|-----------------------------|---------------------------------------|---|--|---|---|----|
|    | Compound Amount Factor cal  | Present Worth Factor pwf              | Sinking Fund Factor sff                 | Capital Recovery Factor crf                    | Compound Amount Factor cal              | Present Worth Factor pwf                |    |
|    | Given P To find S $(1+i)^n$ | Given S To find P $\frac{1}{(1+i)^n}$ | Given S To find R $\frac{i}{(1+i)^n-1}$ | Given P To find R $\frac{i(1+i)^n}{(1+i)^n-1}$ | Given R To find S $\frac{(1+i)^n-1}{i}$ | Given R To find P $\frac{1}{(1+i)^n-1}$ |    |
| 1  | 1.200                       | 0.8333                                | 1.0000                                  | 1.2000   | 1.000                                   | 0.833                                   | 1  |
| 2  | 1.440                       | 0.6944                                | 0.45455                                 | 0.65455  | 2.200                                   | 1.528                                   | 2  |
| 3  | 1.728                       | 0.5787                                | 0.27473                                 | 0.47473  | 3.640                                   | 2.106                                   | 3  |
| 4  | 2.074                       | 0.4823                                | 0.18629                                 | 0.38629  | 5.368                                   | 2.589                                   | 4  |
| 5  | 2.488                       | 0.4019                                | 0.13438                                 | 0.33438  | 7.442                                   | 2.991                                   | 5  |
| 6  | 2.986                       | 0.3349                                | 0.10071                                 | 0.30071  | 9.930                                   | 3.326                                   | 6  |
| 7  | 3.583                       | 0.2791                                | 0.07742                                 | 0.27742  | 12.916                                  | 3.605                                   | 7  |
| 8  | 4.300                       | 0.2324                                | 0.06061                                 | 0.26061  | 16.499                                  | 3.837                                   | 8  |
| 9  | 5.160                       | 0.1938                                | 0.04808                                 | 0.24808  | 20.799                                  | 4.031                                   | 9  |
| 10 | 6.192                       | 0.1615                                | 0.03852                                 | 0.23852  | 25.959                                  | 4.192                                   | 10 |
| 11 | 7.430                       | 0.1346                                | 0.03110                                 | 0.23110  | 32.140                                  | 4.327                                   | 11 |
| 12 | 8.916                       | 0.1122                                | 0.02524                                 | 0.22524  | 39.590                                  | 4.439                                   | 12 |
| 13 | 10.699                      | 0.0925                                | 0.02062                                 | 0.22062  | 48.497                                  | 4.533                                   | 13 |
| 14 | 12.839                      | 0.0779                                | 0.01689                                 | 0.21689  | 59.194                                  | 4.611                                   | 14 |
| 15 | 15.407                      | 0.0649                                | 0.01388                                 | 0.21388  | 72.035                                  | 4.675                                   | 15 |
| 16 | 18.488                      | 0.0541                                | 0.01144                                 | 0.21144  | 87.442                                  | 4.730                                   | 16 |
| 17 | 22.186                      | 0.0451                                | 0.00944                                 | 0.20944  | 105.931                                 | 4.775                                   | 17 |
| 18 | 26.623                      | 0.0374                                | 0.00781                                 | 0.20781  | 128.117                                 | 4.812                                   | 18 |
| 19 | 31.948                      | 0.0313                                | 0.00644                                 | 0.20644  | 154.740                                 | 4.844                                   | 19 |
| 20 | 38.338                      | 0.0261                                | 0.00534                                 | 0.20534  | 186.688                                 | 4.870                                   | 20 |
| 21 | 46.005                      | 0.0217                                | 0.00444                                 | 0.20444  | 225.025                                 | 4.891                                   | 21 |
| 22 | 55.204                      | 0.0181                                | 0.00369                                 | 0.20369  | 271.031                                 | 4.909                                   | 22 |
| 23 | 66.247                      | 0.0151                                | 0.00307                                 | 0.20307  | 326.237                                 | 4.925                                   | 23 |
| 24 | 79.497                      | 0.0126                                | 0.00255                                 | 0.20255  | 392.484                                 | 4.937                                   | 24 |
| 25 | 95.394                      | 0.0105                                | 0.00212                                 | 0.20212  | 471.981                                 | 4.948                                   | 25 |
| 26 | 114.475                     | 0.0087                                | 0.00174                                 | 0.20174  | 567.377                                 | 4.954                                   | 26 |
| 27 | 137.370                     | 0.0073                                | 0.00147                                 | 0.20147  | 681.852                                 | 4.964                                   | 27 |
| 28 | 164.845                     | 0.0061                                | 0.00122                                 | 0.20122  | 819.223                                 | 4.970                                   | 28 |
| 29 | 197.813                     | 0.0051                                | 0.00102                                 | 0.20102  | 984.067                                 | 4.975                                   | 29 |
| 30 | 237.376                     | 0.0042                                | 0.00085                                 | 0.20085  | 1181.881                                | 4.979                                   | 30 |
| 31 | 284.851                     | 0.0035                                | 0.00070                                 | 0.20070  | 1419.257                                | 4.982                                   | 31 |
| 32 | 341.822                     | 0.0029                                | 0.00059                                 | 0.20059  | 1704.108                                | 4.985                                   | 32 |
| 33 | 410.186                     | 0.0024                                | 0.00049                                 | 0.20049  | 2045.930                                | 4.988                                   | 33 |
| 34 | 492.223                     | 0.0020                                | 0.00041                                 | 0.20041  | 2456.116                                | 4.990                                   | 34 |
| 35 | 590.668                     | 0.0017                                | 0.00034                                 | 0.20034  | 2946.334                                | 4.992                                   | 35 |
| 40 | 1469.771                    | 0.0007                                | 0.00014                                 | 0.20014  | 7343.9                                  | 4.997                                   | 40 |
| 45 | 3657.258                    | 0.0003                                | 0.00005                                 | 0.20005  | 18281.3                                 | 4.999                                   | 45 |
| 50 | 9100.427                    | 0.0001                                | 0.00002                                 | 0.20002  | 46497.1                                 | 4.999                                   | 50 |
| ∞  |                             |                                       |   | 0.20000  |   | 5.000                                   | ∞  |

Table - 20

## ANNEXURE 'C'—(Contd.)

TABLE 20

Capital Recovery Factors for Interest Rate from 25% to 50%

| n  | 25%     | 30%     | 35%     | 40%     | 45%     | 50%     | n  |
|----|---------|---------|---------|---------|---------|---------|----|
| 1  | 1.25000 | 1.30000 | 1.35000 | 1.40000 | 1.45000 | 1.50000 | 1  |
| 2  | 0.69444 | 0.73679 | 0.77553 | 0.81657 | 0.85816 | 0.90000 | 2  |
| 3  | 0.51230 | 0.55063 | 0.58966 | 0.62936 | 0.66966 | 0.71053 | 3  |
| 4  | 0.42344 | 0.46163 | 0.50076 | 0.54077 | 0.58156 | 0.62306 | 4  |
| 5  | 0.37169 | 0.41058 | 0.45046 | 0.49126 | 0.53318 | 0.57583 | 5  |
| 6  | 0.33282 | 0.37239 | 0.41296 | 0.45426 | 0.49626 | 0.53892 | 6  |
| 7  | 0.31634 | 0.35687 | 0.39880 | 0.44192 | 0.48627 | 0.53108 | 7  |
| 8  | 0.30240 | 0.34192 | 0.38489 | 0.42907 | 0.47427 | 0.52030 | 8  |
| 9  | 0.28976 | 0.32824 | 0.37119 | 0.41634 | 0.46244 | 0.51335 | 9  |
| 10 | 0.28037 | 0.31746 | 0.35832 | 0.40132 | 0.44723 | 0.50887 | 10 |
| 11 | 0.27249 | 0.30773 | 0.34639 | 0.40133 | 0.44726 | 0.50585 | 11 |
| 12 | 0.26495 | 0.31145 | 0.34882 | 0.40718 | 0.45327 | 0.50388 | 12 |
| 13 | 0.26454 | 0.31024 | 0.34722 | 0.40510 | 0.45162 | 0.50258 | 13 |
| 14 | 0.26150 | 0.30782 | 0.34532 | 0.40363 | 0.45049 | 0.50172 | 14 |
| 15 | 0.25912 | 0.30598 | 0.34393 | 0.40259 | 0.44972 | 0.50114 | 15 |
| 16 | 0.25724 | 0.30458 | 0.34290 | 0.40185 | 0.44918 | 0.50074 | 16 |
| 17 | 0.25576 | 0.30351 | 0.34214 | 0.40132 | 0.44881 | 0.50051 | 17 |
| 18 | 0.25459 | 0.30269 | 0.34158 | 0.40094 | 0.44856 | 0.50034 | 18 |
| 19 | 0.25366 | 0.30207 | 0.34117 | 0.40067 | 0.44839 | 0.50023 | 19 |
| 20 | 0.25292 | 0.30159 | 0.34087 | 0.40048 | 0.44827 | 0.50015 | 20 |
| 21 | 0.25233 | 0.30122 | 0.34064 | 0.40034 | 0.44818 | 0.50010 | 21 |
| 22 | 0.25186 | 0.30094 | 0.34048 | 0.40024 | 0.44813 | 0.50007 | 22 |
| 23 | 0.25148 | 0.30072 | 0.34035 | 0.40017 | 0.44809 | 0.50004 | 23 |
| 24 | 0.25119 | 0.30055 | 0.34026 | 0.40012 | 0.44806 | 0.50003 | 24 |
| 25 | 0.25095 | 0.30043 | 0.34019 | 0.40009 | 0.44804 | 0.50002 | 25 |
| 26 | 0.25076 | 0.30033 | 0.34014 | 0.40006 | 0.44803 | 0.50001 | 26 |
| 27 | 0.25061 | 0.30025 | 0.34011 | 0.40005 | 0.44802 | 0.50001 | 27 |
| 28 | 0.25048 | 0.30019 | 0.34008 | 0.40003 | 0.44801 | 0.50001 | 28 |
| 29 | 0.25039 | 0.30015 | 0.34006 | 0.40002 | 0.44801 | 0.50000 | 29 |
| 30 | 0.25031 | 0.30011 | 0.34004 | 0.40002 | 0.44801 | 0.50000 | 30 |
| 31 | 0.25025 | 0.30009 | 0.34003 | 0.40001 | 0.44800 | 0.50000 | 31 |
| 32 | 0.25020 | 0.30007 | 0.34002 | 0.40001 | 0.44800 | 0.50000 | 32 |
| 33 | 0.25016 | 0.30005 | 0.34002 | 0.40001 | 0.44800 | 0.50000 | 33 |
| 34 | 0.25013 | 0.30004 | 0.34001 | 0.40000 | 0.44800 | 0.50000 | 34 |
| 35 | 0.25010 | 0.30003 | 0.34001 | 0.40000 | 0.44800 | 0.50000 | 35 |
| ∞  | 0.25000 | 0.30000 | 0.34000 | 0.40000 | 0.44800 | 0.50000 | ∞  |

Table - 21

ANNEXURE 'C'—(Contd.)

TABLE 21

Single Payment Present Worth Factors for Interest Rates from 25% to 50%

| n  | 25%    | 30%    | 35%    | 40%    | 45%    | 50%    | n  |
|----|--------|--------|--------|--------|--------|--------|----|
| 1  | 0.8000 | 0.7692 | 0.7407 | 0.7143 | 0.6897 | 0.6667 | 1  |
| 2  | 0.6400 | 0.5917 | 0.5487 | 0.5102 | 0.4756 | 0.4444 | 2  |
| 3  | 0.5120 | 0.4552 | 0.4064 | 0.3644 | 0.3289 | 0.2963 | 3  |
| 4  | 0.4096 | 0.3501 | 0.3011 | 0.2603 | 0.2262 | 0.1975 | 4  |
| 5  | 0.3277 | 0.2693 | 0.2230 | 0.1859 | 0.1560 | 0.1317 | 5  |
| 6  | 0.2621 | 0.2072 | 0.1652 | 0.1328 | 0.1076 | 0.0878 | 6  |
| 7  | 0.2097 | 0.1594 | 0.1224 | 0.0949 | 0.0742 | 0.0585 | 7  |
| 8  | 0.1678 | 0.1226 | 0.0906 | 0.0678 | 0.0512 | 0.0390 | 8  |
| 9  | 0.1342 | 0.0943 | 0.0671 | 0.0484 | 0.0353 | 0.0260 | 9  |
| 10 | 0.1074 | 0.0725 | 0.0497 | 0.0346 | 0.0243 | 0.0173 | 10 |
| 11 | 0.0859 | 0.0558 | 0.0368 | 0.0247 | 0.0168 | 0.0116 | 11 |
| 12 | 0.0687 | 0.0429 | 0.0273 | 0.0176 | 0.0116 | 0.0077 | 12 |
| 13 | 0.0550 | 0.0330 | 0.0202 | 0.0126 | 0.0080 | 0.0051 | 13 |
| 14 | 0.0440 | 0.0254 | 0.0150 | 0.0090 | 0.0055 | 0.0034 | 14 |
| 15 | 0.0352 | 0.0195 | 0.0111 | 0.0064 | 0.0038 | 0.0023 | 15 |
| 16 | 0.0281 | 0.0150 | 0.0082 | 0.0046 | 0.0026 | 0.0015 | 16 |
| 17 | 0.0225 | 0.0116 | 0.0061 | 0.0033 | 0.0018 | 0.0010 | 17 |
| 18 | 0.0180 | 0.0089 | 0.0045 | 0.0023 | 0.0012 | 0.0007 | 18 |
| 19 | 0.0144 | 0.0068 | 0.0033 | 0.0017 | 0.0009 | 0.0005 | 19 |
| 20 | 0.0115 | 0.0053 | 0.0025 | 0.0012 | 0.0006 | 0.0003 | 20 |
| 21 | 0.0092 | 0.0040 | 0.0018 | 0.0009 | 0.0004 | 0.0002 | 21 |
| 22 | 0.0074 | 0.0031 | 0.0014 | 0.0006 | 0.0003 | 0.0001 | 22 |
| 23 | 0.0059 | 0.0024 | 0.0010 | 0.0004 | 0.0002 | 0.0001 | 23 |
| 24 | 0.0047 | 0.0018 | 0.0007 | 0.0003 | 0.0001 | 0.0001 | 24 |
| 25 | 0.0038 | 0.0014 | 0.0006 | 0.0002 | 0.0001 | ..     | 25 |
| 26 | 0.0030 | 0.0011 | 0.0004 | 0.0002 | 0.0001 | ..     | 26 |
| 27 | 0.0024 | 0.0008 | 0.0003 | 0.0001 | ..     | ..     | 27 |
| 28 | 0.0019 | 0.0006 | 0.0002 | 0.0001 | ..     | ..     | 28 |
| 29 | 0.0015 | 0.0005 | 0.0002 | 0.0001 | ..     | ..     | 29 |
| 30 | 0.0012 | 0.0004 | 0.0001 | ..     | ..     | ..     | 30 |
| 31 | 0.0010 | 0.0003 | 0.0001 | ..     | ..     | ..     | 31 |
| 32 | 0.0008 | 0.0002 | 0.0001 | ..     | ..     | ..     | 32 |
| 33 | 0.0006 | 0.0002 | 0.0001 | ..     | ..     | ..     | 33 |
| 34 | 0.0005 | 0.0001 | ..     | ..     | ..     | ..     | 34 |
| 35 | 0.0004 | 0.0001 | ..     | ..     | ..     | ..     | 35 |



Table – 22

ANNEXURE 'C'—(Concl.)

TABLE 22

Series Present Worth Factors for Interest Rates from 25% to 50%

| n  | 25%   | 30%   | 35%   | 40%   | 45%   | 50%   | n  |
|----|-------|-------|-------|-------|-------|-------|----|
| 1  | 0.800 | 0.769 | 0.741 | 0.714 | 0.690 | 0.667 | 1  |
| 2  | 1.440 | 1.361 | 1.289 | 1.224 | 1.165 | 1.111 | 2  |
| 3  | 1.932 | 1.816 | 1.696 | 1.587 | 1.493 | 1.407 | 3  |
| 4  | 2.362 | 2.164 | 1.997 | 1.849 | 1.720 | 1.605 | 4  |
| 5  | 2.689 | 2.436 | 2.220 | 2.035 | 1.876 | 1.737 | 5  |
| 6  | 2.951 | 2.643 | 2.385 | 2.168 | 1.983 | 1.824 | 6  |
| 7  | 3.161 | 2.802 | 2.507 | 2.263 | 2.057 | 1.883 | 7  |
| 8  | 3.329 | 2.925 | 2.598 | 2.331 | 2.109 | 1.922 | 8  |
| 9  | 3.463 | 3.019 | 2.665 | 2.379 | 2.144 | 1.948 | 9  |
| 10 | 3.571 | 3.092 | 2.715 | 2.414 | 2.168 | 1.965 | 10 |
| 11 | 3.656 | 3.147 | 2.752 | 2.438 | 2.188 | 1.977 | 11 |
| 12 | 3.725 | 3.190 | 2.779 | 2.456 | 2.196 | 1.985 | 12 |
| 13 | 3.780 | 3.223 | 2.799 | 2.469 | 2.204 | 1.990 | 13 |
| 14 | 3.824 | 3.249 | 2.814 | 2.478 | 2.210 | 1.993 | 14 |
| 15 | 3.859 | 3.268 | 2.825 | 2.484 | 2.214 | 1.995 | 15 |
| 16 | 3.887 | 3.282 | 2.834 | 2.489 | 2.216 | 1.997 | 16 |
| 17 | 3.910 | 3.295 | 2.840 | 2.492 | 2.218 | 1.998 | 17 |
| 18 | 3.928 | 3.304 | 2.844 | 2.494 | 2.219 | 1.999 | 18 |
| 19 | 3.942 | 3.311 | 2.848 | 2.496 | 2.220 | 1.999 | 19 |
| 20 | 3.954 | 3.316 | 2.850 | 2.497 | 2.221 | 1.999 | 20 |
| 21 | 3.963 | 3.319 | 2.852 | 2.498 | 2.221 | 2.000 | 21 |
| 22 | 3.970 | 3.323 | 2.853 | 2.498 | 2.222 | 2.000 | 22 |
| 23 | 3.976 | 3.325 | 2.854 | 2.499 | 2.222 | 2.000 | 23 |
| 24 | 3.981 | 3.327 | 2.855 | 2.499 | 2.222 | 2.000 | 24 |
| 25 | 3.985 | 3.329 | 2.856 | 2.499 | 2.222 | 2.000 | 25 |
| 26 | 3.988 | 3.330 | 2.856 | 2.500 | 2.222 | 2.000 | 26 |
| 27 | 3.990 | 3.331 | 2.856 | 2.500 | 2.222 | 2.000 | 27 |
| 28 | 3.992 | 3.331 | 2.857 | 2.500 | 2.222 | 2.000 | 28 |
| 29 | 3.994 | 3.332 | 2.857 | 2.500 | 2.222 | 2.000 | 29 |
| 30 | 3.995 | 3.332 | 2.857 | 2.500 | 2.222 | 2.000 | 30 |
| 31 | 3.996 | 3.332 | 2.857 | 2.500 | 2.222 | 2.000 | 31 |
| 32 | 3.997 | 3.333 | 2.857 | 2.500 | 2.222 | 2.000 | 32 |
| 33 | 3.997 | 3.333 | 2.857 | 2.500 | 2.222 | 2.000 | 33 |
| 34 | 3.998 | 3.333 | 2.857 | 2.500 | 2.222 | 2.000 | 34 |
| 35 | 3.998 | 3.333 | 2.857 | 2.500 | 2.222 | 2.000 | 35 |
| ∞  | 4.000 | 3.333 | 2.857 | 2.500 | 2.222 | 2.000 | ∞  |

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**ANNEXURE 'D'**  
**RATE OF RETURN- USING DISCOUNTED CASH FLOW METHOD**

To simplify calculations, a project evaluation sheet (Exhibit I) together with an Interpolation Chart (Exhibit II) has been prepared to obtain rate of return using the discounted cash flow method.

**Procedure-** Using project evaluation sheet:

- (a) In column Trial I enter as disbursements the net estimated investment by years. Enter estimated annual returns for the years in which they will occur, and include terminal salvage value (if any) as a return in the year in which it will be realized.
- (b) Total the disbursements and the annual returns for trial I and enter the results in A and B lines respectively.
- (c) To obtain the interest rate which equates the present value of the disbursements and annual returns, calculate their present worth in trials 2,3,4 and 5 by multiplying the amounts in trial I by the factors indicated in trials 2 to 5. Add columns to obtain totals A and B.
- (d) Calculate the ratio of A to B for each trial by dividing the total present worth of disbursements, Totals (A), by the total present worth of annual returns, Totals (B).

Note .--- Trial 5 should be completed only if trial 4 has a ratio of A to B less than 1

- (e) On interpolation chart, plot ratios A/B against the trial rate at which they were calculated.
- (f) Join points with a smooth curve and read rate of return on the vertical axis opposite the intersection of the smooth curve with the vertical line representing a ratio of A to B of I. This is the interest rate which equates the present value of investments with the present value of annual returns.

Note. If a smooth curve does not result from joining the four points plotted, an error has been made in calculations or plotting. A minimum of 4 points is, therefore, necessary to check accuracy.

**Exhibit I**

**PROJECT EVALUATION SHEET**

| Timing               | Trial 1<br>0% Int.<br>Rate | Trial 2<br>10% Int. Rate |               | Trial 3<br>25% Int. Rate |               | Trial 4<br>40% Int. Rate |               | Trial 5<br>60% Int. Rate |               |
|----------------------|----------------------------|--------------------------|---------------|--------------------------|---------------|--------------------------|---------------|--------------------------|---------------|
| Period               | Disbursement               | Factor                   | Present worth | Factor                   | Present worth | Factor                   | Present worth | Factor                   | Present worth |
| 5 <sup>th</sup> Year | ..                         | 1.46                     |               | 2.44                     |               | 3.84                     |               | 6.56                     |               |
| 4 <sup>th</sup>      | ..                         | 1.33                     |               | 1.95                     |               | 2.74                     |               | 4.10                     |               |
| 3 <sup>rd</sup>      | ..                         | 1.21                     |               | 1.56                     |               | 1.96                     |               | 2.56                     |               |
| 2 <sup>nd</sup>      | ..                         | 1.10                     |               | 1.25                     |               | 1.40                     |               | 1.60                     |               |
| 1 <sup>st</sup>      | ..                         | 1.00                     |               | 1.00                     |               | 1.00                     |               | 1.00                     |               |
| Totals (A)           |                            | ...                      |               |                          |               |                          |               |                          |               |

**ANNEXURE 'D' –(Concl.)**

| Period | Annual Return | Factor | Present | Factor | Present | Factor | Present | Factor | Present |
|--------|---------------|--------|---------|--------|---------|--------|---------|--------|---------|
|--------|---------------|--------|---------|--------|---------|--------|---------|--------|---------|

|                      |    |                  |       |                  |       |                  |       |                  |       |
|----------------------|----|------------------|-------|------------------|-------|------------------|-------|------------------|-------|
|                      |    |                  | worth |                  | worth |                  | worth |                  | worth |
|                      |    | 10% Int.<br>Rate |       | 25% Int.<br>Rate |       | 40% Int.<br>Rate |       | 60% Int.<br>Rate |       |
| 1 <sup>st</sup> Year | .. | .91              |       | .80              |       | .71              |       | .63              |       |
| 2 <sup>nd</sup>      | .. | .83              |       | .64              |       | .51              |       | .39              |       |
| 3 <sup>rd</sup>      | .. | .75              |       | .51              |       | .36              |       | .24              |       |
| 4 <sup>th</sup>      | .. | .68              |       | .41              |       | .26              |       | .15              |       |
| 5 <sup>th</sup>      | .. | .62              |       | .33              |       | .19              |       | .10              |       |
| 6 <sup>th</sup>      | .. | .56              |       | .26              |       | .13              |       | .06              |       |
| 7 <sup>th</sup>      | .. | .51              |       | .21              |       | .09              |       | .04              |       |
| 8 <sup>th</sup>      | .. | .47              |       | .17              |       | .07              |       | .02              |       |
| 9 <sup>th</sup>      | .. | .42              |       | .13              |       | .05              |       | .01              |       |
| 10 <sup>th</sup>     | .. | .39              |       | .11              |       | .03              |       | .01              |       |
| 11 <sup>th</sup>     | .. | .35              |       | .09              |       | .02              |       | .01              |       |
| 12 <sup>th</sup>     | .. | .32              |       | .07              |       | .02              |       |                  |       |
| 13 <sup>th</sup>     | .. | .29              |       | .06              |       | .01              |       |                  |       |
| 14 <sup>th</sup>     | .. | .26              |       | .04              |       | .01              |       |                  |       |
| 15 <sup>th</sup>     | .. | .24              |       | .04              |       |                  |       |                  |       |
| 16 <sup>th</sup>     | .. | .22              |       | .03              |       |                  |       |                  |       |
| 17 <sup>th</sup>     | .. | .20              |       | .02              |       |                  |       |                  |       |
| 18 <sup>th</sup>     | .. | .18              |       | .02              |       |                  |       |                  |       |
| 19 <sup>th</sup>     | .. | .16              |       | .01              |       |                  |       |                  |       |
| 20 <sup>th</sup>     | .. | .15              |       | .01              |       |                  |       |                  |       |
| 21 <sup>st</sup>     | .. | .14              |       |                  |       |                  |       |                  |       |
| 22 <sup>nd</sup>     | .. | .12              |       |                  |       |                  |       |                  |       |
| 23 <sup>rd</sup>     | .. | .11              |       |                  |       |                  |       |                  |       |
| 24 <sup>th</sup>     | .. | .10              |       |                  |       |                  |       |                  |       |
| 25 <sup>th</sup>     | .. | .09              |       |                  |       |                  |       |                  |       |
| 26 <sup>th</sup>     | .. | .08              |       |                  |       |                  |       |                  |       |
| 27 <sup>th</sup>     | .. | .08              |       |                  |       |                  |       |                  |       |
| 28 <sup>th</sup>     | .. | .07              |       |                  |       |                  |       |                  |       |
| 29 <sup>th</sup>     | .. | .06              |       |                  |       |                  |       |                  |       |
| 30 <sup>th</sup>     | .. | .06              |       |                  |       |                  |       |                  |       |
| Totals (B)           |    |                  |       |                  |       |                  |       |                  |       |

## Exhibit II

## INTERPOLATION CHART

[illegible]

|  |   |     |  |  |     |  |  |     |  |     |  |     |  |     |  |     |  |  |
|--|---|-----|--|--|-----|--|--|-----|--|-----|--|-----|--|-----|--|-----|--|--|
|  | 5 |     |  |  |     |  |  |     |  |     |  |     |  |     |  |     |  |  |
|  | 0 |     |  |  |     |  |  |     |  |     |  |     |  |     |  |     |  |  |
|  | 0 | 0.5 |  |  | 1.0 |  |  | 1.5 |  | 2.0 |  | 2.5 |  | 3.0 |  | 3.5 |  |  |

**RATIO A/B**

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## ANNEXURE 'F'

### ECONOMIC EVALUATION OF RAILWAY INVESTMENTS

A purely financial appraisal of investment proposals does not necessarily lead to the selection of projects which best serve the needs of the community. The inadequacy of financial analysis in this regard derives from the fact that projected cash inflows and outflows associated with feasible investment alternatives do not correctly reflect the actual benefits to the community flowing from them or the costs that they impose on the economy. Financial and economic appraisals, however, need not always lead to conflicting decisions a financially viable project will also be acceptable on economic grounds whenever the economic return on investment is likely to be at least as high as its financial yield. But, there can be instances of financially sound investment proposals which may not turn out to be worthwhile propositions because the relevant cash outflows do not include all the associated costs to the economy. Again, an investment which is not expected to be profitable, may still yield an adequate, or even a fairly high, economic return if the projected cash earnings represent only a part of the benefits or incomes that are likely to be generated by it.

2. Economic benefits attributable to a particular investment can, for a number of reasons, exceed the revenues directly accruing to the Railways in the form of fare and freight receipts. In the first place, most users of a facility may be willing and able to pay somewhat more than what they are actually charged by the Railways. Secondly, there may also be instances where what the consumers are actually able to pay for rail transportation is (because of uneven-income distribution) less than the benefit they derive from it. This, indeed, is the main justification for a preferential fare structure for certain passenger and suburban services. Finally, for economic or social policy reasons freight rates on certain key commodities may be set at levels which do not fully cover rail transportation costs. The entire benefit derived by the users of Railways can never be quantified; however, at least that part of it which consists of the difference between cost of transportation and fares or freight rates actually charged-can be precisely ascertained ([Remarks I](#)). The provision of a rail transport facility thus directly adds to the well-being of the community by more than the receipts that accrue thereby to the Railways.

3. Rail transportation, however, can make a substantial indirect contribution as well to general well-being by facilitating economic expansion. A new line, in a backward region not well endowed with alternative modes of transportation, stimulates the growth of output and employment by widening the market for local products as well as by creating a market for some hitherto unexploited natural resource. The quantification of such indirect benefits can at best be approximative. For one thing, the expected expansion of regional or local economic activity is difficult to forecast. For another, the quantification of "developmental benefits" poses the problem of allocating expected additions to output and incomes between the Railway project and other complementary investments in industry, agriculture or commerce.

4. Great care should be taken in estimating social benefits for the purpose of economic appraisal of railway investments. Such benefits should, to the extent possible, be quantified with a reasonable degree of accuracy. Thorough investigations at the traffic survey stage would help in identifying the "developmental effects" and in estimating broadly the magnitude of the complementary investments that may be required. Also, the assumptions and reasons underlying any judgement about non-quantifiable benefits, should be clearly spelt out. Fortunately, the assessment of social benefits is necessary only in the case of proposed investments in new rail lines or operations ; as regards investment for modernisation and improvement, which constitute the bulk of the Railways' capital outlay, one need only estimate the social costs entailed by investment alternatives in order to pick out the least cost solution from the point of view of the economy.

5. The expenditure flows associated with Railway projects can, to varying extents, diverge from the cost to the economy of acquiring resources needed for their implementation and operation. The prices at which certain inputs and resources are made available to the Railways, for instance, may understate or exaggerate their real cost to the economy. Thus, the interest rate which is in line with the usual return on new capital

investment in the economy may not be the same as the "dividend" the Railways have to pay on the capital-at-charge. Similarly, the rupee equivalent of direct foreign exchange expenditure may differ from the cost of saving or earning an equivalent amount of foreign exchange. Moreover, the relative prices of various types of equipment and materials purchased by the Railways will be different from the comparative costs of producing them for the reason that the rates of indirect taxes (or subsidies) vary from product to product. Lastly, there are certain types of real costs which do not at all get recorded in the financial cash flows. Environmental damage can, for example, be a major unrecorded element of cost.

6. In selecting investments which impose the least cost on the economy, cash outflows have to be recomputed in such a way as to minimise the distortions caused by the use of prices actually paid for inputs (including the prices of capital and foreign exchange) and by the neglect of other costs which do not figure at all in expenses. Environmental effects of investments are the most difficult to estimate. However, in a number of cases the choice of projects may be influenced much more by the interest and exchange rate, that are utilised than by the correction of distortions introduced by indirect taxes, subsidies and environmental effects. A preliminary sensitivity analysis is useful for picking out the more important. of the factors distorting costs; such factors can then be subjected to a detailed investigation.

7. For economic evaluation of Railway Projects, the interest or discount rate is currently set at 10 percent. This implies that the cost of capital comprises a depreciation or capital recovery factor and interest charged at 10 per cent per annum; a project is thus just acceptable if the expected earnings from it during its lifetime make it possible to recover the investment with a return of 10 per cent per annum, that is, if the DCF rate of return on it is 10 percent.

8. In the cash flows utilised for economic evaluation of high speed diesel oil is not valued at the price actually paid by the Railways for it. Instead, all taxes and duties payable on it are excluded from the price; and, the duty-free price is adjusted upwards so as to allow for the comparative scarcity of crude oil in the Indian economy. At present, this adjustment factor is exactly half the current rate of excise duty on high-speed diesel oil.

9. There is no direct readjustment of the official exchange rate for the purpose of computing the scarcity value of imported equipments, spares and materials. However, there is an implicit adjustment in as much as the duty paid on imports is retained as a cost item in the cash-flows ideally, other indirect taxes like excise duties, sales taxes, local taxes and other cesses and levies, should be excluded from the cost of domestically procured inputs. But in many cases it has been found, particularly in the analysis of investment for modernisation of traction, that the exclusion of indirect taxes and similar levies does not make any material difference to the ranking of the proposed alternatives.

10. Electric power is valued not at the price at which it is sold to the Railways by the State Electricity Boards but at its estimated cost to the economy. The latter is derived from actual production cost by revaluing its interest component at the rate of 10 per cent per annum and its foreign exchange component at an exchange rate 33 percent-higher than the current official rupee price of foreign currencies.

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## **FINANCIAL AND ECONOMIC EVALUATION OF INVESTMENT ALTERNATIVES**

### **An Example.**

A highly simplified hypothetical example of choice between diesel and electric traction is presented here for the purpose of illustrating the essential difference between financial and economic evaluation. This type of choice is basically a problem of minimising the cost of handling a given volume of traffic over specified sections.

The two project alternatives, dieselisation and electrification, are defined as follows-

- (i) The project life, which includes the construction period, extends in both cases up to 44 years.
- (ii) The level of traffic remains unchanged over the life time of the project.
- (iii) Annual operating expenses exclude depreciation and do not vary from one year to another.
- (iv) Capital costs exclude interest during construction ([Remark II](#))
- (v) Capital outlay on dieselisation is spread over a period of three years; it comprises the expenditure on acquisition of rolling stock and construction of sheds.
- (vi) Capital outlay on electrification is phased over four years; it comprises the expenditure on rolling stock and construction of OHE.

Given these assumptions, the financial cost cash-flows associated with the two illustrative traction alternatives can be presented in the following manner :

| Financial cost to Railways                      |        | (Rs. crores). |
|---|--------|---------------|
| Year  | Diesel | Electric      |
| 1   | ..     | 3.0           |
| 2   | 0.5    | 6.0           |
| 3   | 0.5    | 15.0          |
| 4   | 10.0   | 6.0           |
| 5 <sup>th</sup> to 44 <sup>th</sup> (each year) | 4.0    | 2.5           |

#### Discounted Present Worth of Financial Costs.

| Interest Rate. | Diesel | Electric |
|----------------|--------|----------|
| 6%             | 56.5   | 55.3     |
| 7%             | 49.2   | 50.3     |

It would be seen that when discounted at 6 per cent the present worth of the financial cost flow relating to electrification works out to be lower than that of the financial cost flow associated with dieselisation by Rs. 1.2 crores. But the situation is reversed when the cost flows are discounted at 7 per cent, in which case dieselisation turns out to be cheaper by Rs. 1.1 crores. Thus, in this hypothetical case, the depreciation inclusive financial cost of electrification is lower only at rates of interest below 7 per cent. The rate of interest at which the two alternatives will impose identical costs can be found out by linear interpolation. This turns out to be 6.5 percent; at lower rates of interest electrification is the cheaper alternative; but becomes the costlier one at interest rates exceeding 6.5 per cent. This is as it should be; for electrification is the more capital intensive mode of traction.

The estimation of cash-flows relevant for the computation of the cost to the economy is based on the following assumptions :-

- (i) The basic price, inflated to the extent of 50 per cent of the excise duty, is taken as the appropriate scarcity value of high-speed diesel oil.
- (ii) The cost to the economy of electricity generation and transmission is assumed to be 7 paise per KWH as compared to 10 paise per KWH assumed to be actually paid by the Railways.
- (iii) Fuel costs constitute 70 per cent of operating expenses under diesel and 50 per cent of operating expenses under electric traction.

Under these assumptions, the cost to the economy of the uniform annual operating expenses associated with dieselisation and electrification works out to be Rs. 3.00 and Rs. 2.12 crores respectively. But, the cost to the economy of capital outlays continues to be the same as the financial cost. The discounted present worth of the cash flow corresponding to the cost to the economy at 3 and 4 percent interest rates is as follows:

Discounted Present Worth of Costs to the Economy.

| Interest Rate | Diesel | Electric |
|---------------|--------|----------|
| 3%            | 71.4   | 70.8     |
| 4%            | 60.2   | 62.4     |

It will be seen from the above that in this hypothetical case, from the point of view of cost to the economy, electrification turns out to be cheaper than dieselisation only at rates of interest which do not exceed 4 per cent. The break even rate of interest, at which both alternatives involve identical costs, is approximately 3.2 per cent.

**Remarks I** - Likewise, the difference between the cost to the consumer of rail transportation and that of other modes of transport replaced (partly or wholly) by it is a tangible and measurable social gain.

**Remarks II**- If the income flows are computed from the date of completion of the project, the capital outlay will be compounded at the desired interest rate.

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## ANNEXURE 'E'

EXAMPLE (I) :-

Yard re-modeling and provision of crossing stations on X-Y section of N. Railway.

|                              |               |
|------------------------------|---------------|
| Estimated capital cost       | Rs. 27,56,000 |
| Interest during construction | Rs. 3,93,011  |
| Total                        | Rs. 31,49,011 |

Financial Implications-

Earnings in 1976-77-

| (i) Additional traffic expected- |          | Wagon per day |         |
|----------------------------------|----------|---------------|---------|
|                                  |          | 1976-77       | 1977-78 |
| Inward                           | LSHS     | 28            | 38      |
|                                  | Coal     | 20            | 27      |
|                                  |          | 48            | 65      |
| Outward                          |          | 38            | 50      |
|                                  | G. Total | 86            | 115     |

|       |  |  |
|-------|--|--|
| (ii)  | Lead from X to Y   | 157 Km.                                  |
| (iii) | Average load per 4-wheeler LSHS/HSLS Other heavy merchandise | 18 tonnes in tank wagons<br>19.5 tonnes. |
|       | Coal.  | 21.3 tonnes.                             |
|       | Over all average load  | 19.5 tonnes.                             |
| (iv)  | Tare weight of a wagon                                       | 10 tonnes.                               |
| (v)   | Turn round on A Division                                     | 3.71 days.                               |
| (vi)  | Earnings per tonne.-<br>Fertilizer<br>Coal<br>LSHS/HSLS      | 4.71<br>3.26<br>8.33                     |

|       |                                  |   |  |
|-------|----------------------------------|---|--|
| (vii) | Earnings 1976-77 for entire year | = | Rs(28x18x8.33)+(20x21.3x3.26) + (38x19.5x4.71) |
|       |                                  |   | 100 100 100                                    |
|       |                                  | = | Rs 41.98 + 13.88 + 34.90                       |
|       |                                  | = | Rs. 157x365x90.76 = Rs. 52,01,001.80           |

| Cost of moving additional traffic-     |        |
|--|--------|
| (i) Traction                           | Diesel |
| (ii) Number of marshalling yard/yards  |        |
| (iii) Number of engine changing points |        |

|        |       |   |     |   |   |     |             |
|--------|-------|---|-----|---|---|-----|-------------|
|        | (iv)  | Total wagon days  |     | 365x86x3.71   | = |     | 116457      |
|        | (v)   | Total No. of wagons run loaded trip   |     | 365x86  | = |     | 31390       |
|        | (vi)  | Total No. of wagons run empty trip  |     | 365x66  | = |     | 24090       |
|        | (vii) | Documentation charges @ Rs 1.78 per invoice.  | Rs. | 31390x1.78  | = | Rs. | 55874.20    |
| (viii) |       | Other terminal charges @ Rs. 12.41 per wagon.   | Rs. | 31390x12.41   | = | Rs. | 389549.90   |
| (ix)   |       | Provision and maintenance of carrying units @ Rs1.49 per wagon per day  | Rs. | 116457x1.49   | = | Rs. | 173520.93   |
| (x)    | (a)   | GTKM for diesel engines loaded trip   | Rs. | 31390x29.5x157  | = | Rs. | 145382785   |
|        |       | Haulage charges @ Rs. 3.73 per 1000 GTKM.   | Rs. | $\frac{145382785 \times 3.73}{1000}$                    | = | Rs. | 5,42,277.78 |
|        | (b)   | GTKM for diesel engines empty trip  | Rs. | 24090x10x157  | = | Rs. | 37821300    |
|        |       | Haulage charges @ Rs. 3.73 per 1000 GTKM.   | Rs. | $\frac{37821300 \times 3.73}{1000}$                     | = | Rs. | 141073.45   |
|        | (c)   | Line haul (movement) service-other than transportation expenses, including train passing staff @ Rs. 1.53 per 1000 GTKM For loaded trip | Rs. | $\frac{31390 \times 29.5 \times 157 \times 1.53}{1000}$ | = | Rs. | 2,22,453.60 |
|        |       | --do--For empty trip.   | Rs. | $\frac{24090 \times 10 \times 157 \times 1.53}{1000}$   | = | Rs. | 57,866.59   |
|        | (d)   | Line Haul (movement) services cost of track and signalling @ Rs. 1.33 For loaded Trip   | Rs. | $\frac{31390 \times 29.5 \times 157 \times 1.33}{1000}$ | = | Rs. | 1,93,359.10 |
|        |       | For empty trip  | Rs. | $\frac{24090 \times 10 \times 157 \times 1.33}{1000}$   | = | Rs. | 50,302.33   |
|        | (e)   | Marshalling yard cost   | Nil |   |   |     |             |
|        | (f)   | Engine changing cost  | Nil |   |   |     |             |
|        | (g)   | Total haulage cost  | Rs. | 18,26,260.04  |   |     |             |
|        | (h)   | Add allowance for 10%   | Rs. | 20,08,886.04  |   |     |             |
|        | (i)   | Marginal cost @ 78%   | Rs. | 15,66,931.11  |   |     |             |

|  |     |   |     |              |  |  |  |
|--|-----|---|-----|--------------|--|--|--|
|  | (i) | Annual maintenance charges per first and subsequent years | Rs. | 1,14,564.00  |  |  |  |
|  |     | Total working expenses                                    | Rs. | 16,81,495.11 |  |  |  |

|                          |  |  |  |     |              |              |
|--------------------------|--|--|--|-----|--------------|--------------|
| Net earnings in 1976-77- |  |  |  |     |              |              |
| Earnings                 |  |  |  | Rs  | 52,01,001.80 |              |
| Working expenses         |  |  |  | (-) | Rs           | 16,81,495.11 |
| Net earnings per year    |  |  |  | Rs  | 35,19,506.69 |              |

|  |     |                                   |  |   |  |  |
|--|-----|-----------------------------------|--|---|--|--|
| Earnings in 1977-78 and onwards-   |     |                                   |  |   |  |  |
| (i) Earning per year   | Rs. | 157 x365                          | $\frac{(38 \times 18 \times 8.33)}{100}$ | + | $\frac{(27 \times 21.3 \times 3.26)}{100}$ | = $\frac{(50 \times 19.5 \times 4.17)}{100}$ |
|  | Rs. | 157x365x56.98 + 18.74 + 45.92     |  |   |  |  |
|  | Rs. | 157x365x121.64 = Rs. 69,70,580.20 |  |   |  |  |
| Cost of moving additional traffic  |     |                                   |  |   |  |  |
| (i) Total wagon days   |     |                                   | 365x115x3.71                             | = | 155727                                     |  |
| (ii) Total No. of wagons run- loaded trip                                    |     |                                   | 365x115                                  | = | 41975                                      |  |
| (iii) Total No. of wagons run- empty trip                                    |     |                                   | 365x85                                   | = | 31025                                      |  |
| (iv) Documentation charges @ Rs 1.78 per invoice.                            | Rs. | 41975x1.78                        |  | = | Rs.  | 74715.50                                     |
| (v) Other terminal charges @ Rs. 12.41 per wagon.                            | Rs. | 41975x12.41                       |  | = | Rs.  | 520902.75                                    |
| (vi) Provision and maintenance of carrying units @ Rs1.49 per wagon per day. | Rs. | 155727x1.49                       |  | = | Rs.  | 232033.23                                    |

|       |     |  |     |   |   |     |           |
|-------|-----|--|-----|---|---|-----|-----------|
| (vii) | (a) | GTKM for diesel engines- loaded trip   | Rs. | 41975x29.5x157  | = | Rs. | 194407212 |
|       |     | Haulage charges @ Rs. 3.73 per 1000/GTKM   | Rs. | $\frac{194407212 \times 3.73}{1000}$                    | = | Rs. | 725139    |
|       | (b) | GTKM for diesel engine empty trip  | Rs. | 31025x10x157  | = | Rs. | 48709250  |
|       |     | Haulage charges @ Rs. 3.73 per 1000/GTKM   | Rs. | $\frac{48709250 \times 3.73}{1000}$                     | = | Rs. | 181685.50 |
|       | (c) | Line haul (movement) service- other than transportation expenses including train passing staff @ Rs. 1.53 per 1000 GTKM: For loaded trip | Rs. | $\frac{41975 \times 29.5 \times 157 \times 1.53}{1000}$ | = | Rs. | 297443.00 |
|       |     | For empty trip   | Rs. | $\frac{51025 \times 10 \times 157 \times 1.53}{1000}$   | = | Rs. | 74525.15  |

|  |     |   |     |                             |   |     |           |
|--|-----|---|-----|-----------------------------|---|-----|-----------|
|  | (d) | Line Haul (movement) services:<br>For loaded trip                         | Rs. | 41975x29.5x157x1.33<br>1000 | = | Rs. | 258561.52 |
|  |     | cost of track and signalling trip @<br>Rs. 1.33<br>--do-- For empty trip. | Rs. | 31025x10x157x1.33<br>1000   | = | Rs. | 64,783.30 |

|     |                       |     |              |
|-----|-----------------------|-----|--------------|
| (e) | Marshalling yard cost | Nil |              |
| (f) | Engine changing cost  | Nil |              |
| (g) | Total haulage cost    | Rs. | 24,29,798.00 |
| (h) | Add allowance for 10% | Rs. | 26,72,775.00 |

|        |  |     |              |
|--------|--|-----|--------------|
| (viii) | Marginal cost @ 78%  | Rs. | 20,84,765.00 |
| (ix)   | Annual maintenance charges for first<br>and subsequent years | Rs. | 1,14,564.00  |
| (x)    | Total working expenses                                       | Rs. | 21,99,329.00 |
|        | Net earnings 1997-98 and onwards-                            |     |              |
|        | Earnings   | Rs. | 69,70,580.00 |
|        | Working expenses (-)   | Rs. | 21,99,329.00 |
|        | Net earnings per year  | Rs. | 47,71,251.00 |

| Rolling Stock Requirement in 1977-78 and onwards- |                                     |  |                                  |
|---|-------------------------------------|--|----------------------------------|
| (1)   | Diesel engines (cost Rs. 21,00,000) |  |                                  |
|   | (a)                                 | Average lead of a diesel engine                                | 65 wagons                        |
|   | (b)                                 | Lead from C to D   | 157 Km                           |
|   | (c)                                 | Total No. of trains per day 100/65                             | 1.5                              |
|   | (d)                                 | Train Kms. Per day   | 1.5x2x157 =471                   |
|   | (e)                                 | Engine Km. Per day per engine in use (diesel)                  | 387                              |
|   | (f)                                 | Bare No. of diesel engine required                             | 471/387 = 1.2                    |
|   | (g)                                 | Add for spares @ 6.96%   | 1.2 x $\frac{106.96}{100}$ =1.28 |
|   |                                     |  | Say 1.3                          |
|   | (h)                                 | Cost of 1.3 engines @ Rs. 21,00,000                            | Rs. 27,30,000                    |
| (ii)  |                                     | Covered wagons (Cost Rs.21,014).                               |                                  |
|   |                                     | Wagons required per day for carrying coal<br>for carrying urea | 27 (15 to be back loaded)<br>35  |
|   |                                     | Total  | 62                               |

Total bare number of covered wagons required (62x3.71 turn round) 230.02

Add spares @ Rs. 5.32%  $\frac{230.02 \times 105.32}{100}$  = 242.25  
Say 242



Rate of return by DCF method-

|  |     |             |
|--|-----|-------------|
| (i) Capital cost   | Rs. | 1,77,27,407 |
| (ii) Life of assets  |     | 30 Years    |
| (iii) Salvage value @ 10% (excluding earth work)                                   | Rs. | 2,17,413    |
| (iv) Net earnings 1976-77  | Rs. | 35,19,507   |
| Net earnings 1977-78   | Rs. | 47,71,251   |
| (v) Present worth calculations-  |     |             |
| @ 25% $(-177.27) + [(35.20) (0.8)] + [47.71 (3.995-0.8)] + [(2.17 \times 0.0012)]$ |     |             |
| - 177.27 + 28.16 + 152.43 + 0.0026   |     |             |
| - 177.27 + 180.59  |     |             |
| + 3.32   |     |             |

ROR is about 25%

Note - in this computation, at 25% discount rate 0.8 is the single payment PWF for the 1st Year, 3.995 is the PWF for uniform cash Flow in the 30<sup>th</sup> year 0.0012 is the PWF for Single payment in the 30<sup>th</sup> year.

#### EXAMPLE (2)

##### Economics of Dieselisation of the K.V. (N.G.) Railway

| A. Basic data—                                    | Diesel) | Steam | Difference (S-D) |
|---|---------|-------|------------------|
| Capital cost (Rs. Lacs)                           | 165.00  | 52.50 | -112.50          |
| Life (years)                                      | 30      | 40    |                  |
| Salvage value (Rs. Lacs)                          | 16.50   | 13.35 | -3.15            |
| Annual Operating Expenses excluding Depreciation- |         |       |                  |
| Fuel consumption                                  | 17.23   | 32.18 | +14.95           |
| Maintenance expenses                              | 6.32    | 6.29  | -0.03            |
| Running staff                                     | 4.71    | 7.59  | +2.88            |
| Annual cost                                       | 28.26   | 46.06 | 17.80            |

#### B. Rate of return on extra capital of diesels-

The extra capital over steam on diesel is Rs 112.5 lacs.

Calculate ROR by taking present worth of difference (S-D)

|                                   |   |   |
|-----------------------------------|---|---|
| PW at 12% of difference           | = | -112.5 + 17.8 (p w f 30 years at 12%)           |
|                                   | = | - 3.15 (p w f 30 years 12% S p)                 |
|                                   | = | -112.5 + 17.8 (8.055) - 3.15 (0.0334) = + 30.77 |
| PW at 15% of difference           | = | -112.5 + 17.8 (6.566) - 3.15 (0.0151) = + 4.33  |
| PW at 20% of difference           | = | -112.5 + 17.8 (4.979) - 3.15 (.0042) = -23.88   |
| Rate of return (by interpolation) | = | $\frac{15 + 4.33 \times 5}{28.21} = 15.8\%$     |

C. Conventional method of calculation\_

|     |                               |   |                                  |         |
|-----|-------------------------------|---|----------------------------------|---------|
| (a) | Annual cost                   | 28.26   | 46.06                            | 17.80   |
|     | Depreciation at 3.75%         |   |                                  |         |
|     | Sinking Fund                  | 2.79*   | 0.53 \$                          | -2.26   |
|     | Total Annual Costs            | 31.05   | 46.59                            | +15.54  |
|     |                               | * On capital cost less 10% salvage value.                 |                                  |         |
|     |                               | \$ On capital cost of Rs 52.5 lacs less 10% salvage value |                                  |         |
| (b) | Return on Capital:            |   |                                  |         |
|     | Net capital outlay (165-52.5) | =   | Rs. 112.5                        |         |
|     | Annual Recurring Savings      | =   | Rs. 15.54 lacs                   |         |
|     | Return on Capital             | =   | $\frac{\text{Rs. 15.54}}{112.5}$ | = 13.8% |

EXAMPLE (3):-

**Financial Benefits as a Result of saving in Detentions to Goods Trains and in Staff with the provision of Tokenless Block instruments on A-B Section**

|                              |  |  |                         |
|------------------------------|--|--|-------------------------|
| Estimated initial investment | Rs.20,80,000   |  |                         |
| (1) Crossing-                |  |  |                         |
| (a)                          | 17 diesel and 1 steam trains are being detained for 3.5 occasions for crossing and TOS per train and the saving in detention would be to the extent of 7 mts. per incidence per train. |  |                         |
| (i)                          | Diesel   | :  | 17x3.5x7 = 6 hrs,56 mts |
| (ii)                         | Steam  | :  | 1x3.5x7 = 24 mts        |
|                              | TOTAL  |  | = 7 hrs. 20 mts         |
| (b)                          | Token lost cases-  |  |                         |
|                              | 0.5 diesel train missed token and suffered detention of 14 mts. per train which will be eliminated:  |  |                         |
|                              | 0.5x14   | = 7 mts.   |                         |
| Total                        | Diesel   | a (i) + (b)  | = 7 hrs. 3 mts          |
|                              | Steam  | a (ii)   | 24 mts                  |
| Avg. load per Train          | Diesel   |  | 67 Wagon                |
|                              | Steam  |  | 45 Wagon                |
| (A) (a)                      | Wagon days saved (bare)  | $\frac{67 \times 7.05}{24} + \frac{45 \times 4}{24}$ | = 20                    |
| (b)                          | Add for spares @ 5.32% on 20 wagons  |  | = 1/21                  |



|       |     |  |             |        |
|-------|-----|--|-------------|--------|
| 2.(i) | (a) | Diesel engine hours saved                | 7.05        |        |
| )     | (b) | Effective engine hours daily             | 18.8        |        |
|       | (c) | Therefore bare No. of engine saved daily | <u>7.05</u> | = 0.37 |
|       |     |  | 18.8        |        |
|       | (d) | Add for spares @ 0.96%                   | <u>.03</u>  |        |
|       |     | Total                                    | 0.40        |        |
|       |     |  |             |        |
| (ii)  | (a) | Steam engine hours saved                 | .4          |        |
|       | (b) | Effective hours daily                    | 12 hours    |        |
|       | (c) | Bare No. of engine saved                 | <u>.4</u>   | = .03  |
|       |     |  | 12          |        |
|       | (d) | Add for spare @ 14.6%                    | <u>.004</u> |        |
|       |     | Total                                    | .03         |        |

|                                 |             |
|---------------------------------|-------------|
| Annual saving per wagon         | = Rs. 2418  |
| Annual saving per diesel engine | = Rs.778300 |
| Annual saving on steam engine   | = Rs.157166 |

|     |  |                    |
|-----|--|--------------------|
| (a) | Saving in respect of 21 wagons 21x2418 | = Rs.50778         |
| (b) | Saving in respect of 40 diesel         | = Rs.311320        |
| (c) | Saving in respect of .03 steam         | = Rs.4715          |
|     | Total                                  | <u>= Rs.366813</u> |

It is presumed that due to various difficulties in the day to day operation, saving at 80% only will be achieved on conservative estimate = Rs.293450

|     |   |              |
|-----|---|--------------|
| (2) | Annual maintenance expenses during the 1 <sup>st</sup> and subsequent years | = Rs. 21590  |
| (3) | Net saving (Rs.293450 – 21590)  | = Rs. 271860 |

The work is financially justified as shown below:

Annual rate of return by DCF method-

|       |  |                    |
|-------|--|--------------------|
| (i)   | Cost of the work including interest                                    | Rs.2267854         |
| (ii)  | Salvage value @ 10% (excluding interest)                               | Rs.208000          |
| (iii) | Life of assets (avg)   | 25 years           |
| (iv)  | Annual saving  | Rs.293450          |
| (v)   | Annual cost during first and subsequent years (excluding depreciation) | Rs.21590           |
| (vi)  | Net annual saving-   | Rs.2,93,450-21,590 |
|       |  | Rs.2,71,860        |

|     |  |        |        |
|-----|--|--------|--------|
|     |  | 10%    | 12%    |
| (4) | Present worth factor for uniform cash flow over 25 years         | 9.077  | 7.843  |
|     | Present worth factor for single Payment in 25 <sup>th</sup> year | 0.0923 | 0.0588 |

|            |   |              |   |                 |   |                   |   |          |
|------------|---|--------------|---|-----------------|---|-------------------|---|----------|
| NPV at 10% | = | (-22,67,854) | + | (2,71,860x9.077 | + | (2,08,000x0.0923) | = | 2,19,400 |
| NPV at 12% | = | (-22,67,854) | + | 2,71,860x7.843  | + | (2,08,000x0.0588) | = | 1,21,000 |

By interpolation:  $10\% + \frac{2.19 \times 2}{2.19 + 1.21} = 10\% + \frac{4.38}{3.40} = 11.13\%$  Which is the ROR under the DCF

|   | Increase | Decrease |
|---|----------|----------|
| 1. Annual repairs and maintenance charges on Rs.20,80,000/- @ 3%  | 62,400   | -        |
| 2. Annual repairs and maintenance charges on Rs.8,50,000/-@ 3%<br>(Present day cost)                                | -        | 25,500   |
| 3. Annual sinking fund on Rs.19,20,000/- less scrap value Rs.192000/- net<br>Rs.17,28,000/- @ 0.0249 (age 25 year)  | 43,027   | -        |
| 4. Annual sinking fund on Rs.1,60,000/- less scrap value Rs.16,000/- net<br>Rs.1,44,000/- @ 0.0676 (age 12 year)    | 9,734    | -        |
| 5. Annual sinking fund on Rs.1,60,000/- less scrap value Rs.16,000/- net<br>Rs.1,44,000/- @ 0.0249 ( age 25 years)  | -        | 3,586    |
| 6. Annual sinking fund on Rs.2,65,000/- less scrap value Rs.26,500/- net<br>Rs.2,38,500/- @ 0.0112 ( age 40 years)  | -        | 2,671    |
| 7. Saving in terms of wagons and engine detentions  | -        | 3,68,614 |
| 8. Saving in staff :-<br>2 Block Maintainer Gr.175-240 @ 436.51 = 10476<br>2 Khalasies Gr.70-85 @ 202.42 P.M.. 4834 | -        | 15,310   |
|   | 1,15,161 | 3,40,517 |

Details of interest @ 6% during 4 years period of construction:-

| Year                 | Outlay         | Interest  | Amount at the end of the year |
|----------------------|----------------|---|-------------------------------|
| 1 <sup>st</sup> year | 500000         | $\frac{(500000)}{2} \times \frac{6}{100}$           | 15000                         |
| 2 <sup>nd</sup> year | 1000000        | $\frac{(1000000)}{2} + 515000 \times \frac{6}{100}$ | 60900                         |
| 3 <sup>rd</sup> year | 580000         | $\frac{(580000)}{2} + 1575900 \times \frac{6}{100}$ | 111954                        |
|                      | <u>2080000</u> |   | <u>187854</u>                 |

EXAMPLE (4) :-

#### Provision of departmental line wires on A-B Section of X Railway.

Estimated initial cost : Rs.25.08 lakhs (including Rs.1.47 lakhs for staff quarters).

Outflow of cash during the Project Construction stage-

| Year | 0%                   | 6%                   | 10%       | 15%       |
|------|----------------------|----------------------|-----------|-----------|
| - 2  | (-) 6,00,000         | (-) 6,54,000         | --        | --        |
| - 1  | (-) 12,00,000        | (-) 12,72,000        | --        | --        |
| 0    | (-) 7,08,000         | (-) 7,08,000         | --        | --        |
|      | <u>(-) 25,08,000</u> | <u>(-) 26,34,000</u> | <u>--</u> | <u>--</u> |

NPV of the Project, assuming even cash flow of Rs.2,81,184 (details given below), at 10% over a life of 60 years will be  $2,81,184 \times 9.967 = 28,02,561$ .

As the NPV is more than the initial investment inclusive of interest during construction, the project is financially justified.

Details of the anticipated annual saving of Rs.2,81,184

Financial Implication:-

|   | <u>Increase</u> | <u>Decrease</u> |
|---|-----------------|-----------------|
| 1. Annual repairs and maintenance charges on Rs.25,08,000 @ 3%                  | 75,240          | -               |
| 2. Annual rental savings  |                 |                 |
| (a) Iron wire per mile @ Rs.54.23 x4 per conductor (136 miles)                  | -               | 29,501          |
| (b)Copper wire per mile @ Rs.72.27 x 4 per conductor (136miles)                 | -               | 39,314          |
| 3. Annual operational savings as per details attached                           | -               | 2,83,764        |
| 4. Financial implications arising out of Engg's portion as per details attached | -               | 3,845           |
| 5. Total  | <u>75,240</u>   | <u>3,56,424</u> |

Net saving during 1<sup>st</sup> and subsequent years = 3,56,424 – 75,240 = 2,81,184

#### Details of item 4 :-

|   | <u>Increased by</u> | <u>Decreased by</u> |
|---|---------------------|---------------------|
| Annual rent recoverable from type II quarters ( 7 units)            |                     |                     |
| $\frac{7 \times (110 + 380) \times 12}{2}$                          |                     |                     |
| @ 10%   | ...                 | 2,982               |
| Annual rent recoverable from staff of type I quarters<br>( 7 units) |                     |                     |
| $\frac{7 \times (70 + 110) + 47 \times 12}{4}$                      |                     |                     |
| @ 7.1/2%  | ....                | 863                 |
|   | ....                | <u>3,845</u>        |

Net annual increase during the first and the subsequent year = Rs.3845

#### Details of items 3

Details of operational savings -It is expected that with the provision of ACSR line wire, the control efficiency will be 90% and above. The efficiency below 90 is primarily due to copper wire thefts. During February, 1970 for 13 days the efficiency was 90% and above and average hours per train is 4 hrs-55 mts. as against 5 hrs-45 mts. per train during the balance of 15 days. The difference in the hours on road is 50 mts or .83 mts per train.

|   |                                   |       |
|---|-----------------------------------|-------|
| 1. Average number of trains (only Dn trains excluding one works train as per line capacity statement 1968-69) | =                                 | 13.1  |
| 2. Total T.G. accounted for   | =                                 | 370   |
| 3. Number of trains effected below 90% efficiency   | =                                 | 197   |
| 4. Percentage of trains effected to total trains accounted for  | = $\frac{197 \times 100}{370}$    | 53.24 |
| 5. Percentage of average trains effected to total T.G. running on section i.e. 13.1                           | = $\frac{53.24 \times 13.1}{100}$ | 6.97  |
| 6. Average load per train on branch line  | =                                 | 56    |

'A' Saving on wagons:-

|  |   |  |
|--|---|--|
| (a) No. of hours to be save                | = | 6.97x56x .83 wagon hrs.                |
| (b) Converting wagon hours into wagon days | = | $\frac{6.97 \times 56 \times .83}{24}$ |

|                              |   |  |
|------------------------------|---|--|
| (c) By adding spares @ 3.23% | = | $\frac{6.97 \times 56 \times .83}{24} \times \frac{103.23}{100} = 13.87$ |
| (d) Saving on one wagon      | = | Rs. 2229/-   |
| (e) Annual saving on 13.87   | = | $2229 \times 13.87 = \text{Rs.} 30916$                                   |

'B' Saving on engine :-

|   |   |  |
|---|---|--|
| (a) Total detention to be saved   | = | $6.97 \times .83$  |
| (b) Converting into No. of Diesel Engine @ 19.1 hrs.<br>(Daily effective hour)                | = | $\frac{6.97 \times .83}{19.1}$                                 |
| (c) By adding spare @ 8.22%   | = | $\frac{6.97 \times .83}{19.1} \times \frac{108.22}{100} = .32$ |
| (d) Saving on .32 engine @Rs.7,90,152(fraction of an<br>engine W/O interest and depreciation) | = | $790152 \times .32 = \text{Rs.} 2,52,848$                      |
| (e) Total saving of 'A' and 'B'   | = | $30916 + 252848 = \text{Rs.} 2,83,764$                         |

#### EXAMPLE (5):-

##### Provision of line capacity in M.G. section of 'X' Railway.

A section (82 Kms) is partially doubled in two patches over two stretches totalling 52 Kms. On the 30 Kms. long single line section, there are 4 block stations and all these stations have two reception lines at present thereby limiting the capacity of the stations either to crossing of a train or merely to give precedence at the station, both crossing and precedence cannot take place at the same time.

2. The traffic is expected to increase from 20 trains each way on the single line section at present to 24 trains in the course of a year or two. At the end of 5 years, one more passenger train and two goods trains are expected to be introduced, increasing the train density to 27 either way. As against the projected line capacity required at 80% utilization for the above level of traffic at 30 and 34 in the 1st and the 5<sup>th</sup> the year respectively, the line capacity at present is restricted to 27. All capacity calculations assume diesel traction.

3. The following alternative are being considered for increasing the line capacity to match the progressive traffic requirement :-

Alternative (1) : Doubling of the entire 30 Kms section - Cost Rs.1.90 crores; capacity 44 paths either way.

Alternative (2): Doubling the section in two phases:

- Immediate doubling of 20 Kms section - Cost Rs.1 crore; capacity 32 paths either way.
- Doubling of the remaining 10 Kms length at a cost of Rs.90 lakhs in 5<sup>th</sup> year - capacity 44 paths each way

Alternative (3): (a) Provision of one additional reception line at each of the 4 block stations at an approximate cost of Rs. 10 lakhs straightaway; capacity 30 paths each way.  
(b) Doubling of the entire 30 Kms section in 5<sup>th</sup> year-cost Rs.1.90 crores; capacity 44 paths each way.

The additional earnings likely to accrue on account of additional traffic worked out, commodity wise, as apportioned to the section in the 1<sup>st</sup> and the 5<sup>th</sup> years on the traffic projections for these years assuming the level of traffic to remain constant during this period and 5<sup>th</sup> year and beyond, are tabulated below :-

| Sr. No. | Commodities    | 1971-72 and<br>onwards | 1974-75 to 1975-<br>76 | 1976-77 and<br>onwards |
|---------|----------------|------------------------|------------------------|------------------------|
| 1.      | Cement         | 56,450                 | 1,25,823               | 1,95,197               |
| 2.      | Pulses         | 19,549                 | 46,149                 | 72,843                 |
| 3.      | Salt           | 1,28,745               | 2,37,120               | 3,45,495               |
| 4.      | Onions         | 15,626                 | 38,756                 | 61,887                 |
| 5.      | Rock Phosphate | 46,097                 | 1,23,315               | 2,00,534               |
| 6.      | Vegetable Oil  | 89,363                 | 1,69,253               | 2,49,143               |
| 7.      | POL            | 4,84,477               | 6,01,383               | 8,38,289               |
|         | <b>TOTAL</b>   | <b>8,40,307</b>        | <b>14,01,799</b>       | <b>19,63,288</b>       |

- (a) Plus 1 goods train.  
(b) Plus 1 + 1 = 2 goods train.  
(c) Plus 2 + 1 = 3 goods train.

4. The financial implications for the three alternatives worked out on the D.C.F. technique are given in the statements annexed. It may be pointed out that only goods earnings have been taken for working out the financial implications and unit cost data with interest has been applied.

#### Alternative (1)

Full Doubling:-

If doubling is done straightaway, the return comes to 8%. In this case the cash out-flow is Rs.1.90 crores during 1971-72 and 1972-73 while the cash in flow is at the level of 8,40,000 for 1971-72 to 1973-74, Rs.14,01,800 from 1974-75 to 1975-76 and Rs.19,63,000 for the remaining period 1976-77 to 2001-02.

| Year               | Cash flow           | Cumulative discount (8%) factor for |                 |                       |
|--------------------|---------------------|-------------------------------------|-----------------|-----------------------|
|                    |                     | 1 <sup>st</sup><br>Year             | Next 2<br>Years | Remaining<br>25 years |
| 1971-72            | 1,00,00,000         | -                                   | -               | -                     |
| 1972-73            | 90,00,000x.85       | -                                   | -               | -                     |
| 1971-72 to 1973-74 | 8,40,000 each year  | 2.57                                | -               | -                     |
| 1974-75 to 1975-76 | 14,01,800           | -                                   | 1.42            | -                     |
| 1976-77 to 2001-02 | 19,63,000 each year | -                                   | -               | 7.26                  |
|                    |                     |                                     |                 | <b>TOTAL</b>          |
|                    |                     |                                     |                 | <b>-100,00,000</b>    |
|                    |                     |                                     |                 | <b>-76,50,000</b>     |
|                    |                     |                                     |                 | <b>+21,58,000</b>     |
|                    |                     |                                     |                 | <b>+19,90,500</b>     |
|                    |                     |                                     |                 | <b>+142,51,000</b>    |
|                    |                     |                                     |                 | <b>+7,49,000</b>      |

Note: It is assumed that simultaneously with the doubling work in progress, it will be possible to carry the additional traffic in 1971-72 and 1972-73.

#### Alternative (2)

**Doubling in two Phases:**

In case the doubling is taken up in two Phases, the first phase of doubling A-B taken up immediately, i. e. in 1971-72, and the second phase viz, doubling of B-C taken up in 1976-77, the rate of return would be about 9% as worked out below:-

|                      |               |
|----------------------|---------------|
| Cost of first phase  | Rs.100,00,000 |
| Cost of second phase | Rs. 90,00,000 |

| Year               | Cash flow  | Cumulative discount(8%)            |              |                        | Present Value    |
|--------------------|------------|------------------------------------|--------------|------------------------|------------------|
|                    |            | Factor for 1 <sup>st</sup> 3 years | Next 2 years | For remaining 25 years |                  |
| 1971-72            | 100,00,000 | -                                  | -            | -                      | -100,00,000      |
| 1971-72 to 1973-74 | 8,40,000   | 2.57                               | -            | -                      | +21,58,000       |
| 1974-75 to 1975-76 | 14,01,800  | -                                  | 1.42         | -                      | +19,90,500       |
| 1976-77            | 90,00,000  | .68                                | -            | -                      | -61,20,000       |
| 1976-77 to 2006-07 | 19,63,000  | -                                  | -            | 7.26                   | +142,51,000      |
|                    |            |                                    |              | <b>TOTAL</b>           | <b>+22,79,00</b> |

At 10% the computation will be:

$$(-100,00,000)+(8,40,000 \times 2.49)+(14,01,800 \times 1.30) - (90,00,000 \times 0.62)+(19,63,000 \times 5.64) \\ = -100,00,000+20,91,600+18,22,34 - 55,80,000+110,71,320 = - 5,94,740$$

The return is a little over 9%

### Alternative (3)

(Extra reception lines followed by full Doubling: -)

The complete project inclusive of the first phase viz., provision of additional reception line at three stations and the second phase viz., doubling (after 5 years) the total life span being 30 years.

The rate of return works out to slightly above 13% as under :-

| Year                         | Cash flow  | Cumulative discount factor in 30 years at 12% |                    | Present Value    |
|------------------------------|------------|---|--------------------|------------------|
|                              |            | 1 <sup>st</sup> 5 year                        | Remaining 25 years |                  |
| 1971-72                      | 10,00,000  | -   | -                  | - 10 lakh        |
| 1971-72 to 1975-76 each year | 8,40,000   | 3.605   | -                  | +30.28 lakh      |
| 1975-76                      | 100,00,000 | .5674   | -                  | -56.74 lakh      |
| 1976-77                      | 90,00,000  | .5066   | -                  | -45.59 lakh      |
| 1976-77 to 2001-02 each year | 19,63,000  |   | 4.45               | +87.35 lakh      |
|                              |            |   |                    | <b>5.30 lakh</b> |

With this scheme an extra goods train cannot be introduced for two years during (1974 -75 to 1975-76). This entails an annual loss of Rs.1.26 lakh. (Extra wagons Rs.14175, extra locos 1,12,704 because of detentions as capacity utilization over 80%). Discounted to present values, this will reduce the above net figure of Rs.5.30 lakhs by further Rs.1.80 lakh but the rate of return will not be altered significantly.

EXAMPLE (6):-

### Providing a Diesel Loco Shed for homing 50 mainline B.G. Diesel Electric Locomotives 'X' Railway

(A) Capital costs (estimated) and phasing of expenditure (Rs. lakhs)

| (1) | Diesel  | Total | Loco Shed | Loco Motives |                                      |
|-----|---------|-------|-----------|--------------|--------------------------------------|
|     | 1974-75 | 295   | 25        | 270          | (10 WDM 2 Locos at Rs.27 lakhs each) |
|     | 1975-76 | 320   | 50        | 270          | - do -                               |
|     | 1976-77 | 311   | 41        | 270          | - do -                               |

|  |     |     |       |        |
|--|-----|-----|-------|--------|
| 1977-78  | 270 | -   | 270   | - do - |
| 1978-79  | 270 | -   | 270   | - do - |
|  |     | 116 | 1350  |        |
| Scrap value of locos (at Rs.1,00,000 per loco) |     |     | (-)50 |        |
|  |     |     | 1300  |        |

|      |  |   |              |                 |  |
|------|--|---|--------------|-----------------|--|
| (II) | Steam<br>(replacem<br>ent of<br>existing<br>locos):- | 1974-75<br>1975-76<br>1976-77<br>1977-78<br>1978-79 | Loco<br>Shed | Loco<br>Motives |  |
|      |  |   |              | 145             | 2.5 steam taken as equivalent to one WDM2<br>Cost per Steam Loco assumed at Rs.5.8<br>lakhs. |
|      |  |   |              | 145             |  |
|      |  |   |              | 145             |  |
|      |  |   |              | 145             |  |
|      |  |   |              | 145             |  |
|      |  |   |              | 725             |  |
|      | Estimated scrap value<br>(at Rs.23000 per loco)      |   |              | (-)29           |  |
|      |  |   |              | 696             |  |

Estimated economic life : Even though 40 years per steam and 30 years per diesel, the life is assumed to be 30 years in both cases. (Discount factor after 30 years is negligible).

(B) Operating and Maintenance costs:-

(i) Basic Data:-

|  | Steam   | Diesel  |
|--|---|---|
| (a) Km. per day for goods services(for steam and all Railway B.G. for diesel loco)   | 83  | 323   |
| (b) Average gross load per train (excluding loco)  | 1329 t  | 1591 t  |
| (c) Locos in use daily (with 17.6% repairs allowance for steam, or 15% of total holding and 12.1/2% for diesels)   | ...   | 43.75 WDM2  |
| (d) Steam locos on line equivalent to 50 WDM2 Locos- vide (a) to (c) above.<br>(This gives a ratio of 4.68 steam equal to one diesel however in the computations for this appraisal, the conservative and generally accepted ratio of 2.5 steam to one diesel has been adopted.) | 234   | $\frac{43.75 \times 323 \times 1591}{85 \times 1329} \times \frac{100}{85}$ |
| (e) Km per loco per annum (derived from diesel loco operation).  | $\frac{103.158 \times 1591}{1329 \times 2.5}$<br>= 49.398 | $\frac{323 \times 365 \times 7}{8}$<br>= 103.158                            |
| (f) Cost of fuel per 1000 GTKM   | Rs.2.94   | Rs. 2.31  |
| (g) Cost of repairs and maintenance per engine Km.   | Rs.0.71   | Rs. 0.45  |
| (h) Consumption of lubricating oil per 100 engine Km.  | 4.50 litres   | 11.2 litres   |
| (i) Cost of lubricant per litre (in terms of latest purchase rate etc.)  | Rs.1.71   | Rs.2.42   |

**(ii) Cost Data**

|     |   |   |   |
|-----|---|---|---|
| (a) | Repairs and maintenance per annum                                     | 0.71x49,398<br>=Rs. 35,073                  | 0.45x103,158<br>Rs.46,421                       |
| (b) | Cost of fuel per annum  | 1329x49398<br>x2.94x.001<br>=Rs. 1,93,011   | 1,591x103.158<br>x2.31x.001<br>= Rs. 379,127    |
| (c) | Cost of lubricating oil per annum                                     | <u>49,398x4.5x1.71</u><br>100<br>= Rs. 3801 | <u>103,158x11.2x2.42</u><br>100<br>= Rs. 27,960 |
| (d) | Wages of running staff per annum<br>(estimated for staff requirement) | Rs.23,493                                   | Rs.28,458                                       |
| (e) | Kilometrage allowance per annum                                       | Rs.8,052                                    | Rs.13,411                                       |
| (f) | Total cost per locomotive per annum                                   | Rs.2,63,430                                 | Rs.4,95,377                                     |
| (g) | Equivalent cost at 2.5 steam : 1 diesel                               | Rs.6,58,575                                 | Rs.4,95,377                                     |
| (h) | Saving in diesel operation per loco per annum                         | Rs.1,63,198<br>(say) Rs.1.63 lakh           | .....   |

**(C) Financial Analysis (DCF) (Cash outflows)**

Rs. lakhs

| Year                    | Index   | Interest/<br>Discount<br>factor @ 10% | Steam     | Diesel    | Absolute | Saving (+)<br>Additional (-)<br>Discounted |
|-------------------------|---------|---------------------------------------|-----------|-----------|----------|--|
| 1974 -75                | -2      | 1.21                                  | (145+66)* | (295+49)* | -133     | -161                                       |
| 1975 -76                | -1      | 1.10                                  | (145+132) | (320+98)  | -141     | -155                                       |
| 1976 -77                | 0       | 1.0                                   | (145+198) | (311+147) | -115     | -115                                       |
| 1977 -78                | 1       | 0.91                                  | (145+263) | (270+198) | -50      | -45  |
| 1978 -79                | 2       | 0.83                                  | (145+329) | (270+245) | -41      | -34  |
| 1979 - 80 to<br>2009-10 | 3 to 30 | 6.93                                  | 329       | 245       | +84      | +582                                       |
| Residual<br>value       | 30      | 0.057                                 | +29       | +50       | +21      | +1   |
|                         |         |                                       |           |           |          | <u>+23</u>                                 |

\* Capital and Revenue cash outflows are shown separately for easy reference.

This analysis shows that the proposed diesel shed to home 50 WDM2's is financially justified, the return under DCF being a little over 10%

\*\*\*\*\*



## ANNEXURE 'F'

### ECONOMIC EVALUATION OF RAILWAY INVESTMENTS

A purely financial appraisal of investment proposals does not necessarily lead to the selection of projects which best serve the needs of the community. The inadequacy of financial analysis in this regard derives from the fact that projected cash inflows and outflows associated with feasible investment alternatives do not correctly reflect the actual benefits to the community flowing from them or the costs that they impose on the economy. Financial and economic appraisals, however, need not always lead to conflicting decisions a financially viable project will also be acceptable on economic grounds whenever the economic return on investment is likely to be at least as high as its financial yield. But, there can be instances of financially sound investment proposals which may not turn out to be worthwhile propositions because the relevant cash outflows do not include all the associated costs to the economy. Again, an investment which is not expected to be profitable, may still yield an adequate, or even a fairly high, economic return if the projected cash earnings represent only a part of the benefits or incomes that are likely to be generated by it.

2. Economic benefits attributable to a particular investment can, for a number of reasons, exceed the revenues directly accruing to the Railways in the form of fare and freight receipts. In the first place, most users of a facility may be willing and able to pay somewhat more than what they are actually charged by the Railways. Secondly, there may also be instances where what the consumers are actually able to pay for rail transportation is (because of uneven-income distribution) less than the benefit they derive from it. This, indeed, is the main justification for a preferential fare structure for certain passenger and suburban services. Finally, for economic or social policy reasons freight rates on certain key commodities may be set at levels which do not fully cover rail transportation costs. The entire benefit derived by the users of Railways can never be qualified; however, at least that part of it which consists of the difference between cost of transportation and fares or freight rates actually charged-can be precisely ascertain. \*The provision of a rail transport facility thus directly adds to the well-being of the community by more than the receipts that accrue thereby to the Railways.

\*Likewise, the difference between the cost to the consumer of rail transportation and that of other modes of transport replaced (partly or wholly) by it is a tangible and measurable social gain.

3. Rail transportation, however, can make a substantial indirect contribution as well to general well-being by facilitating economic expansion. A new line, in a backward region not well endowed with alternative modes of transportation, stimulates the growth of output and employment by widening the market for local products as well as by creating a market for some hitherto unexploited natural resource. The quantification of such indirect benefits can at best be approximative. For one thing, the expected expansion of regional or local economic activity is difficult to forecast. For another, the quantification of "developmental benefits" poses the problem of allocating expected additions to output and incomes between the Railway project and other complementary investments in industry, agriculture or commerce.

4. Great care should be taken in estimating social benefits for the purpose of economic appraisal of railway investments. Such benefits should, to the extent possible, be quantified with a reasonable degree of accuracy. Thorough investigations at the traffic survey stage would help in identifying the "developmental effects" and in estimating broadly the magnitude the complementary investments that may be required. Also, the assumptions and reasons underlying any judgement about non-quantifiable benefits. should be clearly spelt out. Fortunately, the assessment of social benefits is necessary only in the case of proposed investments in new rail lines or operations ; as regards investment for modernisation and improvement, which constitute the bulk of the Railways' capital outlay, one need only estimate the social costs entailed by investment alternatives In order to pick out the least cost solution from the point of view of the economy.

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5. The expenditure flows associated with Railway projects can, to varying extents, diverge from the cost to the economy of acquiring resources needed for their implementation and operation. The prices at which certain inputs and resources are made available to the Railways, for instance, may understate or exaggerate their, real cost to the economy. Thus the interest rate which is in line with the usual return on new capital investment in the economy may not be the same as the "dividend" the Railways have to pay on the capital-at-charge. Similarly, the rupee equivalent of direct foreign exchange expenditure may differ from the cost of saving or earning an equivalent amount of foreign exchange. Moreover, the relative prices of various types of equipment and materials purchased by the railways will be different from the comparative costs of producing them for the reason that the rates of indirect taxes (or subsidies) vary from product to product. Lastly, there are certain types of real costs which do not at all get recorded in the financial cash flows. Environmental damage can, for example, be a major unrecorded element of cost.

6. In selecting investments which impose the least cost on the economy, cash out flows have to be recomputed in such a way as to minimise the distortions caused by the use of prices actually paid for inputs (including the prices of capital and foreign exchange) and by the neglect of other costs which do not figure at all in expenses. Environmental effects of investments are the most difficult to estimate. However in a number of cases the choice of projects may be influenced much more by the interest and exchange rate, that are utilised than by the correction of distortions introduced by indirect taxes, subsidies and environmental effects. A preliminary sensitivity analysis is useful for picking out the more important, of the factors distorting costs; such factors can then be subjected to a detailed investigation.

7. For economic evaluation of Railway Projects, the interest or discount rate is currently set at 10 percent. This implies that the cost of capital comprises a depreciation or capital recovery factor and interest charged at 10 per cent per annum; a project is thus just acceptable if the expected earnings from it during its lifetime make it possible to recover the investment with a return of 10 per cent per annum, that is, if the DCF rate of return on it is 10 percent.

8. In the cash flows utilised for economic, evaluation of high speed diesel oil is not valued at the price actually paid by the Railways for it. Instead, all taxes and duties payable on it are excluded from the price; and, the duty-free price is adjusted upwards so as to allow for the comparative scarcity of crude oil in the Indian economy. At present this adjustment factor is exactly half the current rate of excise duty on high-speed diesel oil.

9. There is no direct readjustment of the official exchange rate for the purpose of computing the scarcity value of imported equipment, spares and materials. However, there is an implicit adjustment in as much as the duty paid on imports is retained as a cost item in the cash-flows. Ideally, other indirect taxes like excise duties, sales taxes, local taxes and other cesses and levies, should be excluded from the cost of domestically procured inputs. But in many cases it has been found, particularly in the analysis of investment for modernisation of traction, that the exclusion of indirect taxes and similar levies does not make any material difference to the ranking of the proposed alternatives.

10. Electric power is valued not at the price at which it is sold to the Railways by the State Electricity Boards but at its estimated cost to the economy. The latter is derived from actual production cost by revaluing its interest component at the rate of 10 per cent per annum and its foreign exchange component at an exchange rate 33 per cent-higher than the current official rupee price of foreign currencies.

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## FINANCIAL AND ECONOMIC EVALUATION OF- INVESTMENT ALTERNATIVES

### An Example.

A highly simplified hypothetical example of choice between diesel and electric traction is presented here for the purpose of illustrating the essential difference between financial and economic evaluation. This type of choice is basically a problem of minimising the cost of handling a given volume of traffic over specified sections.

The two project alternatives, dieselisation and electrification, are defined as follows-

- (i) The project life, which includes the construction period, extends in both cases up to 44 years.
- (ii) The level of traffic remains unchanged over the life time of the project.
- (iii) Annual operating expenses exclude depreciation and do not vary from one year to another.
- (iv) Capital costs exclude interest during construction\*\*
- (v) Capital outlay on dieselisation is spread over a period of three years; it comprises the expenditure on acquisition of rolling stock and construction of sheds.
- (vi) Capital outlay on electrification is phased over four years; it comprises the expenditure on rolling stock and construction of OHE.

\*\*If the income flows are computed from the date of completion of the project, the capital outlay will be compounded at the desired interest rate.

Given these assumptions, the financial cost cash-flows associated with the two illustrative traction alternatives can be presented in the following manner :

| Financial cost to Railways                      |        | (Rs. crores). |
|---|--------|---------------|
| Year  | Diesel | Electric      |
| 1   | ..     | 3.0           |
| 2   | 0.5    | 6.0           |
| 3   | 0.5    | 15.0          |
| 4   | 10.0   | 6.0           |
| 5 <sup>th</sup> to 44 <sup>th</sup> (each year) | 4.0    | 2.5           |

#### Discounted Present Worth of Financial Costs.

| Interest Rate. | Diesel | Electric |
|----------------|--------|----------|
| 6%             | 56.5   | 55.3     |
| 7%             | 49.2   | 50.3     |

It would be seen that when discounted at 6 per cent the present worth of the financial cost flow relating to electrification works out to be lower than that of the financial cost flow associated with dieselisation by Rs. 1.2 crores. But the situation is reversed when the cost flows are discounted at 7 per cent, in which case dieselisation turns out to be cheaper by Rs. 1.1 crores. Thus, in this hypothetical case, the depreciation inclusive financial cost of electrification is lower only at rates of interest below 7 per cent. The rate of interest at which the two alternatives will impose identical costs can be found out by linear interpolation. This turns out to be 6.5 percent; at lower rates of interest electrification is the cheaper alternative; but becomes the costlier one at interest rates exceeding 6.5 per cent. This is as it should be; for electrification is the more capital intensive mode of traction.

The estimation of cash-flows relevant for the computation of the cost to the economy is based on the following assumptions :-

(i) The basic price, inflated to the extent of 50 per cent of the excise duty, is taken as the appropriate scarcity value of high-speed diesel oil.

(ii) The cost to the economy of electricity generation and transmission is assumed to be 7 paise per KWH as compared to 10 paise per KWH assumed to be actually paid by the railways.

(iii) Fuel costs constitute 70 per cent of operating expenses under diesel and 50 per cent of operating expenses under electric traction.

Under these assumptions, the cost to the economy of the uniform annual operating expenses associated with dieselisation and electrification works out to be Rs. 3.00 and Rs. 2.12 crores respectively. But, the cost to the economy of capital outlays continues to be the same as the financial cost. The discounted present worth of the cash flow corresponding to the cost to the economy at 3 and 4 percent interest rates is as follows:

Discounted Present Worth of Costs to the Economy.

| Interest Rate | Diesel | Electric |
|---------------|--------|----------|
| 3%            | 71.4   | 70.8     |
| 4%            | 60.2   | 62.4     |

It will be seen from the above that in this hypothetical case, from the point of view of cost to the economy, electrification turns out to be cheaper than dieselisation only at rates of interest which do not exceed 4 per cent. The break even rate of interest, at which both alternatives involve identical costs, is approximately 3.2 per cent.

\*\*\*\*\*

**ANNEXURE 'G'**  
(See Paragraph 240)

The examples given below are intended to illustrate the principles set out in [paragraph 238](#) et seq. The data assumed are hypothetical and the conclusions arrived at in these examples are purely illustrative. The methods adopted are not to be regarded as exhaustive or as precluding the use of alternative methods which may be found to be more appropriate.

1. Renewal of a Locomotive.-(i) Whether to recondition or to renew a locomotive, given the following data :-

| Particulars.                             | Old Locomotive.                   | New Locomotive              |
|--|-----------------------------------|-----------------------------|
| Cost of the locomotive                   | Rs. 50,000<br>(Second-hand cost). | Rs. 5,00,000<br>(New cost). |
| Cost of reconditioning                   | Rs. 50,000                        | .....                       |
| Rate of interest                         | 6 percent.                        | 6 percent.                  |
| Life                                     | 10 years                          | 40 years                    |
| Scrap Value                              | Rs. 10,000                        | Rs. 20,000                  |
| Maintenance Operation and Repair Charges | Rs. 50,000 a year.                | Rs. 40,000 a year           |

- (ii) The average annual cost of the existing locomotive after reconditioning would be Rs.62,831 made up of the following :-**

|   |        |
|---|--------|
|   | Rs.    |
| (a) Cost of maintenance, operation, repairs, etc.                       | 50,000 |
| (b) Interest at 6 per cent on Rs. 1,00,000 (Rs. 50,000 Plus Rs. 50,000) | 6,000  |
| (c) Sinking Fund Payment at 6 per cent ( $90,000 \times 0.0759$ )       | 6,831  |
| Total   | 62,831 |

- (iii) The average annual cost of the new locomotive would be Rs.75,520 made up of the following:-**

|   |        |
|---|--------|
|   | Rs,    |
| (a) Cost of maintenance, operation, repairs, etc.   | 40,000 |
| (b) Interest at 6 per cent on Rs.5,40,000 (i.e., new cost Rs.5,00,000+ the second hand cost of the old locomotive, Rs.50,000- the scrap value of old locomotive Rs. 1 0,000). | 32,400 |
| (c) Sinking Fund Payment at 6 per cent ( $4,80,000 \times 0.0065$ ).  | 3,120  |
| Total   | 75,520 |

- (iv) It follows from the above figures that, with the data assumed, it is cheaper to recondition the old locomotive than to replace it by a new one.

- (v) Applying the DCF method also, it is observed that for an initial investment of Rs. 5 lakhs, the NPV for 40 years on the basis of the saving of Rs.10,000/- reckoned at 10 per cent p.a. adds up to Rs.1,02,210 only ( $10,000 \times 9.779$ ) + ( $20,000 \times 0.0221$ ). The purchase of new locomotive is, therefore, not justified.

2. Renewal of a Bridge.- (i) Whether to recondition or to renew a bridge, given the following data:-

| Particulars.                       | Old Locomotive. | New Locomotive. |
|------------------------------------|-----------------|-----------------|
| Cost                               | 10,000          | 40,000          |
| Scrap Value                        | 2,000           | 4,000           |
| Scrap Value (after reconditioning) | 4,000           | .....           |
| Interest                           | 6 per cent      | 6 per cent      |
| Life                               | 30 years        | 60 years        |
| Reconditioning Cost                | 10,000          | .....           |

Note.-Maintenance cost is the same for both the reconditioned and new bridge

- (ii) The annual cost of service of the reconditioned unit will be Rs. 1,402 vide details given below:-

|  |       |
|--|-------|
|  | Rs.   |
| (a) Interest at 6 percent on Rs.20,000 (i.e. Rs:10,000+10,000)         | 1,200 |
| (b) Sinking Fund Payment at 6 percent on Rs16,000 (i.e. 16,000x0.0126) | 202   |
| Total  | 1,402 |

- (iii) The annual cost of service of the new girders ,will be Rs.2,948 vide details below.-

|   |       |
|---|-------|
|   | Rs.   |
| (a) Interest at 6 per cent on Rs.48,000, i. e., on cost of new girders + second hand value of old girders-scrap, value of old girders) Rs. 40,000+ Rs. 1 0,000-Rs.2,000). | 2,880 |
| (b) Sinking Fund Payment at 6 per cent on Rs.36,000 (Rs,40,000-Rs.4,000) 36,000x0.0019)   | 68    |
| Total   | 2,948 |

- (iv) It follows that reconditioning is cheaper.

3. Renewal of Permanent Way.--(i) To determine whether a line of 85 lb. B. H. rails should be fitted with 2 additional sleepers, one, Duplex joint sleeper and new fish-plates and bolts, or replaced with 90 lb. F. F. rails, given the following data :-

|  |                                    |
|--|------------------------------------|
| For providing additional fittings.                       | Fitting new 90lb.rails             |
| Cost of two additional sleepers including fittings Rs 60 | Cost of 2 new 90 lbs. rails Rs.550 |
| Cost of Duplex joint sleepers including fittings 64      | Including carriage and laying..... |

|  |            |                  |             |
|--|------------|------------------|-------------|
| Cost of fish-bolts and plates                      | 10         | Life             | 60 years.   |
| Cost of fitting these in each                      | 7          | Scrap value      | Rs. 207     |
| Life of 85 lb. rails                               | 30 years   | Rate of interest | 6 per cent. |
| Scrap value of rails 36 ft. long                   | Rs. 100    |                  |             |
| Scrap value of fittings                            | 5          |                  |             |
| Second-hand cost of two 85 lb. rails, 36 ft. long. | 243        |                  |             |
| Rate of interest                                   | 6 per cent |                  |             |

Note -(1) Maintenance and repair cost are considered to be the same in both cases.

(2) Steel scrap has a very high price in the market and new rails are comparatively cheap from indigenous sources.

(3) The old rails cannot be used elsewhere.

(ii) The average annual cost of service of the existing 85 lb. track after additional fittings are made will be Rs. 26.27 vide calculations below:-

(a) Interest at 6 per cent on the—

|  |            |
|--|------------|
|  | Rs.        |
| Cost of 2 sleepers                         | 60         |
| Cost of Duplex Joint sleepers new          | 64         |
| Cost of fish-plates and bolts              | 10         |
| Cost of fitting                            | 7          |
| Second-hand value of old rail              | 243        |
|  | <hr/>      |
|  | 384        |
| Less scrap value of fish- plates and bolts | 5          |
|  | <hr/>      |
|  | 379 =22.74 |

(b) Sinking Fund Payment at 6 percent on Rs. (60+64+10+7+ 243) -  
(100+5) or Rs.279=0.0126x279)

3.53

Total

---

26.27

---

(iii) The average annual cost of service of new rails will be Rs.41.93, vide calculations below.-

Rs.

(a) interest at 6 percent on-

|   |           |
|---|-----------|
| Cost of new rails and fittings, etc.        | 550       |
| Plus second-hand cost of old rails.         | 243       |
|   | <hr/>     |
| Less scrap value of old rails and fittings. | 793       |
|   | 105       |
|   | <hr/>     |
|   | 688=41.28 |

(b) Sinking Fund Payment at 6 per cent on Rs.500-207  
=(343x0.0019)

=0.65

Total

---

41.93

---

(iv) With the data assumed it is cheaper to provide 2 extra sleepers 1 Duplex Point sleepers and new fish-plates and bolts to the existing track than to replace it with 90 lb. F. F. rails. If, however, it were possible to use the B. H. rails elsewhere on the line, it might be cheaper to provide new rails than to provide these additional fittings.

4. Re-alignment of Line.-(i) To determine whether the re-alignment of a track by abandoning the arc and following the chord, is justifiable, given the following data :-

|   |              |
|---|--------------|
| Length of arc                                   | 15 miles     |
| Length of chord                                 | 10 miles     |
| Cost of chord                                   | Rs. 5,00,000 |
| Scrap value of items recoverable from the arc   | Rs. 50,000   |
| Scrap value of items recoverable from the chord | Rs. 40,000   |
| Second-hand value of all assets of the arc      | Rs. 3,00,000 |
| Savings in operation and maintenance costs      | Rs. 70,000   |
| Loss on tickets owing to reduction of mileage   | Rs. 10,000   |
| Extra traffic expected.                         | Rs. 15,000   |
| Rate of interest.                               | 6 per cent   |

Note.-There is keen bus competition on the section running along the arc and the chord will cut this competition as the road runs along the arc and not the chord, and it is very unlikely another road will be built along the chord.

(ii) The net saving due to re-alignment is Rs. (70,000-10,000+ 15,000) or Rs. 75,000.

(iii) The average annual cost excluding the cost of operation and maintenance of the realigned track will be Rs.49,140 vide calculations below.-

|   |               |
|---|---------------|
|   | Rs.           |
| (a) Interest on Rs. 7,50,000 (i.e. Rs. 5,00,000+ Rs. 3,00,000-Rs. 50,000) at 6 per cent.  | 45,000        |
| (b) Sinking Fund Payment at 6 percent required to provide Rs.4,60,000(i. e. 5,00,000-Rs.40,000) at the end of 35 years-(0.0090x4,60,000). | 4,140         |
| Total   | <u>49,140</u> |

Note.-There are many assets on the track having varying normal lives. For the purpose of this calculation, a life of 35 years has been taken as a fair average for all the assets involved.

(iv) Hence it may be seen that realignment is justified since, it will yield a net saving of about Rs.26,000 p. a.

\*\*\*\*\*



**ANNEXURE-'H'**  
(See Paragraph 242)

The examples given below are intended to illustrate the principle set out in paragraph 241. The data assumed are hypothetical and the results arrived at in these examples are purely illustrative.

1. If, in the case of an asset where the average annual cost of service is the basis on which the second hand value has to be fixed.-

|  |          |
|--|----------|
| the normal life is   | N years. |
| the first cost is  | Rs. C    |
| the scrap value is   | Rs. S    |
| life as second-hand asset is   | n years. |
| the annual cost of operation and maintenance, repairs, etc. of the asset while new is.                                     | Rs. 0    |
| the annual cost of operation and maintenance, repairs, etc. in the second-hand condition r is the annual rate of interest. | Rs. 01   |

$dN$  is the sinking fund Payment required to be paid annually so that at the end of N years, the sinking fund provides Re. 1.

$dn$  is the sinking fund Payment required to be paid annually so that at the end of n years the sinking fund provides Re. 1.

then, 'X', the second-hand value of the asset is such that the average annual cost of the second hand asset is equal to the average annual cost of the new asset, or  $Xr + (X-S) dn + 01 = Cr + (C-S) dN + 0$ . Simplifying the equation, we have :-

$$\begin{aligned} Xr + X dn - Sdn + 01 &= Cr + (C-S) dN + 0. \\ X(r+dn) &= Cr + (C-S) dN + 0 + Sdn - 01. \\ X &= \frac{Cr + (C-S) dN + 0 + Sdn - 01}{r+dn} \end{aligned}$$

Illustration. - If Rs. 10,000 be the first cost of an asset with 60 years of normal life and a scrap value of Rs.2,500, the rate of interest is 3 percent or .03 per rupee and the average maintenance and repair cost for the first 20 years is Rs.250 and for the next 40 years Rs.350, then applying the above formula, the second-hand value at the end of 20 years will be.

$$\text{Rs. } \frac{10,000 \times .03 + (10,000 - 2,500) \cdot 0061^* + 250 + 2,500 \times .0133^* - 350}{.03 + .0133}$$

Or  $\frac{279}{.0433}$  i.e., Rs.6,443.

\* These are obtained from the Table in [Annexure B](#).

2. In the case of an asset the second-hand value of which is to be determined on the basis of 'the average cost per unit of service; if the same notation as in Example (1) were used and.-

if  $u$  is the average number of annual units of service rendered by the asset while new, and  $u_1$  the average number of units of service rendered by the asset while second-hand, then,  $X$  the second-hand value of the asset is such that-

|  |
|--|
| $\frac{Xr + (X-S) \frac{dn+01}{U_1}}{U_1} = \frac{Cr + (C-S) \frac{dN+0}{u}}{u}$                               |
| <p>There fore, <math>X = \frac{u_1 / u [ Cr + (C-S) \frac{dN+0}{u} ] - 0.1 S \frac{dn}{r+dn}}{r+dn}</math></p> |

Illustration.- If Rs. 1,00,000 be the cost of an asset with a normal life of 35 years and a scrap value of Rs.10,000; if the rate of interest is assumed to be 3 percent or .03, the average operation, maintenance and repairs costs while new, Rs. 1,20,000 per annum and the average operation, maintenance and repairs costs in the second-hand condition Rs. 1,03,000 per annum; and if, the average serviceability of the asset while new be 1,20,000 units per annum and 1,00,000 units in the second-hand condition, then applying the formula above, the second-hand value of the asset at the end of 20 years will be.-

$$\begin{aligned}
 & \frac{1,00,000}{Rs. 1,20,000} - [ 1,00,000 \times .03 + (1,00,000 - 10,000) \cdot 0.165 + 1,20,000 ] - 1,03,000 + 10,000 \times .0538 \\
 & \qquad \qquad \qquad .03 + .0538 \\
 \text{or } & \frac{2551}{2} \times \frac{1}{.0838} \qquad \text{i.e, Rs. 15,221 nearly.}
 \end{aligned}$$

END